

**MAE 4273: EXPERIMENTAL FLUID DYNAMICS**

*Lab Report 2*

*Fall 2019*

**Cylinder Wake Survey**

School of Mechanical and Aerospace Engineering

Oklahoma State University

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**ABSTRACT**

The inclusion of obstacles in a flow field is a common occurrence in external flow scenarios and understanding the resulting disturbance is critical to measuring the induced drag coefficient. This lab examines the effect of a 2” PVC pipe (cylinder) spanning the entire  $z$  direction of the Oklahoma State University Endeavor Wind Tunnel. It looks at the flow quality in the cylinder’s wake and determines the resulting drag force and drag coefficient by measuring differential pressure throughout sections of the cylinder’s wake with a pitot static probe pressure transducer. The cylinder creates a flow disturbance wake most significant immediately behind the cylinder that depreciates further back as the flow smooths out. A drag force as high as 15N was calculated at a flow velocity of 30m/s as a result of the cylinder’s induced wake. This cylinder disrupted the flow and higher levels of drag were induced at higher flow speeds and correspondingly higher Reynolds Numbers.

## **1. INTRODUCTION**

External flow studies involve the introduction of an object or assembly that disrupts the initial flow conditions and paths. The flow disruption can provide engineering and physical benefits such as lift generated from an aircraft airfoil. Understanding the associated flow disruption allows induced drag to be quantified for a given shape at certain flow velocities, and therefore, Reynolds Numbers. Complex shapes may be impossible to analyze mathematically without the aid of computer simulations, and therefore the resulting drag force and drag coefficient may be best determined from experimental data in a wind tunnel.

Determining drag force from an object in an experimental setting can be accomplished in various ways. Nan discusses seven different methods including floating elements on water and oil baths or mechanical devices, load cells, and the Irwin sensor technique [1]. These methods each have their respective advantages including low cost, noise pollution, and ease of calibration but introduce complexities such as sensor sensitivity or facility requirements. None of the methods described include the pitot-static probe pressure measurements and drag force calculation that is presented in this lab. This paper discusses other techniques that could be used to validate and compare the data acquired from one method to another.

External flow testing can also be applied to models of larger-scaled objects such as an aircraft. Warrington explained dynamic similitude as a means to test various airfoils and their drag characteristics and the application to full-scale aircraft. The complications of such wind tunnel testing were also discussed including the induced drag from supporting structures of the model and instruments, as well as friction drag from the wind tunnel walls.

The objectives of this laboratory are as follows:

1. Calibrate and correct the pressure transducer for tunnel fan RPM speeds and the corresponding tunnel flow velocities
2. Measure the spanwise pressure differential behind the wake of a cylinder spanning the entire height of a wind tunnel (to mitigate three-dimensional flow effects) and further into and behind the wake of the initial position.
3. Calculate the induced drag of the wake
4. Calculate the resulting drag coefficient and compare the values to published data for the obtained range of Reynolds Numbers

## **2. EXPERIMENTAL ARRANGEMENTS**

### ***Materials:***

This laboratory primarily used test equipment and did not measure samples, other than the air in the closed-circuit wind tunnel. Inside the tunnel, a 2" PVC pipe was installed in the  $z$  direction to span the entire height of the tunnel and create a two-dimensional flow field. The outer diameter of the pipe was 6cm. It was taped to the bottom of the tunnel and created a 0.25" ledge above the tunnel floor.

### ***Facilities and Equipment:***

The equipment used for this laboratory exercise was the Aerolab closed-circuit wind tunnel (Aerolab, LLC, Jessup, MD, USA) and LabView 2018 (National Instruments, Austin, TX, USA) software suite located in Endeavor 140 at Oklahoma State University. The tunnel is capable of fan speeds of 880 RPM to generate airflow velocities up to 133 km/h in a closed-loop system [1]. Due to the closed-loop nature of the tunnel, it utilizes a M1-3A refrigerant system (Advantage Engineering, Greenwood, IN, USA) to maintain the air at a constant temperature throughout wind tunnel operation. The test section features clear panes for viewing test articles and measures 1.22m in length ( $x$ -direction), 0.61 m in depth ( $y$ -direction), and 0.61m in height ( $z$ -direction). Due to a manufacturer-installed load cell section that raised concerns about flow behavior, a portion of the tunnel was removed and replaced with an acrylic cover to maximize the test section volume and mitigate unwanted air flow patterns. The cover induces a slight cross-section change in the test section by ramping up at  $6^\circ$  from the test section entrance and ramping back down at the test section exit. This assembly with the pitot-static probe and 2" PVC pipe is shown in Figure 1.

The wind tunnel is controlled and operated by a virtual instrument (VI) coded in LabView that Aerolab provided with the tunnel. Their included traverse system is integrated into the VI and allows for motion control of an instrument (in this case, a pitot-static probe) inside the test section, and data acquisition during tunnel operation. This VI can be seen in Figure 2. The interface allows monitoring of the traverse and live data, as well as buttons for operating the tunnel and data acquisition on the far right. Data may be collected continuously or manually in bursts to record traverse position, fan RPM, static pressure, and many flow properties. These data are written to a .CSV file which can be opened in Excel and manipulated like any other spreadsheet for data analysis.

### **Experimental protocols:**

This laboratory exercise involved running a matrix input for 12 different configurations: 8 fan speeds measuring the same  $y$ - $z$  plane behind the PVC pipe at  $x = 22.3\text{cm}$ , 2 fan speeds closer to the cylinder in the  $x$ -direction at  $x = 18.4\text{cm}$ , and 2 fan speeds farthest from the PVC pipe in the  $x$ -direction at  $x = 36.8\text{cm}$ . These configurations are described in Table 1.

The pitot-static probe's initial position in the tunnel was recorded using cartesian coordinates in relation to the test section entrance ramp up ( $x$ -direction), far back wall of the wind tunnel test section ( $y$ -direction) and test section base ( $z$ -direction). Its initial location relative to the test section entrance and PVC pipe is shown below in Figure 3. With the tunnel fan turned off and zero airspeed, the ambient pressure was recorded from the Aerolab VI pressure transducer. The room temperature was recorded from the thermostat thermometer.

Beginning with 40 RPM fan speed control input via VI, the fan speed indicator was allowed to reach steady state, then a pre-programmed .CSV file was executed by the VI and traverse to record 100 samples at 2.5mm (0.1 inch) intervals through the  $y$ -direction. The probe spanning the  $y$ - $z$  plane was to profile the side-to-side plane of the cylinder wake. This process is repeated in intervals of 100 RPM, up to 740 RPM.

To study the effect of cylinder wake in the  $x$ -direction, four additional runs were conducted, two at 140 RPM and two at 340 RPM. The first  $x$ -direction adjustment put the probe at 18.4cm behind the PVC pipe back edge, the second at 36.8cm behind the back edge. The same 2.5mm increments were evaluated by the traverse and probe. The configurations are listed in Table 1.

### **Calculated quantities:**

The data of interest obtained from calibration and tunnel flow quality evaluation include model and dynamic pressure, and fan speed (RPM). Other parameters obtained from ambient conditions include  $P_{air} = 97.56\text{ kPa}$ ,  $T_{air} = 295.93\text{ K}$ , and  $R_g = 287.1 \frac{\text{J}}{\text{kg}\cdot\text{K}}$ .

The ideal gas equation is used to find density from air pressure  $P$ , the gas constant for air  $R_g$ , and air temperature,  $T$ .

$$\rho = \frac{P}{R_g T}$$

To obtain flow velocity from total and static pressure as measured by the pressure transducer and pitot-static probe, Bernoulli's equation is utilized where  $P$  is pressure,  $\rho$  is density,  $V$  is flow velocity,  $g$  is gravitational acceleration, and  $h$  is elevation. The equality between subscripts 1 and 2 indicate a conservation of energy between two states.

$$P_1 + \frac{1}{2}\rho V_1^2 + \rho g h_1 = P_2 + \frac{1}{2}\rho V_2^2 + \rho g h_2$$

Reducing the equation by eliminating the potential energy terms and assuming a  $V_1 = 0\text{ m/s}$  for total pressure yields:

$$V_2 = \sqrt{\frac{2(P_1 - P_2)}{\rho}}$$

Defining  $P_1 = P_t$  for total pressure and  $P_2 = P_s$  for static pressure, results in the following equation that allows for the calculation of flow velocity.

$$V_2 = \sqrt{\frac{2(P_t - P_s)}{\rho}}$$

For  $V$  as freestream velocity,  $x$  as test section length to pitot probe, and  $\mu$  as dynamic viscosity, Reynolds Number is calculated by:

$$Re = \frac{\rho V x}{\mu}$$

Errors are found by dividing the difference of true and calculated values by the true value.

$$Error = \frac{true\ value - measured\ value}{true\ value}$$

For evaluating drag on the cylinder, the drag force is calculated as

$$D = \frac{1}{2} \rho V^2 A C_d$$

Given freestream and wake velocity data, the drag force is more practically calculated by using a drag integrand

$$D_{integrand} = \rho L(u(U_\infty - u))$$

and utilizing the trapezoidal integration rule

$$D = \int_a^b f(x) dx \approx (b - a) \cdot \frac{f(a) + f(b)}{2}$$

For determining the drag coefficient,  $C_d$ ,  $A$  is the frontal area of the cylinder as viewed by the flow. Conversely, the equation may be rewritten to calculate  $C_d$ :

$$C_d = \frac{D}{\frac{1}{2} \rho V^2 A}$$

### **3. RESULTS AND DISCUSSION**

#### ***3.1. Summary***

This laboratory utilized calibrated pressure data to obtain velocity calculations in the wind tunnel and characterize the effect of a cylinder in terms of flow quality downstream of the cylinder obstruction.

The results indicate that wind tunnel flow disruptions exist as a result of the cylinder installed in the center of the flow field. Reductions in wake pressure and velocity are most prevalent directly behind the center of the cylinder. Furthermore, greater drag forces and turbulence exist closest to the cylinder in terms of downstream distance. Finally, flow disruptions are at their maximum for high freestream velocities and Reynolds numbers.

#### ***3.2. Pressure Transducer and Tunnel Fan RPM Calibrations***

To begin this lab's data analysis, a MATLAB script [2] was largely written by Dr. Arvind Santhanakrishnan to automatically calculate values, analyze the raw data, and generate plots by calling upon the saved CSV files.

Initial conditions were defined for ambient temperature, pressure, air gas constant, and dynamic viscosity. The cylinder diameter and length were defined as well as an array for the RPMs studied. These RPMs are listed in Table 1. Other information from the data acquisition was also included such as the number of samples collected (100), and y-locations sampled (142).

Calibration terms were included that utilized findings from the first laboratory, namely the corrected pressure differential vs RPM slope value of 0.9496. The intercept is not included as to prevent the inclusion of negative numbers. Additionally, the freestream velocity equation slope was used to calculate the freestream velocity for a given wind tunnel fan speed. This slope value is 0.0186, but again, the intercept is not included.

At this point, the pressure transducer is calibrated, and the tunnel fan RPM can be associated with a freestream velocity. The ideal gas and Bernoulli's equations are used to calculate wake velocity,  $u$ , and its maximum value is used as the freestream speed,  $U_{inf}$ .

### 3.3. Wake Profiles

For analyzing wake profiles, plots were generated via the MATLAB script to examine how pressure, freestream velocity, wake velocity, drag force, and drag coefficient vary throughout the wind tunnel's cross section.

The first 8 configurations were taken at varying RPMs (40-740) with the probe at a constant  $x$ -distance of 22.9cm behind the cylinder trailing edge. These plots are shown in Figures 5-10.

Figure 5 plots wake pressure differential as a function of probe location spanwise across the tunnel and through the cylinder wake. It also provides the error that results from each sampling location. This figure indicates that at higher freestream velocities, the pressure suction effect of the cylinder is more pronounced and induces a greater pressure difference behind the cylinder. The error also fluctuates more in higher wake velocities. Figure 6 supports this statement as well by graphing freestream velocity as a function of the probe position. At the higher freestream speeds, the velocity differential becomes more significant with as much as a 10m/s reduction as a result of the cylinder obstructing the flow. Figure 7 agrees with this by plotting non-dimensional probe position and wake velocity as fractions of the tunnel width and freestream velocity, respectively. At the lowest observed Reynolds number of 3423, the difference between  $y$  and  $D$  and  $u$  and  $U_{inf}$  is the most significant. One can conclude that for low Reynolds numbers and flow velocities, the cylinder induces the greatest difference in wake and freestream velocities.

Figures 10-14 are plots for the pitot-static probe at an  $x$ -position of 18.4cm behind the cylinder trailing edge. This is closer to the cylinder and inside more of the generated wake. Similar to Figure 5, Figure 11 displays a greater wake pressure difference is created at higher freestream speed, with larger error values as well. This is further supported by Figure 12 that shows as much as a 7m/s reduction in measured wake velocity behind the cylinder at 14m/s freestream velocity. For both fan speeds, the non-dimensionalized wake velocity has the greatest difference from unity immediately behind the cylinder. One can conclude that for the probe closer to the cylinder, strong obstructions to the flow are also generated as a result of the cylinder.

Finally, an  $x$ -location farthest from the probe was selected at 36.8cm behind the cylinder to study how added downstream distance affects the wake flow recovery. Figures 15-19 are the same plots as previously but for data taken 36.8cm downstream. In Figure 15, a less significant pressure distance is observed than with the 18.4cm location. Figure 16 shows only a 3.5m/s reduction in wake velocity at 13m/s freestream velocity, *half* of that for the probe closest to the cylinder wake. There is less of a non-dimensional difference for this added downstream location as can be observed in Figure 17. Based upon these plots compared to the closest upstream location, the wake effects are less pronounced further downstream where the flow can coalesce, recover, and form a flow more similar to that prior to the obstruction. The calculated drag force and drag coefficient are described in the next subsection.

### 3.4. Drag Measurements

To calculate the drag force given pressure data, a drag force integrand was calculated in MATLAB and used in the trapezoidal numerical integration function. This method examines each step  $i$  and calculates the area between the two points as area under the curve to incrementally sum all areas and determine the total drag force at each probe location through the cylinder wake. Thereafter, the corresponding drag coefficient was calculated based upon the freestream speed (dynamic pressure) and

drag force. These plots of drag vs Reynolds number are shown in Figures 8, 13, and 18. In each for a constant 140 or 340 RPM, the drag is directly proportional to distance downstream of the cylinder. For the nearest 18.4cm downstream distance, the drag at 340 RPM was determined to be 3.2N, then 3N, and finally 2.45N for the respective downstream locations. This shows the drag in the wake decreases the further from the cylinder the probe is located.

This observation can be extended to the drag coefficient. According to Tritton [3], the drag coefficient of a cylinder should generally decrease with increase Reynolds number. This is supported by the data obtained in this laboratory in Figures 9, 14, and 19. Figure 9 shows a decrease in  $C_D$  for an increase in Reynolds number. Figures 19 also exhibits such a decrease in  $C_D$  as well, although Figure 14 maintains a nearly constant drag coefficient. This is likely due to the close proximity to the cylinder trailing edge.

The experimental data appears to fit the published data reasonably well, although the data obtained in this laboratory covers a small range of Reynolds numbers and a direct validation is difficult to establish. A more robust study would include the very low and high extremes of Reynolds numbers.

### 3.5. Limitations

The primary assumption made in this study is that airflow is incompressible throughout all parts of the tunnel and therefore constant density during the tests. It was also assumed that air temperature outside the tunnel was identical to the air temperature inside being used during tests. The refrigerant system was also not enabled, so constant temperature throughout the lab experiment was also used.

A limitation was the inability to map velocities nearest the tunnel walls. The traverse had built-in displacement limits that prevented moving the probe within several centimeters of the walls. For this study, the flow nearest the walls was not as great of an interest as with the previous laboratory where boundary layer effects due to the tunnel walls were of interest.

The largest limitation however was the small number of observable Reynolds numbers in the tunnel. Reynolds numbers below 1000 and above  $10^5$  would allow for better validation of experimental data with published figures.

## 4. CONCLUSIONS

## REFERENCES

- [1] Patel, Havya. "Oklahoma State University Endeavor Lab Wind Tunnel Operations Manual." *Aerolab LLC*. June 13, 2018.
- [2] Santhanakrishnan, Arvind. "Lab 2 MATLAB Script." Oklahoma State University. October 6, 2019.
- [3] Tritton, D.J. *Physical Fluid Dynamics*. 2<sup>nd</sup> Edition. Oxford Science Publications. Clarendon Press. 1988. ISBN 978-0198544937.



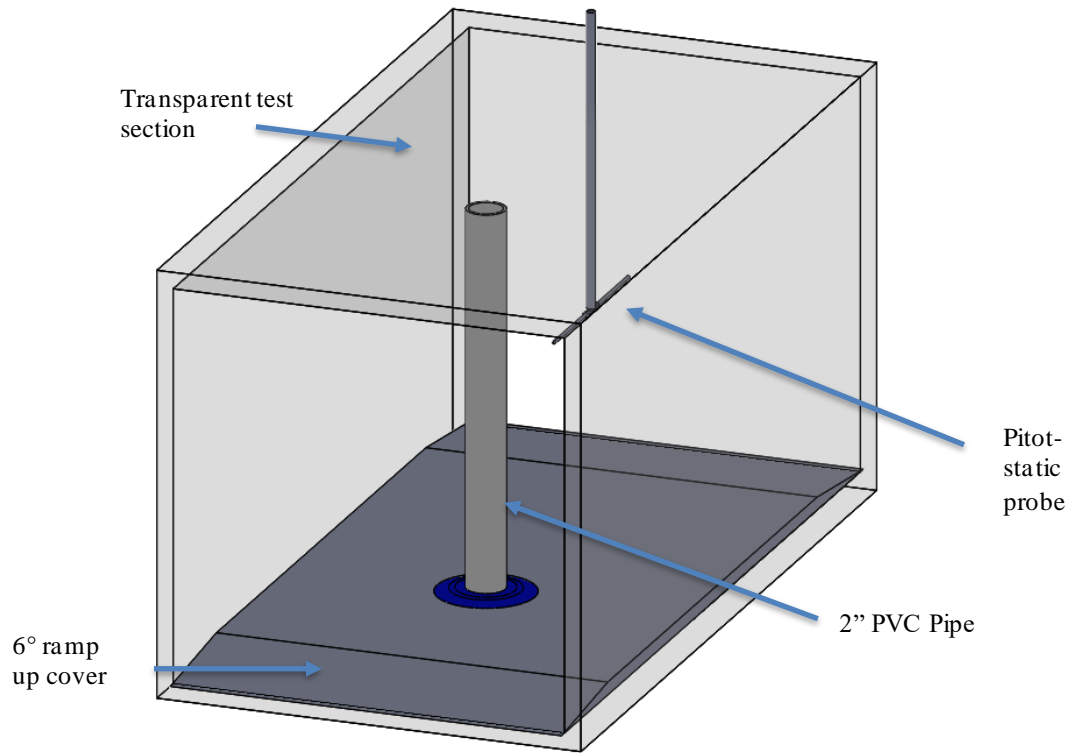


**TABLES**

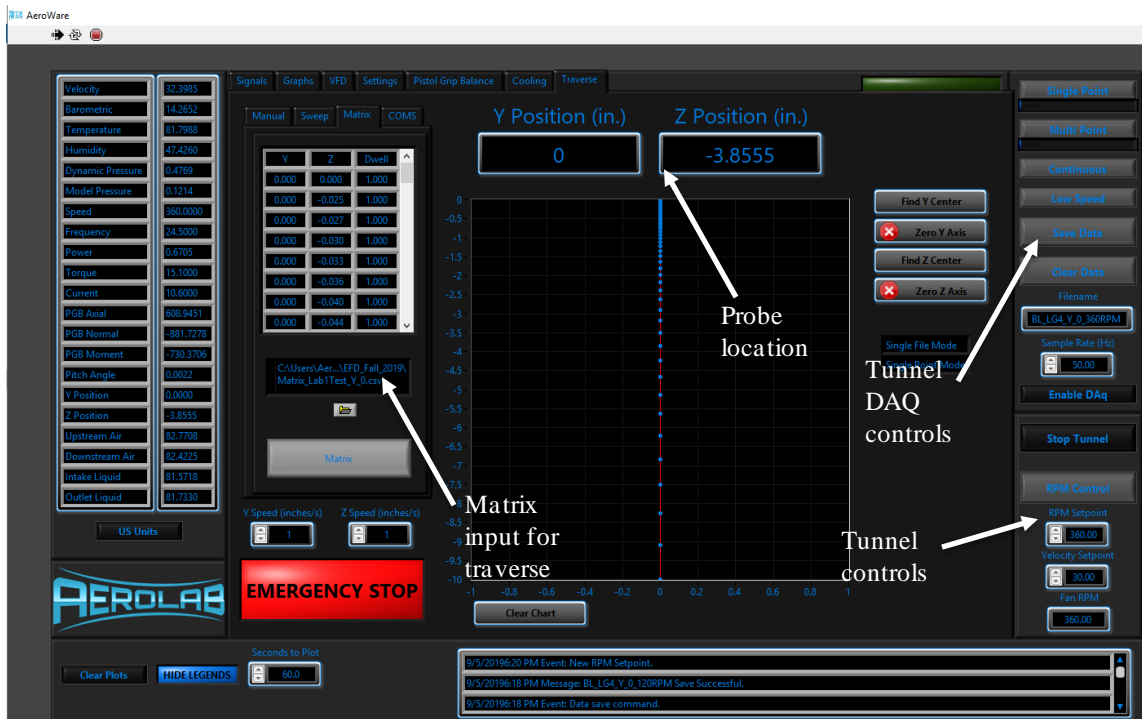
<b>Configuration #</b>	<b>Fan Speed</b>	<b>Probe <math>x</math> location</b>
1	40	22.9 cm
2	140	22.9 cm
3	240	22.9 cm
4	340	22.9 cm
5	440	22.9 cm
6	540	22.9 cm
7	640	22.9 cm
8	740	22.9 cm
9	140	18.4 cm
10	340	36.8 cm
11	140	36.8 cm
12	340	18.4 cm

**Table 1:** Configurations of Fan Speed and Probe Location Behind Wake in  $x$ -Direction.

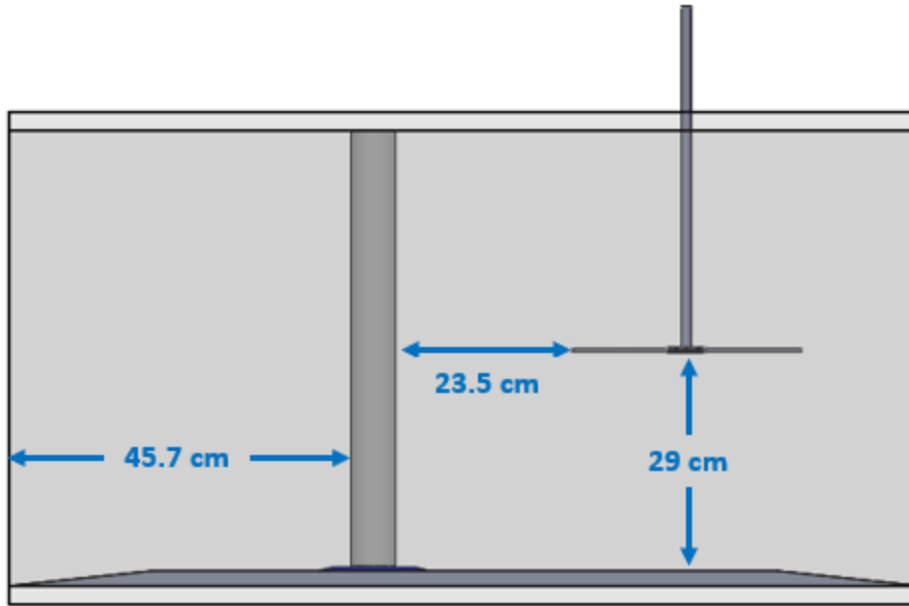
**FIGURES**



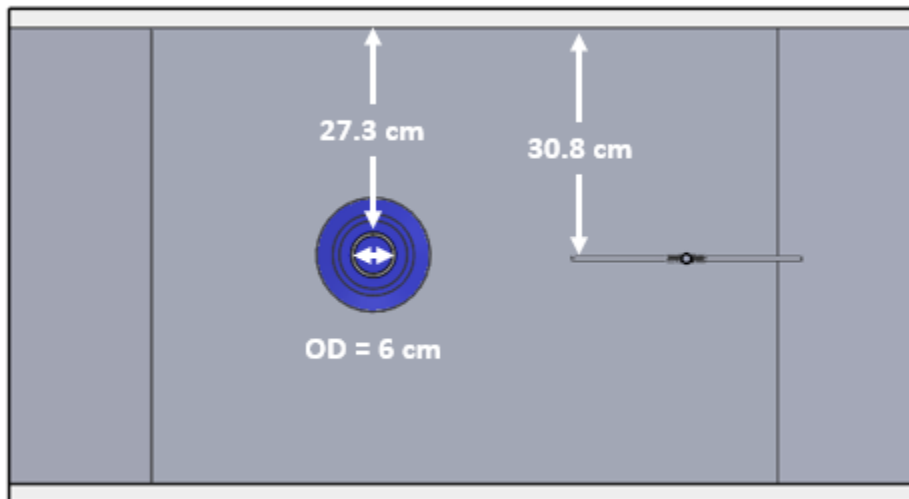
**Figure 1: Wind Tunnel Assembly for Lab 2**



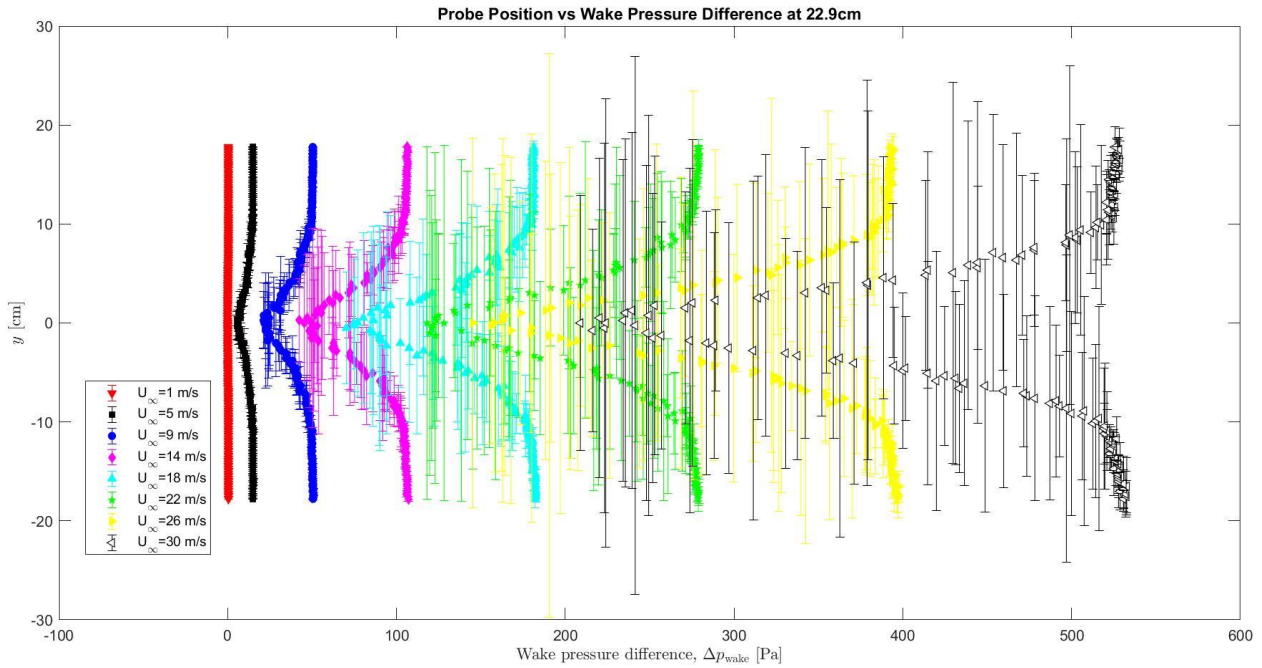
**Figure 2: Screenshot of the Aerolab Wind Tunnel VI, with Buttons Labeled.**



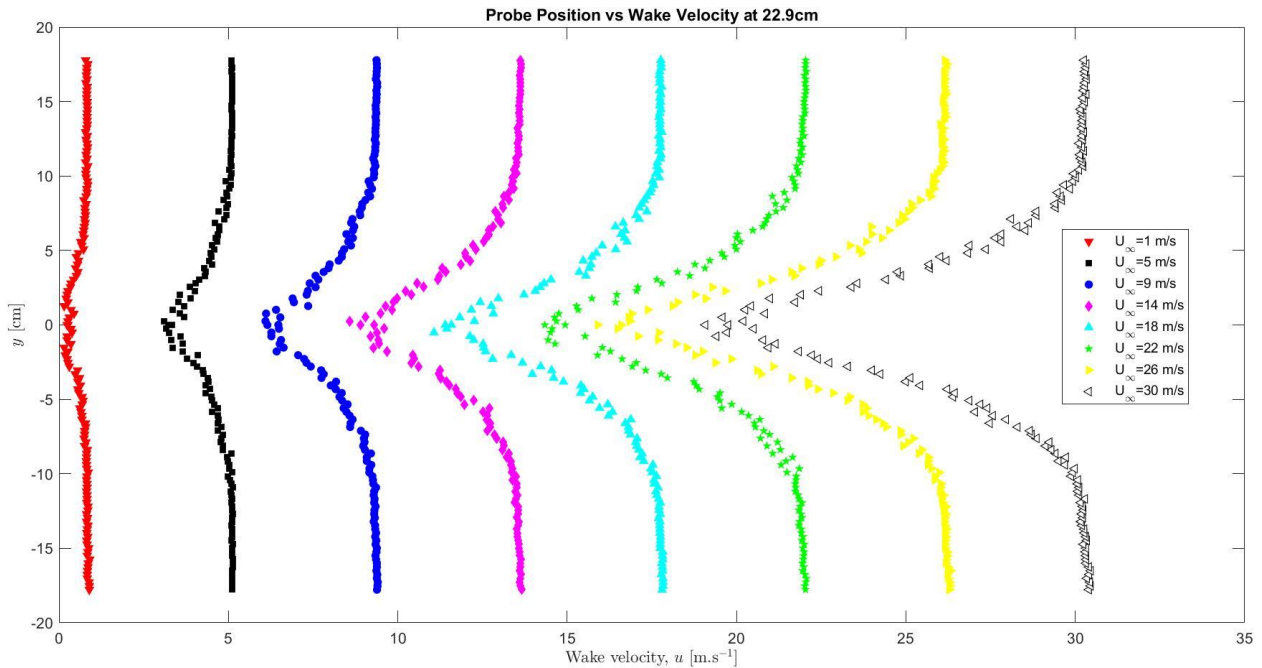
**Figure 3:** Test Section Side View Schematic of Initial Probe Location.



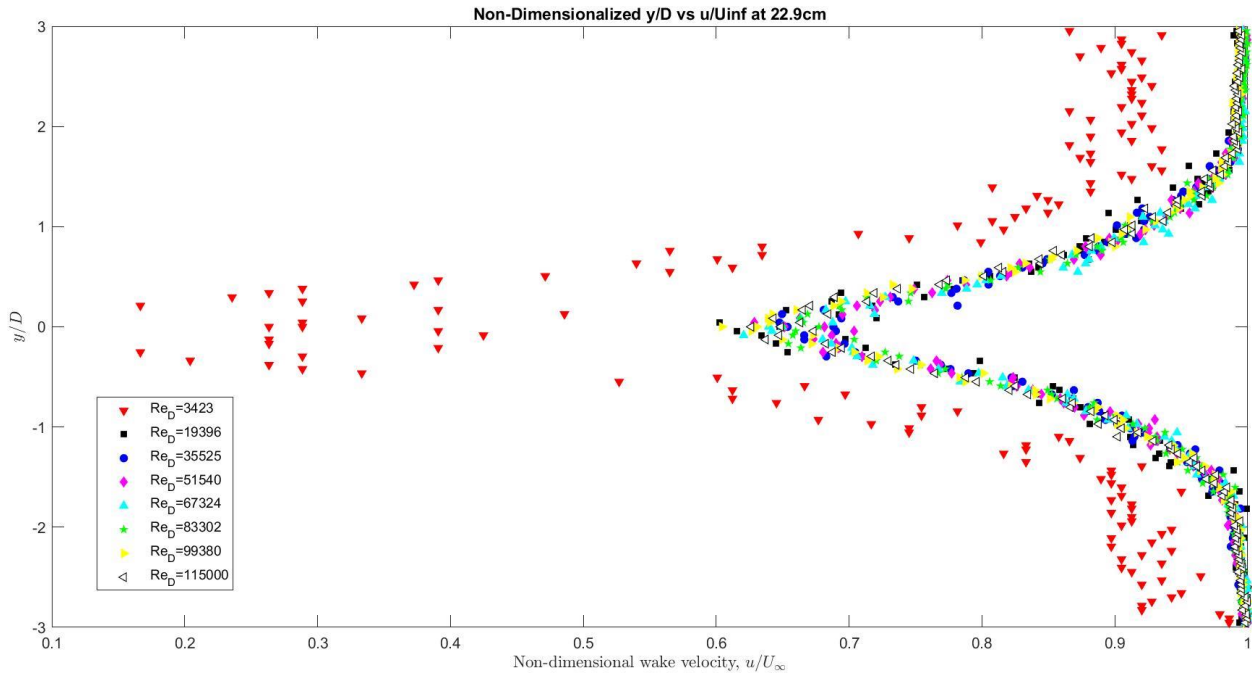
**Figure 4:** Test Section Top View Schematic of Initial Probe Location.



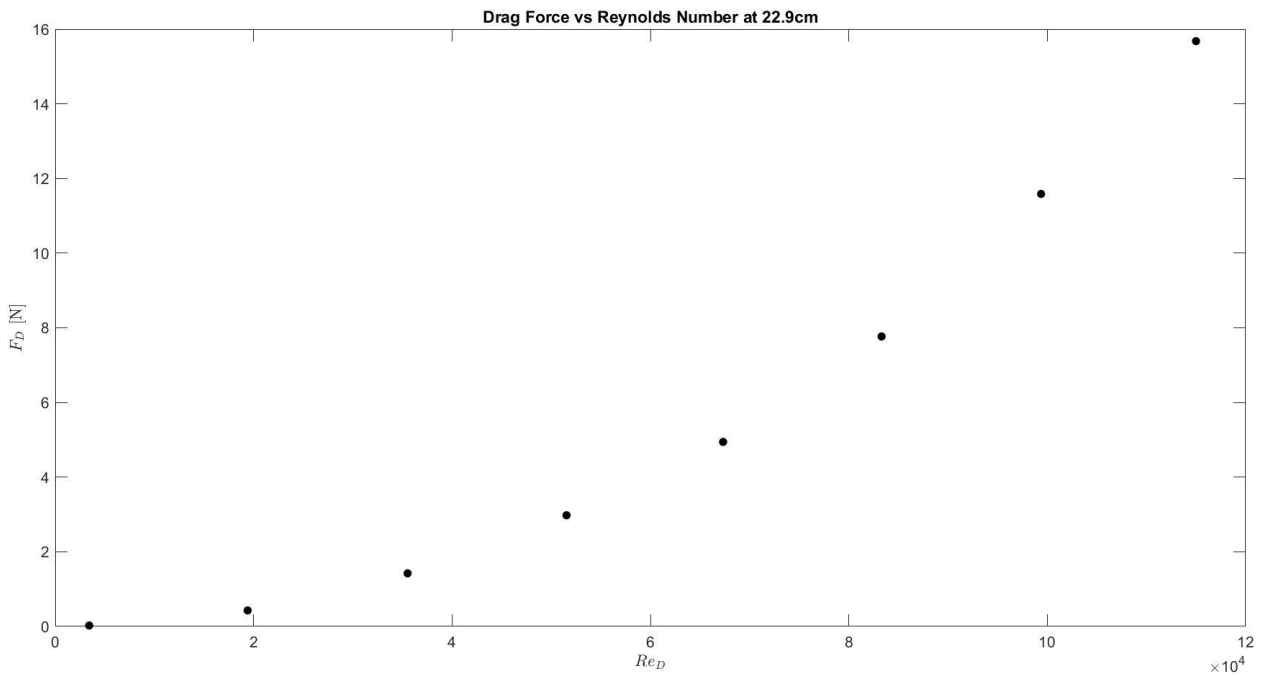
**Figure 5:** Probe location at 22.9cm behind the cylinder indicating increased pressure differential for higher freestream velocities. Overall error variation also increases at higher velocity.



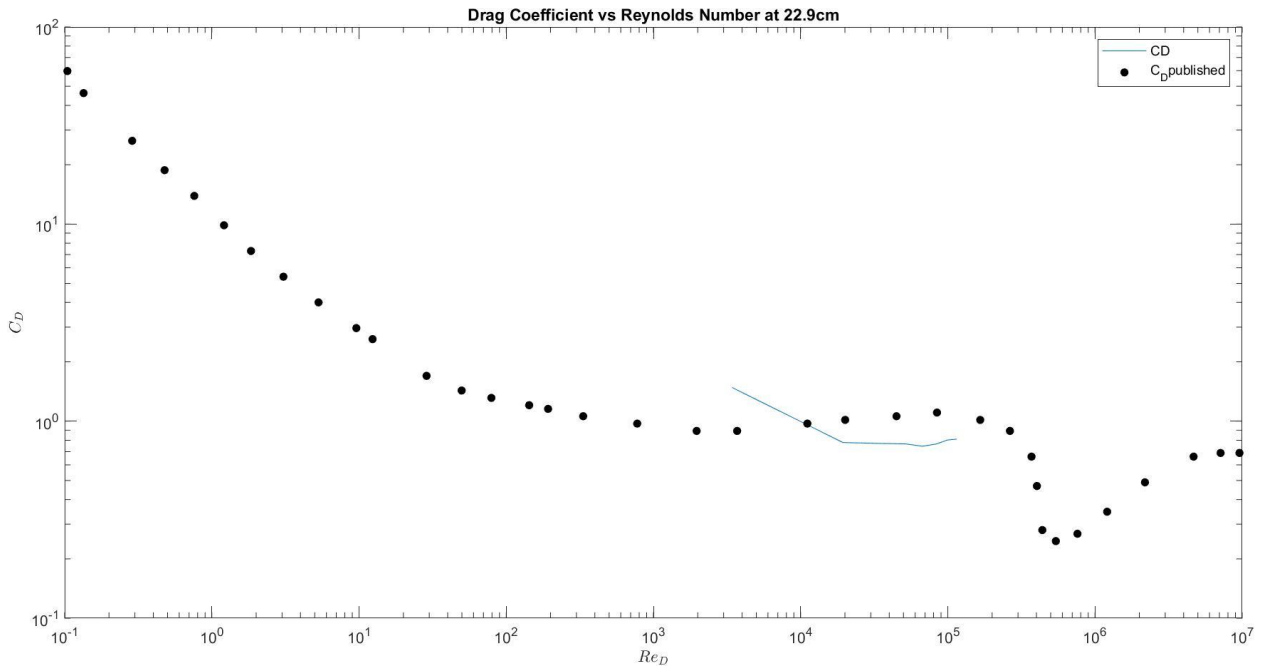
**Figure 6:** Probe location at 22.9cm behind the cylinder indicating increased wake velocity differential for higher freestream velocities. The reduced velocity is most pronounced behind the cylinder at the center of the tunnel.



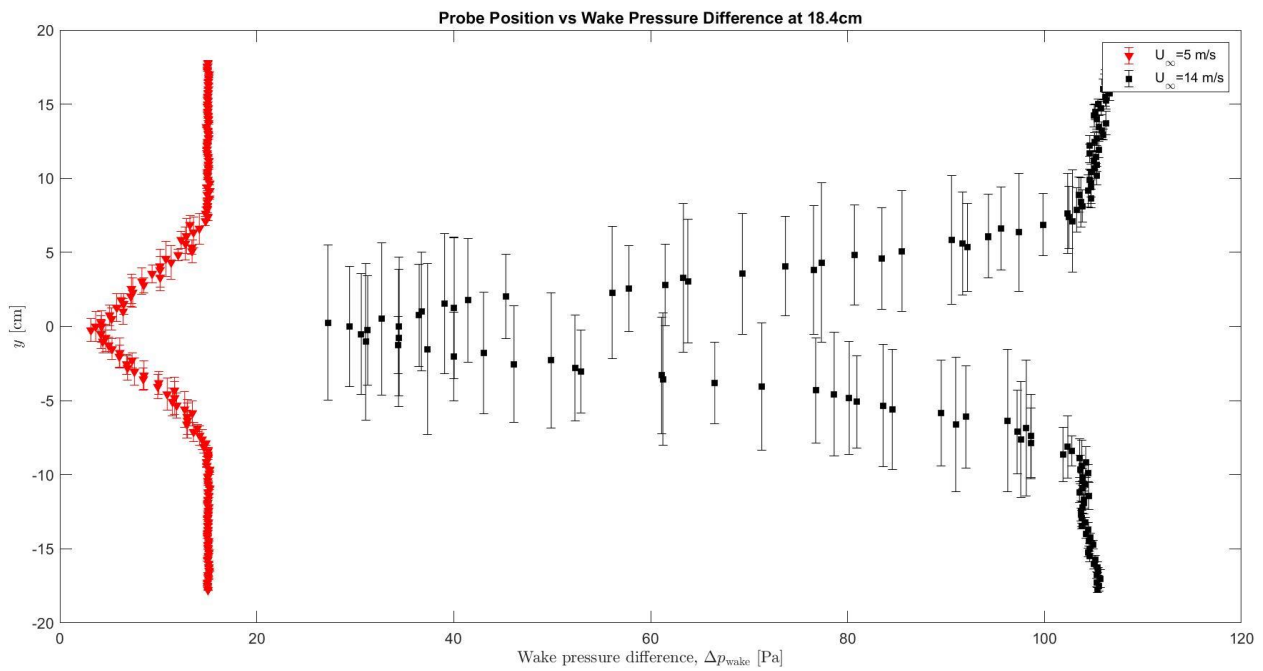
**Figure 7:** Probe location at 22.9cm behind the cylinder of non-dimensionalized probe position and wake velocity. At the lowest Reynolds number <5000, the cylinder has the greatest influence on the freestream speed as function of tunnel speed.



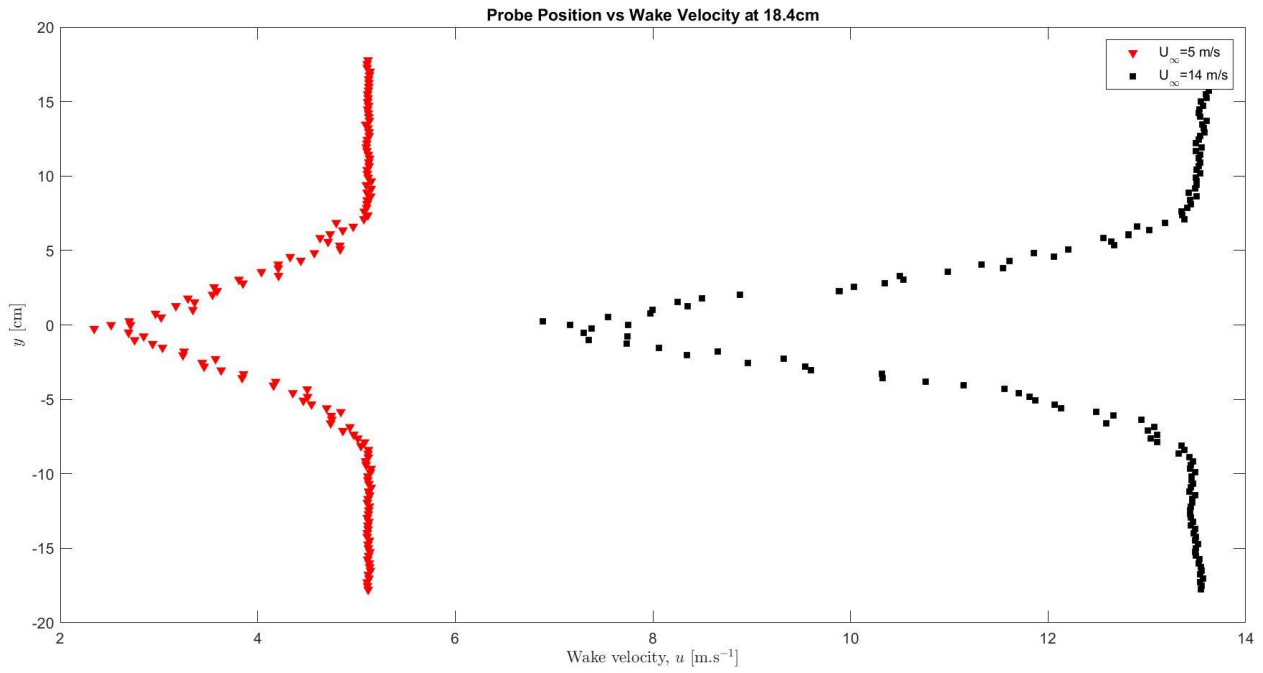
**Figure 8:** Probe location at 22.9cm behind the cylinder plotting drag force as a function of Reynolds number. The drag force experienced by the cylinder increases exponentially with increasing Reynolds number.



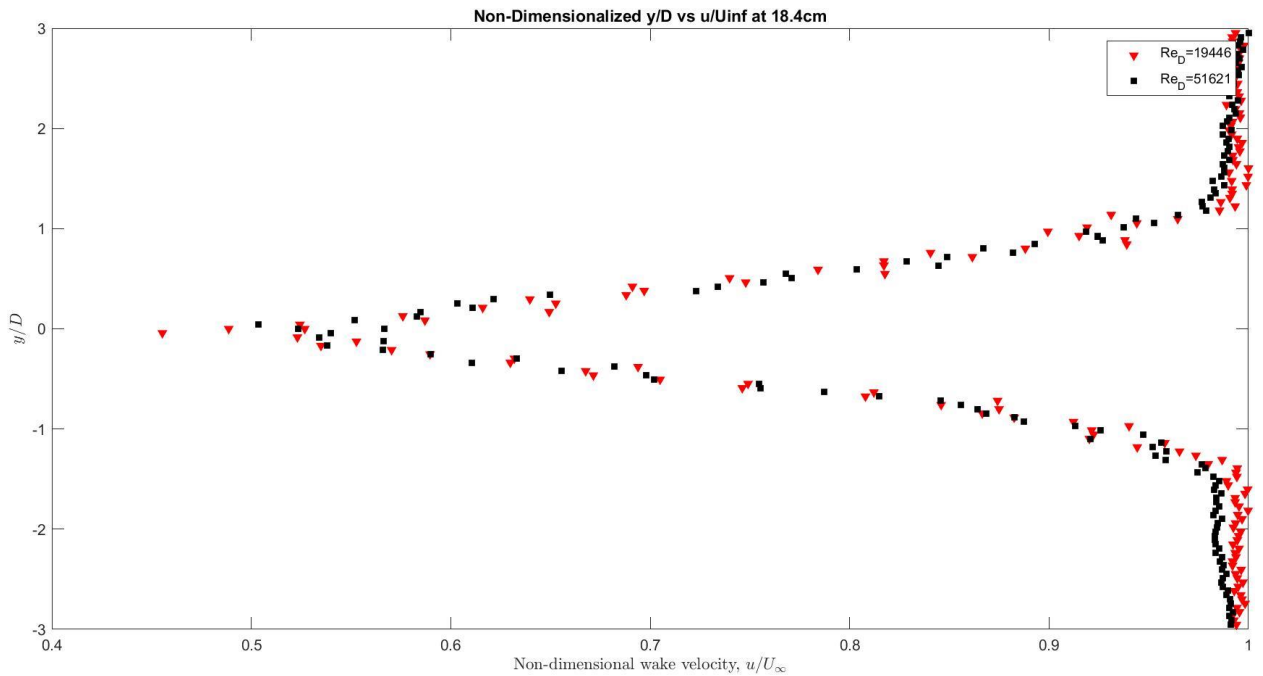
**Figure 9:** Probe location at 22.9cm behind the cylinder plotting drag coefficient as a function of Reynolds number. The black points are book-published values, while the blue line indicates the experimentally-obtained data from this lab. The data gathered covers a limited range of Reynolds numbers, but the range that does fit appears to fit published data reasonably well.



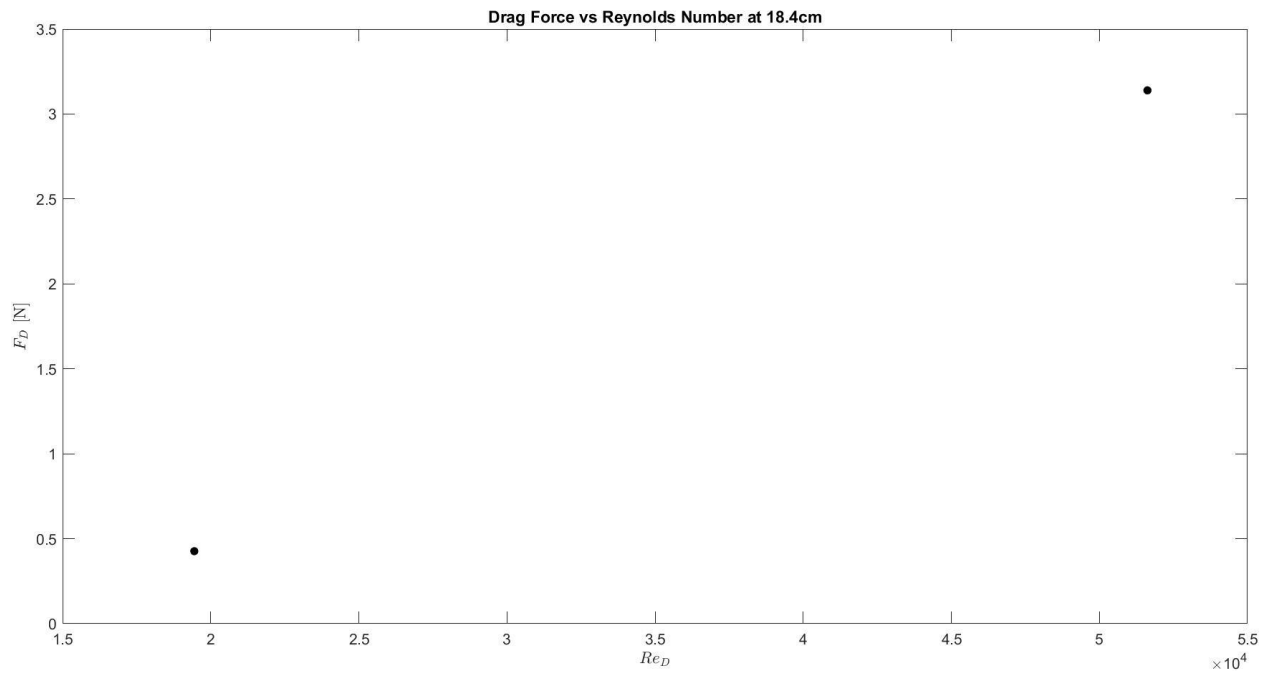
**Figure 10:** Probe location at 18.4cm behind the cylinder increased pressure differential for higher freestream velocities. Overall error variation also increases at higher velocity.



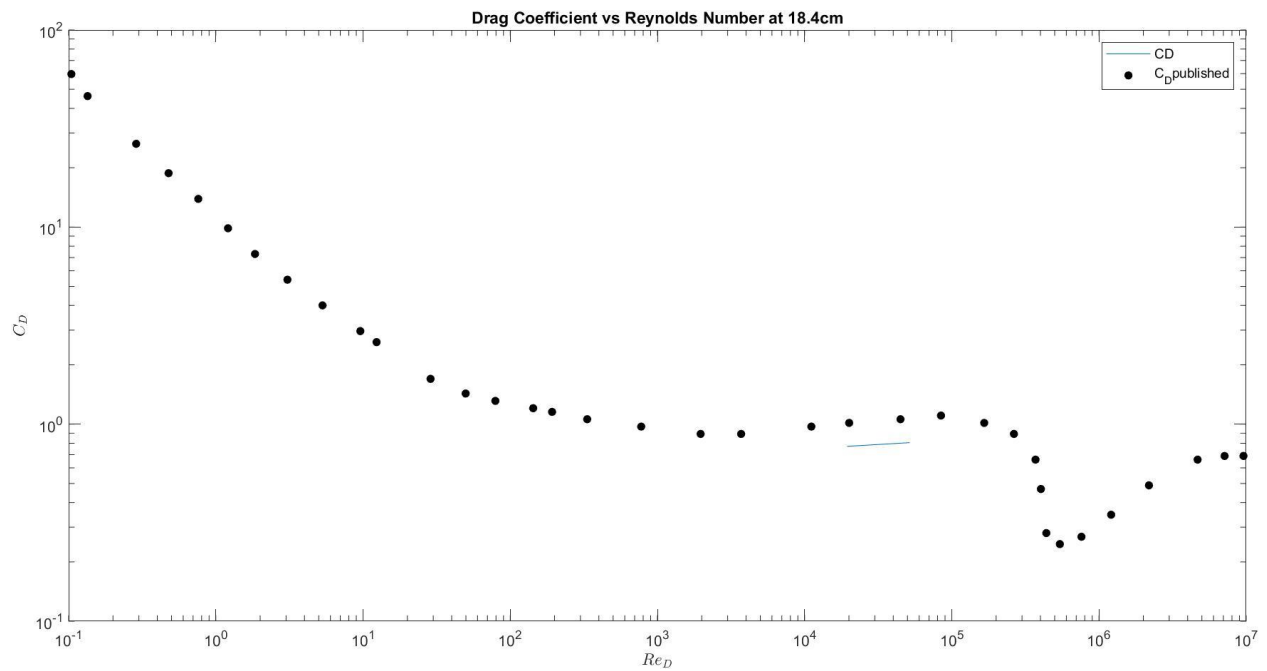
**Figure 11:** Probe location at 18.4cm behind the cylinder indicating increased wake velocity differential for higher freestream velocities. The reduced velocity is most pronounced behind the cylinder at the center of the tunnel.



**Figure 12:** Probe location at 18.44cm behind the cylinder of non-dimensionalized probe position and wake velocity. For the two Reynolds numbers tested, the cylinder affects both by slowing the flow down immediately behind the cylinder.

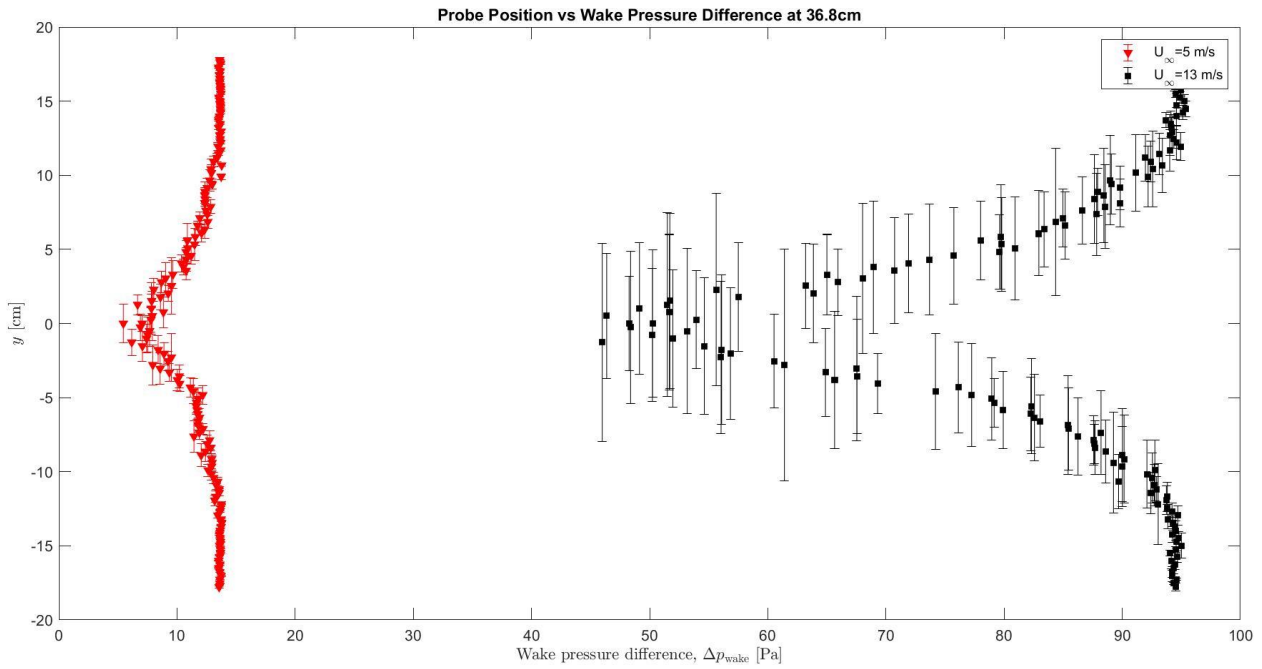


**Figure 13:** Probe location at 18.4cm behind the cylinder plotting drag force as a function of Reynolds number. The drag force experienced by the cylinder increases with increasing Reynolds number.

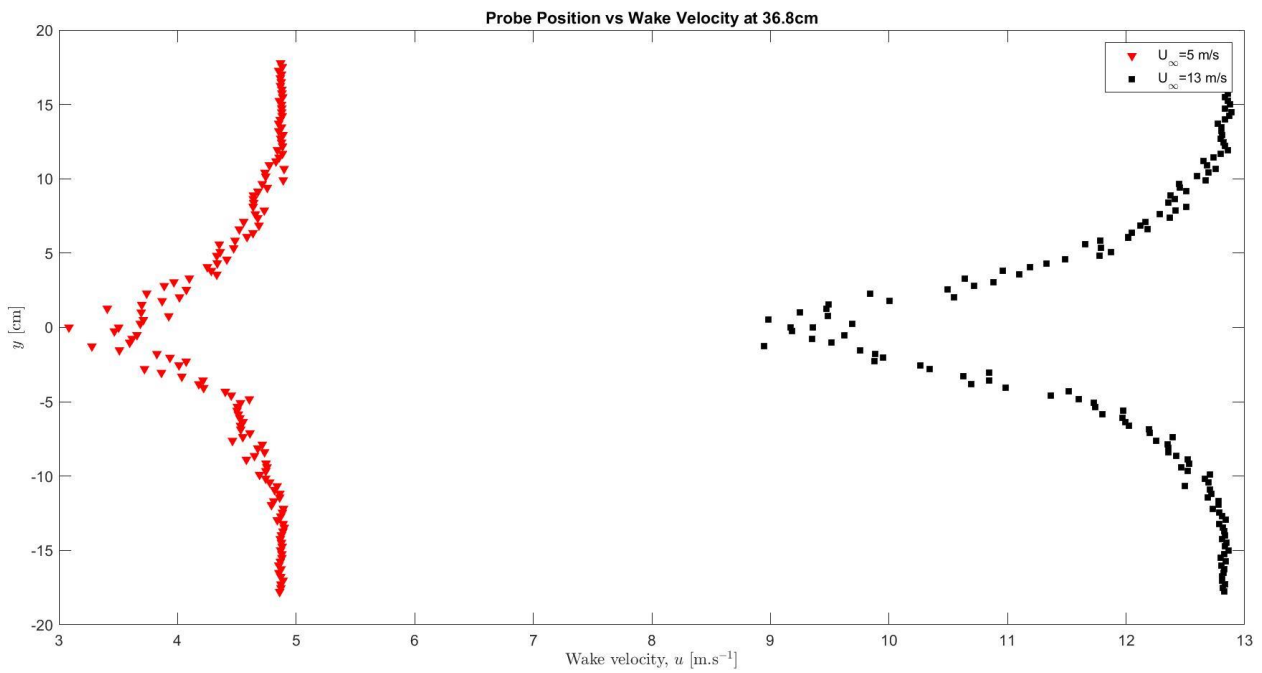


**Figure 14:** Probe location at 18.4cm behind the cylinder plotting drag coefficient as a function of Reynolds number. The black points are book-published values, while the blue line indicates the experimentally-obtained data from this lab. The data gathered covers a limited range of Reynolds numbers, but the range that does fit appears to fit published data reasonably well for being closer to the cylinder than at 22.9cm.

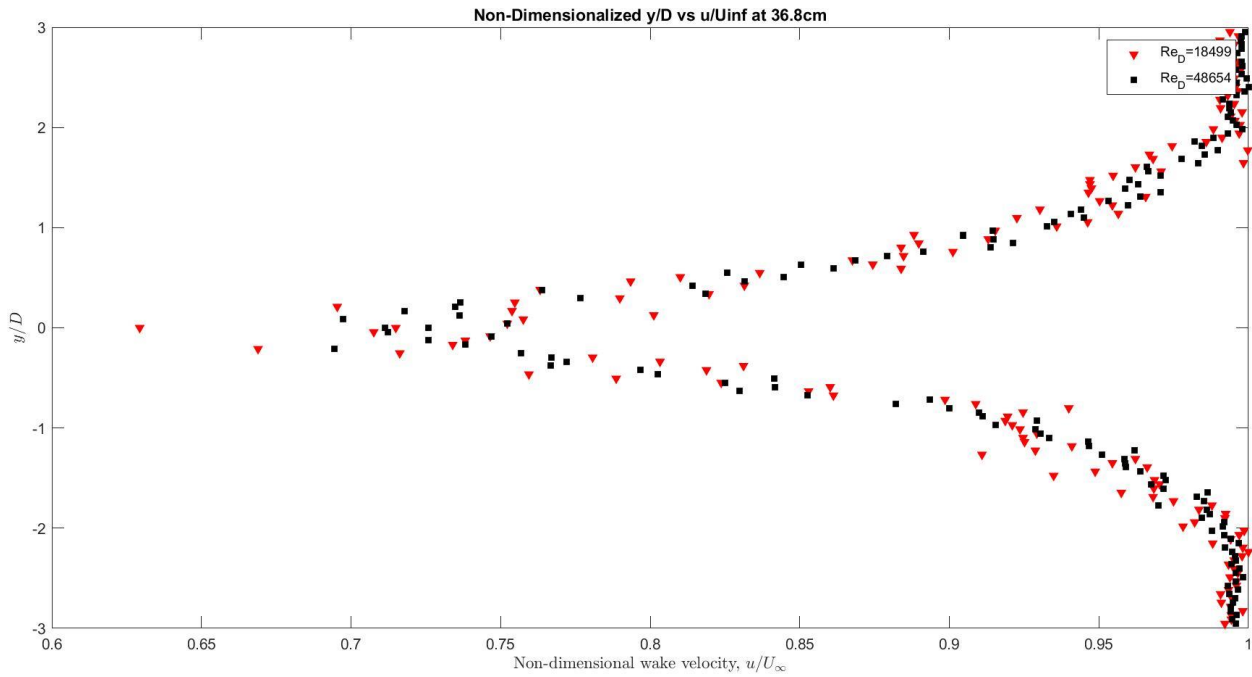




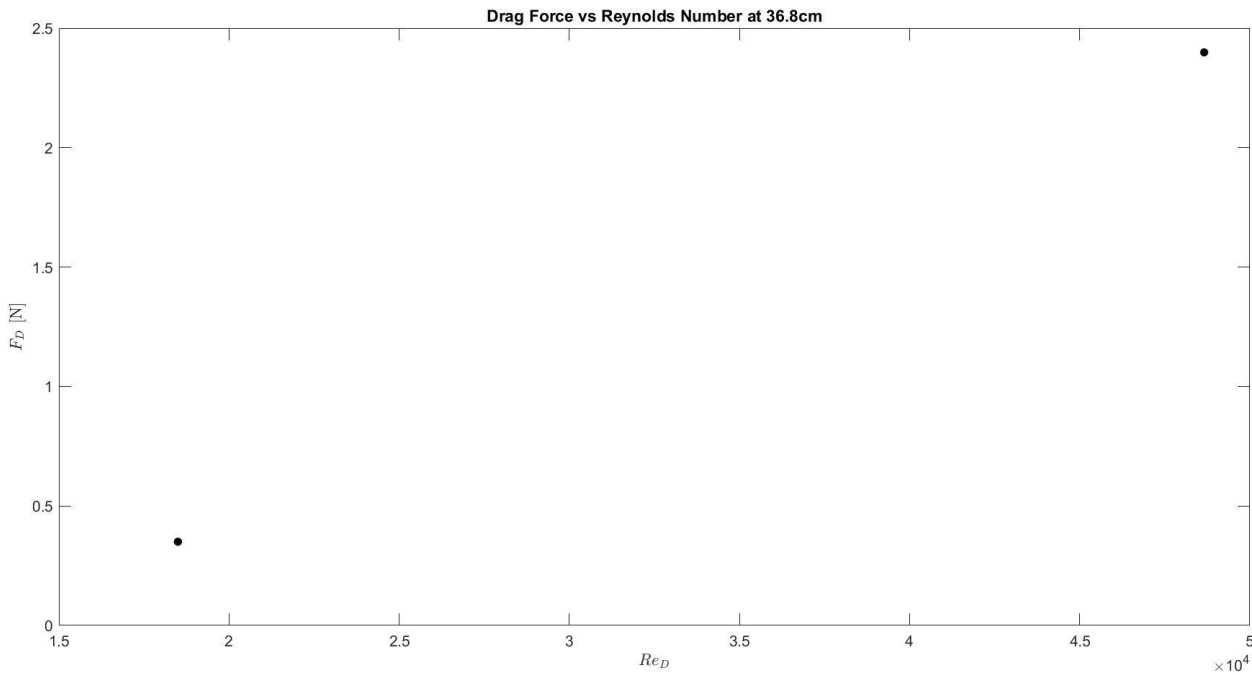
**Figure 15:** Probe location at 36.8cm behind the cylinder increased pressure differential for higher freestream velocities. Overall error variation also increases at higher velocity.



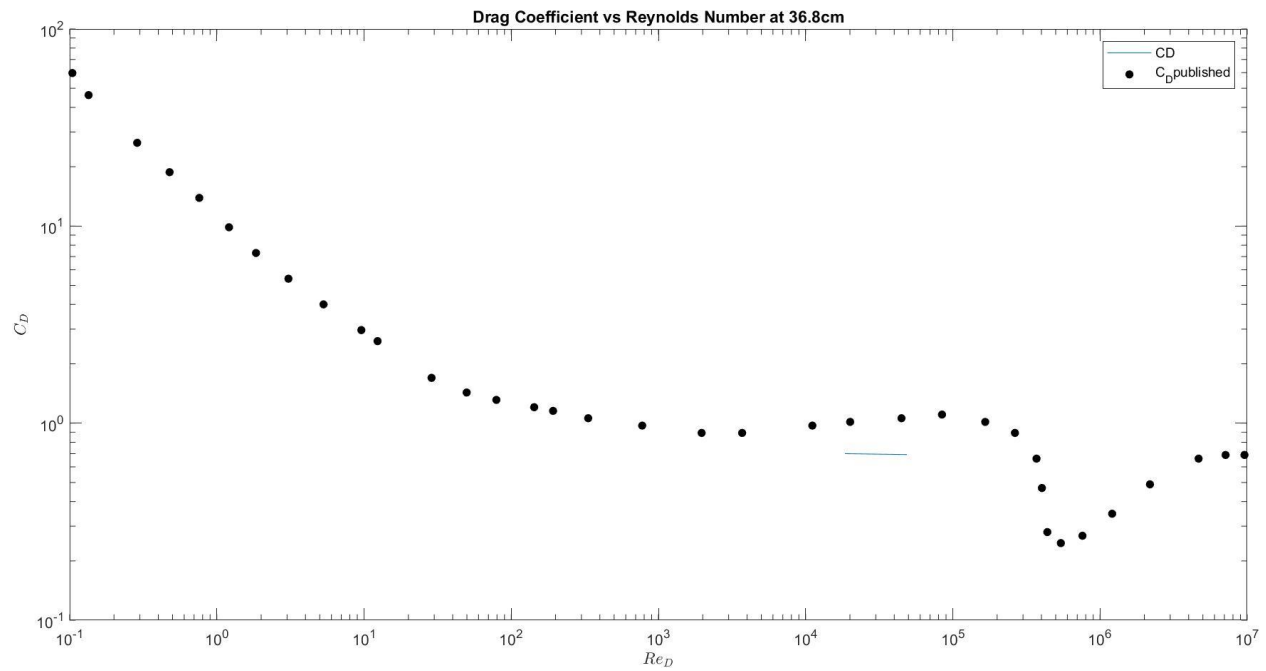
**Figure 16:** Probe location at 36.8cm behind the cylinder indicating increased wake velocity differential for higher freestream velocities. The reduced velocity is most pronounced behind the cylinder at the center of the tunnel.



**Figure 17:** Probe location at 36.8cm behind the cylinder of non-dimensionalized probe position and wake velocity. For the two Reynolds numbers tested, the cylinder affects both by slowing the flow down immediately behind the cylinder.



**Figure 18:** Probe location at 36.8cm behind the cylinder plotting drag force as a function of Reynolds number. The drag force experienced by the cylinder increases with increasing Reynolds number.



**Figure 19:** Probe location at 36.8cm behind the cylinder plotting drag coefficient as a function of Reynolds number. The black points are book-published values, while the blue line indicates the experimentally-obtained data from this lab. These experimental points are farther from the published values than the data for the probe location closer to the cylinder wake.

**APPENDIX****Plots at Probe Location 22.9cm.**

%% MAE 4273 Fall 2019 Lab 2

% Aerolab wind tunnel wake survey CSV file import and drag calculation

% Dr. Arvind Santhanakrishnan, Oct. 6, 2019

% READ BEFORE USING: constants, calibration equations are \*roughly-guessed\*

% User-inputs will need to be changed for your specific test conditions

close all; clear all; clc;

%% Define constants &amp; test conditions

Patm=14.15; % atm. pressure in psi

Tatm\_F=73; % atm. temp. in F

R=287.058; % gas constant in J.kg<sup>-1</sup>.K<sup>-1</sup>

mu=1.831e-5; % dyn. visc. in Pa.s, lookup for correct Tatm value!

D=0.060198; % outer diameter of cylinder in meters

L=0.60325; % length of cylinder in meters

RPM=[140 340]; % # wind tunnel RPMs tested, CHANGE based on your RPM values

%% Define folder path where CSV files are stored (note: MAC OS uses '/' whereas Windows OS uses '\\')

path='C:\Users\lucas\OneDrive\College\MAE 4273\Lab 2\Data\Raw Data\Renamed Raw Data\7in';

cd(path)

Re_exp=[0.104315447	0.134412719	0.287551473	0.477418323	0.759860633	1.209396778
1.845249286	3.06364565	5.306041498	9.58630795	12.35216599	28.75514728
49.80210578	79.26520165	143.2066887	192.4880043	333.3771118	776.0831546
1965.974958	3705.163179	11114.02987	20079.47223	44810.12411	84451.13769
166028.8219	264252.04	370516.3179	403185.205	438734.5487	541932.1973
759860.6328	1209396.778	2184990.441	4674388.132	7131994.657	9586307.95];
C_Dexp=[59.75820111	46.19513847	26.44601552	18.76255272	13.89495494	9.858000137
7.300524071	5.406537936	4.003911523	2.965170628	2.607048246	1.697515172
1.429813862	1.312237433	1.204329547	1.153750232	1.058875063	0.971801667
0.891888489	0.891888489	0.971801667	1.01440453	1.058875063	1.105295141
1.01440453	0.891888489	0.660504493	0.468605578	0.280030263	0.24620924
0.26826958	0.347034515	0.489148802	0.660504493	0.689460384	0.689460384];

%% Define sampling characteristics used for data acquisition

sf=100; % #samples per sec

st=1; % #sec of data acquisition per location

ns=sf\*st; % #samples per location

nloc=142; % #y-locations sampled

%% Define calibration equation terms

deltaP\_corrected\_slope=0.9496; % slope of calibration eq'n for delta P

deltaP\_corrected\_intercept=0; % intercept of calibration eq'n for delta P

Uinf\_RPM\_slope=0.0186; % slope of calibration eq'n for Uinf [m/s] v/s RPM

Uinf\_RPM\_intercept=0; % intercept of calibration eq'n for Uinf [m/s] v/s RPM

% Uinf\_RPM\_slope=0.0373; % slope of calibration eq'n for Uinf [m/s] v/s RPM

% Uinf\_RPM\_intercept=-0.6343; % intercept of calibration eq'n for Uinf [m/s] v/s RPM

```

%% Define unit conversion factors
inchtocmconv=2.54; % 1 in to cm conv.
psitopaconv=6894.75729; % 1 psi to Pa conv.
inh20topaconv=1/0.0040146; % 1 in H2O to Pa conv.
Tatm_K=(Tatm_F-32)*5/9 + 273.15; % F to K conv.

%% Calculate air density using ideal gas equation
rho=(Patm*psitopaconv)/(R*Tatm_K); % air density in kg.m^-3

for i=1:length(RPM)
% for i=1:4
  %% Initialize variables.
  filename = strcat(num2str(RPM(i)), 'rpm.csv');
  data = csvread(filename,2,3);

  %% Assign columns to variables
  deltap=data(:,6); % model pressure
  yloc=data(:,16); % y-location of probe

  %% Reshape y-location and model pressure arrays
  yloc_cols=reshape(yloc(1:ns*nloc),[sf*st,nloc]);
  deltap_cols=reshape(deltap(1:ns*nloc),[sf*st,nloc]);

  %% Calculated calibration eq'n based delta P
  deltaP_cal=deltaP_corrected_slope*deltap_cols+deltaP_corrected_intercept;

  %% Calculate mean and standard deviations
  avg_yloc_cols(1,:)=mean(yloc_cols,1)*inchtocmconv;
  % sd_yloc_cols(1,:)=std(yloc_cols,1)*inchtocmconv;
  % avg_deltap_cols(1,:)=mean(deltap_cols,1)*inh20topaconv;
  % sd_deltap_cols(1,:)=std(deltap_cols,1)*inh20topaconv;
  avg_deltaP_cal(1,:)=mean(deltaP_cal,1)*inh20topaconv;
  sd_deltaP_cal(1,:)=std(deltaP_cal,1)*inh20topaconv;
  u=sqrt(abs(2*avg_deltaP_cal/rho));
  Uinf(i)=max(u);
  % Uinf2(i)=Uinf_RPM_slope*RPM(i)+Uinf_RPM_intercept;

  %% Calculate Reynolds number
  Re(i)=rho*Uinf(i)*D/mu;

  %% Calculate drag force and drag coefficient
  drag_integrand(1,:)=rho*L*(u.*(Uinf(i)-u));
  avg_yloc_cols_mod=fliplr(avg_yloc_cols-min(avg_yloc_cols))*1e-2;
  FD(i)=abs(trapz(avg_yloc_cols_mod',drag_integrand(1,:)));
  CD(i)=FD(i)/(0.5*rho*(Uinf(i))^2*D*L);

  %% Plotting
  if i==1 str = 'rv'; end
  if i==2 str = 'ks'; end
  if i==3 str = 'bo'; end
  if i==4 str = 'md'; end

```

```

if i==5 str = 'c^'; end
if i==6 str = 'gp'; end
if i==7 str = 'y>'; end
if i==8 str = 'k<'; end
if i==9 str = 'kh'; end
str2=['r';'k';'b';'m';'c';'g';'y';'w';'w'];

figure(1), hold on, box on
errorbar(avg_deltaP_cal,avg_yloc_cols,sd_deltaP_cal,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Wake pressure difference,  $\Delta p_{\text{wake}}$  [Pa]', 'interpreter', 'latex');
ylabel('$y$ [cm]', 'interpreter', 'latex');
title('Probe Position vs Wake Pressure Difference at 18.4cm');
set(gca, 'FontSize', 10);

figure(2), hold on, box on
plot(u,avg_yloc_cols,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Wake velocity,  $u$  [m.s-1]', 'interpreter', 'latex');
ylabel('$y$ [cm]', 'interpreter', 'latex');
title('Probe Position vs Wake Velocity at 18.4cm');
set(gca, 'FontSize', 10);

figure(3), hold on, box on
plot(u/Uinf(i),avg_yloc_cols*1e-2/D,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Non-dimensional wake velocity,  $u/U_{\infty}$ ', 'interpreter', 'latex');
ylabel('$y/D$', 'interpreter', 'latex');
title('Non-Dimensionalized y/D vs u/Uinf at 18.4cm')

set(gca, 'FontSize', 10);
end

figure(4), hold on, box on
semilogx(Re,FD,'ko','markersize',5,'markerfacecolor','k')
xlabel('$Re_D$', 'interpreter', 'latex');
ylabel('$F_D$ [N]', 'interpreter', 'latex');
title('Drag Force vs Reynolds Number at 18.4cm');
set(gca, 'FontSize', 10);

figure(5), box on
% semilogx(Re,CD,'ko','markersize',5,'markerfacecolor','k')
loglog(Re,CD, Re_exp,C_Dexp,'ko','markersize',5,'markerfacecolor','k')
xlabel('$Re_D$', 'interpreter', 'latex');
ylabel('$C_D$', 'interpreter', 'latex');
title('Drag Coefficient vs Reynolds Number at 18.4cm')
legend('CD','C_Dpublished')
set(gca, 'FontSize', 10);

%% Insert legends
figure(1)
legend(strcat('U_{\infty}=',num2str(round(Uinf(1))),' m/s'),strcat('U_{\infty}=',num2str(round(Uinf(2))),' m/s'));

```

```
figure(2)  
legend(strcat('U_\infty=',num2str(round(Uinf(1))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(2))),'  
m/s'));
```

```
figure(3)  
legend(strcat('Re_D=',num2str(round(Re(1))),strcat('Re_D=',num2str(round(Re(2)))));
```

**Plots at Probe Location 18.4cm.**

%% MAE 4273 Fall 2019 Lab 2

% Aerolab wind tunnel wake survey CSV file import and drag calculation

% Dr. Arvind Santhanakrishnan, Oct. 6, 2019

% READ BEFORE USING: constants, calibration equations are \*roughly-guessed\*

% User-inputs will need to be changed for your specific test conditions

close all; clear all; clc;

%% Define constants &amp; test conditions

Patm=14.15; % atm. pressure in psi

Tatm\_F=73; % atm. temp. in F

R=287.058; % gas constant in J.kg<sup>-1</sup>.K<sup>-1</sup>

mu=1.831e-5; % dyn. visc. in Pa.s, lookup for correct Tatm value!

D=0.060198; % outer diameter of cylinder in meters

L=0.60325; % length of cylinder in meters

RPM=[40 140 240 340 440 540 640 740]; % # wind tunnel RPMs tested, CHANGE based on your RPM values

%% Define folder path where CSV files are stored (note: MAC OS uses '/' whereas Windows OS uses '\\')

path='C:\Users\lucas\OneDrive\College\MAE 4273\Lab 2\Data\Raw Data\Renamed Raw Data';

cd(path)

```
% Re_published=[1.04E-01 1.34E-01 2.88E-01 4.77E-01 7.60E-01 1.21E+00 1.85E+00 3.06E+00
5.31E+00 9.59E+00 1.24E+01 2.88E+01 4.98E+01 7.93E+01 1.43E+02 1.92E+02      3.33E+02
7.76E+02 1.97E+03 3.71E+03 1.11E+04 2.01E+04 4.48E+04 8.45E+04 1.66E+05 2.64E+05 3.71E+05
4.03E+05 4.39E+05 5.42E+05 7.60E+05 1.21E+06 2.18E+06 4.67E+06 7.13E+06 9.59E+06];
```

```
% C_Dpublished=[5.98E+01 4.62E+01 2.64E+01 1.88E+01 1.39E+01 9.86E+00 7.30E+00 5.41E+00
4.00E+00 2.97E+00 2.61E+00 1.70E+00 1.43E+00 1.31E+00 1.20E+00 1.15E+00 1.06E+00 9.72E-01
8.92E-01 8.92E-01 9.72E-01 1.01E+00 1.06E+00 1.11E+00 1.01E+00 8.92E-01 6.61E-01 4.69E-01
2.80E-01 2.46E-01 2.68E-01 3.47E-01 4.89E-01 6.61E-01 6.89E-01 6.89E-01];
```

```
Re_published=[0.104315447  0.134412719  0.287551473  0.477418323  0.759860633
1.209396778  1.845249286  3.06364565  5.306041498  9.58630795  12.35216599
28.75514728  49.80210578  79.26520165  143.2066887  192.4880043  333.3771118
776.0831546  1965.974958  3705.163179  11114.02987  20079.47223  44810.12411
84451.13769  166028.8219  264252.04  370516.3179  403185.205  438734.5487
541932.1973  759860.6328  1209396.778  2184990.441  4674388.132  7131994.657
9586307.95];
```

```
C_Dpublished=[59.75820111  46.19513847  26.44601552  18.76255272  13.89495494
9.858000137  7.300524071  5.406537936  4.003911523  2.965170628  2.607048246
1.697515172  1.429813862  1.312237433  1.204329547  1.153750232  1.058875063
0.971801667  0.891888489  0.891888489  0.971801667  1.01440453  1.058875063
1.105295141  1.01440453  0.891888489  0.660504493  0.468605578  0.280030263
0.24620924  0.26826958  0.347034515  0.489148802  0.660504493  0.689460384
0.689460384];
```

%% Define sampling characteristics used for data acquisition

sf=100; % #samples per sec

st=1; % #sec of data acquisition per location

ns=sf\*st; % #samples per location



```

nloc=142; % #y-locations sampled

%% Define calibration equation terms
deltaP_corrected_slope=0.9496; % slope of calibration eq'n for delta P
deltaP_corrected_intercept=0; % intercept of calibration eq'n for delta P
Uinf_RPM_slope=0.0186; % slope of calibration eq'n for Uinf [m/s] v/s RPM
Uinf_RPM_intercept=0; % intercept of calibration eq'n for Uinf [m/s] v/s RPM
% Uinf_RPM_slope=0.0373; % slope of calibration eq'n for Uinf [m/s] v/s RPM
% Uinf_RPM_intercept=-0.6343; % intercept of calibration eq'n for Uinf [m/s] v/s RPM

%% Define unit conversion factors
inchtocmconv=2.54; % 1 in to cm conv.
psitopaconv=6894.75729; % 1 psi to Pa conv.
inh20topaconv=1/0.0040146; % 1 in H2O to Pa conv.
Tatm_K=(Tatm_F-32)*5/9 + 273.15; % F to K conv.

%% Calculate air density using ideal gas equation
rho=(Patm*psitopaconv)/(R*Tatm_K); % air density in kg.m^-3

for i=1:length(RPM)
% for i=1:4
    %% Initialize variables.
    filename = strcat(num2str(RPM(i)), 'rpm.csv');
    data = csvread(filename,2,3);

    %% Assign columns to variables
    deltap=data(:,6); % model pressure
    yloc=data(:,16); % y-location of probe

    %% Reshape y-location and model pressure arrays
    yloc_cols=reshape(yloc(1:ns*nloc),[sf*st,nloc]);
    deltap_cols=reshape(deltap(1:ns*nloc),[sf*st,nloc]);

    %% Calculated calibration eq'n based delta P
    deltaP_cal=deltaP_corrected_slope*deltap_cols+deltaP_corrected_intercept;

    %% Calculate mean and standard deviations
    avg_yloc_cols(1,:)=mean(yloc_cols,1)*inchtocmconv;
    % sd_yloc_cols(1,:)=std(yloc_cols,1)*inchtocmconv;
    % avg_deltap_cols(1,:)=mean(deltap_cols,1)*inh20topaconv;
    % sd_deltap_cols(1,:)=std(deltap_cols,1)*inh20topaconv;
    avg_deltaP_cal(1,:)=mean(deltaP_cal,1)*inh20topaconv;
    sd_deltaP_cal(1,:)=std(deltaP_cal,1)*inh20topaconv;
    u=sqrt(abs(2*avg_deltaP_cal/rho));
    Uinf(i)=max(u);
    % Uinf2(i)=Uinf_RPM_slope*RPM(i)+Uinf_RPM_intercept;

    %% Calculate Reynolds number
    Re(i)=rho*Uinf(i)*D/mu;

    %% Calculate drag force and drag coefficient

```

```

drag_integrand(1,:)=rho*L*(u.*(Uinf(i)-u));
avg_yloc_cols_mod=flipr(avg_yloc_cols-min(avg_yloc_cols))*1e-2;
FD(i)=abs(trapz(avg_yloc_cols_mod,drag_integrand(1,:)));
CD(i)=FD(i)/(0.5*rho*(Uinf(i))^2*D*L);

%% Plotting
if i==1 str = 'rv'; end
if i==2 str = 'ks'; end
if i==3 str = 'bo'; end
if i==4 str = 'md'; end
if i==5 str = 'c^'; end
if i==6 str = 'gp'; end
if i==7 str = 'y>'; end
if i==8 str = 'k<'; end
if i==9 str = 'kh'; end
str2=['r';'k';'b';'m';'c';'g';'y';'w';'w'];

figure(1), hold on, box on
errorbar(avg_deltaP_cal,avg_yloc_cols,sd_deltaP_cal,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Wake pressure difference,  $\Delta p_{\text{wake}}$  [Pa]','interpreter','latex');
ylabel('$y$ [cm]','interpreter','latex');
title('Probe Position vs Wake Pressure Difference at 22.9cm');
set(gca, 'FontSize', 10);

figure(2), hold on, box on
plot(u,avg_yloc_cols,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Wake velocity,  $u$  [m.s-1'],'interpreter','latex');
ylabel('$y$ [cm]','interpreter','latex');
title('Probe Position vs Wake Velocity at 22.9cm');
set(gca, 'FontSize', 10);

figure(3), hold on, box on
plot(u/Uinf(i),avg_yloc_cols*1e-2/D,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Non-dimensional wake velocity,  $u/U_{\infty}$ ','interpreter','latex');
ylabel('$y/D$','interpreter','latex');
title('Non-Dimensionalized  $y/D$  vs  $u/U_{\infty}$  at 22.9cm');
set(gca, 'FontSize', 10);
end

figure(4), hold on, box on
semilogx(Re,FD,'ko','markersize',5,'markerfacecolor','k')
xlabel('$Re_D$','interpreter','latex');
ylabel('$F_D$ [N]','interpreter','latex');
title('Drag Force vs Reynolds Number at 22.9cm');
set(gca, 'FontSize', 10);

figure(5), box on
% semilogx(Re,CD,'ko','markersize',5,'markerfacecolor','k')
loglog(Re,CD, Re_published,C_Dpublished,'ko','markersize',5,'markerfacecolor','k')
xlabel('$Re_D$','interpreter','latex');
ylabel('$C_D$','interpreter','latex');

```

```

legend('CD','C_Dpublished')
title('Drag Coefficient vs Reynolds Number at 22.9cm')
set(gca, 'FontSize', 10);

%% % Insert legends
figure(1)
legend(strcat('U_\infty=',num2str(round(Uinf(1))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(2))),'
m/s'),strcat('U_\infty=',num2str(round(Uinf(3))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(4))),'
m/s'),strcat('U_\infty=',num2str(round(Uinf(5))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(6))),'
m/s'),strcat('U_\infty=',num2str(round(Uinf(7))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(8))),' m/s'));
legend('Location','best')

figure(2)
legend(strcat('U_\infty=',num2str(round(Uinf(1))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(2))),'
m/s'),strcat('U_\infty=',num2str(round(Uinf(3))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(4))),'
m/s'),strcat('U_\infty=',num2str(round(Uinf(5))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(6))),'
m/s'),strcat('U_\infty=',num2str(round(Uinf(7))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(8))),' m/s'));

figure(3)
legend(strcat('Re_D=',num2str(round(Re(1))))),strcat('Re_D=',num2str(round(Re(2))))),strcat('Re_D=',num
2str(round(Re(3))))),strcat('Re_D=',num2str(round(Re(4))))),strcat('Re_D=',num2str(round(Re(5))))),strcat('
Re_D=',num2str(round(Re(6))))),strcat('Re_D=',num2str(round(Re(7))))),strcat('Re_D=',num2str(round(Re
(8)))));

```

**Plots at Probe Location 36.8cm.**

```

%% MAE 4273 Fall 2019 Lab 2
% Aerolab wind tunnel wake survey CSV file import and drag calculation
% Dr. Arvind Santhanakrishnan, Oct. 6, 2019

% READ BEFORE USING: constants, calibration equations are *roughly-guessed*
% User-inputs will need to be changed for your specific test conditions

close all; clear all; clc;

%% Define constants & test conditions
Patm=14.15; % atm. pressure in psi
Tatm_F=73; % atm. temp. in F
R=287.058; % gas constant in J.kg^-1.K^-1
mu=1.831e-5; % dyn. visc. in Pa.s, lookup for correct Tatm value!
D=0.060198; % outer diameter of cylinder in meters
L=0.60325; % length of cylinder in meters
RPM=[140 340]; % # wind tunnel RPMs tested, CHANGE based on your RPM values

%% Define folder path where CSV files are stored (note: MAC OS uses '/' whereas Windows OS uses '\\')
path='C:\Users\lucas\OneDrive\College\MAE 4273\Lab 2\Data\Raw Data\Renamed Raw Data\14in';
cd(path)
Re_exp=[0.104315447 0.134412719 0.287551473 0.477418323 0.759860633 1.209396778
1.845249286 3.06364565 5.306041498 9.58630795 12.35216599 28.75514728
49.80210578 79.26520165 143.2066887 192.4880043 333.3771118 776.0831546
1965.974958 3705.163179 11114.02987 20079.47223 44810.12411 84451.13769
166028.8219 264252.04 370516.3179 403185.205 438734.5487 541932.1973
759860.6328 1209396.778 2184990.441 4674388.132 7131994.657 9586307.95];
C_Dexp=[59.75820111 46.19513847 26.44601552 18.76255272 13.89495494 9.858000137
7.300524071 5.406537936 4.003911523 2.965170628 2.607048246 1.697515172
1.429813862 1.312237433 1.204329547 1.153750232 1.058875063 0.971801667
0.891888489 0.891888489 0.971801667 1.01440453 1.058875063 1.105295141
1.01440453 0.891888489 0.660504493 0.468605578 0.280030263 0.24620924
0.26826958 0.347034515 0.489148802 0.660504493 0.689460384 0.689460384];

%% Define sampling characteristics used for data acquisition
sf=100; % #samples per sec
st=1; % #sec of data acquisition per location
ns=sf*st; % #samples per location
nloc=142; % #y-locations sampled

%% Define calibration equation terms
deltaP_corrected_slope=0.9496; % slope of calibration eq'n for delta P
deltaP_corrected_intercept=0; % intercept of calibration eq'n for delta P
Uinf_RPM_slope=0.0186; % slope of calibration eq'n for Uinf [m/s] v/s RPM
Uinf_RPM_intercept=0; % intercept of calibration eq'n for Uinf [m/s] v/s RPM
% Uinf_RPM_slope=0.0373; % slope of calibration eq'n for Uinf [m/s] v/s RPM
% Uinf_RPM_intercept=-0.6343; % intercept of calibration eq'n for Uinf [m/s] v/s RPM

%% Define unit conversion factors

```

```

inchtocmconv=2.54; % 1 in to cm conv.
psitopaconv=6894.75729; % 1 psi to Pa conv.
inh20topaconv=1/0.0040146; % 1 in H2O to Pa conv.
Tatm_K=(Tatm_F-32)*5/9 + 273.15; % F to K conv.

%% Calculate air density using ideal gas equation
rho=(Patm*psitopaconv)/(R*Tatm_K); % air density in kg.m^-3

for i=1:length(RPM)
% for i=1:4
    %% Initialize variables.
    filename = strcat(num2str(RPM(i)), 'rpm.csv');
    data = csvread(filename,2,3);

    %% Assign columns to variables
    deltap=data(:,6); % model pressure
    yloc=data(:,16); % y-location of probe

    %% Reshape y-location and model pressure arrays
    yloc_cols=reshape(yloc(1:ns*nloc),[sf*st,nloc]);
    deltap_cols=reshape(deltap(1:ns*nloc),[sf*st,nloc]);

    %% Calculated calibration eq'n based delta P
    deltaP_cal=deltaP_corrected_slope*deltap_cols+deltaP_corrected_intercept;

    %% Calculate mean and standard deviations
    avg_yloc_cols(1,:)=mean(yloc_cols,1)*inchtocmconv;
    % sd_yloc_cols(1,:)=std(yloc_cols,1)*inchtocmconv;
    % avg_deltap_cols(1,:)=mean(deltap_cols,1)*inh20topaconv;
    % sd_deltap_cols(1,:)=std(deltap_cols,1)*inh20topaconv;
    avg_deltaP_cal(1,:)=mean(deltaP_cal,1)*inh20topaconv;
    sd_deltaP_cal(1,:)=std(deltaP_cal,1)*inh20topaconv;
    u=sqrt(abs(2*avg_deltaP_cal/rho));
    Uinf(i)=max(u);
    % Uinf2(i)=Uinf_RPM_slope*RPM(i)+Uinf_RPM_intercept;

    %% Calculate Reynolds number
    Re(i)=rho*Uinf(i)*D/mu;

    %% Calculate drag force and drag coefficient
    drag_integrand(1,:)=rho*L*(u.*(Uinf(i)-u));
    avg_yloc_cols_mod=fliplr(avg_yloc_cols-min(avg_yloc_cols))*1e-2;
    FD(i)=abs(trapz(avg_yloc_cols_mod',drag_integrand(1,:)));
    CD(i)=FD(i)/(0.5*rho*(Uinf(i))^2*D*L);

    %% Plotting
    if i==1 str = 'rv'; end
    if i==2 str = 'ks'; end
    if i==3 str = 'bo'; end
    if i==4 str = 'md'; end
    if i==5 str = 'c^'; end

```

```

if i==6 str = 'gp'; end
if i==7 str = 'y>'; end
if i==8 str = 'k<'; end
if i==9 str = 'kh'; end
str2=['r';'k';'b';'m';'c';'g';'y';'w';'w'];

figure(1), hold on, box on
errorbar(avg_deltaP_cal,avg_yloc_cols,sd_deltaP_cal,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Wake pressure difference,  $\Delta p_{\text{wake}}$  [Pa]', 'interpreter','latex');
ylabel('$y$ [cm]', 'interpreter','latex');
title('Probe Position vs Wake Pressure Difference at 36.8cm');
set(gca, 'FontSize', 10);

figure(2), hold on, box on
plot(u,avg_yloc_cols,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Wake velocity,  $u$  [m.s-1]', 'interpreter','latex');
ylabel('$y$ [cm]', 'interpreter','latex');
title('Probe Position vs Wake Velocity at 36.8cm');
set(gca, 'FontSize', 10);

figure(3), hold on, box on
plot(u/Uinf(i),avg_yloc_cols*1e-2/D,str,'markersize',5,'markerfacecolor',str2(i))
xlabel('Non-dimensional wake velocity,  $u/U_{\infty}$ ', 'interpreter','latex');
ylabel('$y/D$', 'interpreter','latex');
set(gca, 'FontSize', 10);
title('Non-Dimensionalized y/D vs u/Uinf at 36.8cm')
end

figure(4), hold on, box on
semilogx(Re,FD,'ko','markersize',5,'markerfacecolor','k')
xlabel('$Re_D$', 'interpreter','latex');
ylabel('$F_D$ [N]', 'interpreter','latex');
title('Drag Force vs Reynolds Number at 36.8cm');
set(gca, 'FontSize', 10);

figure(5), box on
% semilogx(Re,CD,'ko','markersize',5,'markerfacecolor','k')
loglog(Re,CD, Re_exp,C_Dexp,'ko','markersize',5,'markerfacecolor','k')
xlabel('$Re_D$', 'interpreter','latex');
ylabel('$C_D$', 'interpreter','latex');
title('Drag Coefficient vs Reynolds Number at 36.8cm')
legend('CD','C_Dpublished')
set(gca, 'FontSize', 10);

%% Insert legends
figure(1)
legend(strcat('U_{\infty}=',num2str(round(Uinf(1))),' m/s'),strcat('U_{\infty}=',num2str(round(Uinf(2))),' m/s'));

figure(2)

```

```
legend(strcat('U_\infty=',num2str(round(Uinf(1))),' m/s'),strcat('U_\infty=',num2str(round(Uinf(2))),'  
m/s'));
```

```
figure(3)
```

```
legend(strcat('Re_D=',num2str(round(Re(1))),strcat('Re_D=',num2str(round(Re(2)))));
```

**Raw Data**

40 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_\infty$	STD $U_\infty$	Avg $U_\infty(U_\infty\max-U_\infty)$	STD $U_\infty(U_\infty\max-U_\infty)$
-7	0.483398	1.12E-16	0.917507	5.58E-16	0.011619	1.74E-17
-6.9	0.483398	1.12E-16	0.917507	5.58E-16	0.011619	1.74E-17
-6.8	0.476446	0.03744	0.910182	0.035953	0.016913	0.031787
-6.7	0.421079	0.03744	0.855484	0.038149	0.062452	0.029762
-6.6	0.421054	0.020886	0.856055	0.020587	0.063027	0.017222
-6.5	0.427981	0.027848	0.862883	0.027449	0.057315	0.022963
-6.4	0.441835	0.034106	0.876539	0.033619	0.045891	0.028124
-6.3	0.448762	0.03481	0.883367	0.034312	0.040179	0.028704
-6.2	0.497202	0.027748	0.93017	0.025455	-0.00064	0.024644
-6.1	0.421054	0.020886	0.856055	0.020587	0.063027	0.017222
-6	0.434908	0.031904	0.869711	0.031447	0.051603	0.026308
-5.9	0.462616	0.031904	0.897023	0.031447	0.028755	0.026308
-5.8	0.414152	0.031079	0.848656	0.031994	0.068164	0.024409
-5.7	0.40725	0.037407	0.841257	0.038894	0.073301	0.029012
-5.6	0.434908	0.031904	0.869711	0.031447	0.051603	0.026308
-5.5	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
-5.4	0.421054	0.020886	0.856055	0.020587	0.063027	0.017222
-5.3	0.441835	0.034106	0.876539	0.033619	0.045891	0.028124
-5.2	0.400323	0.027748	0.834429	0.029746	0.079013	0.020652
-5.1	0.427981	0.027848	0.862883	0.027449	0.057315	0.022963
-5	0.400348	0.041671	0.833857	0.04349	0.078439	0.03216
-4.9	0.434908	0.031904	0.869711	0.031447	0.051603	0.026308
-4.8	0.441835	0.034106	0.87653	0.03361	0.045891	0.028124



			9	9		
-4.7	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
-4.6	0.414177	0.043952	0.848085	0.045239	0.067589	0.03451
-4.5	0.414127	1.67E-16	0.849227	1.12E-15	0.068739	1.26E-16
-4.4	0.400323	0.027748	0.834429	0.029746	0.079013	0.020652
-4.3	0.414152	0.031079	0.848656	0.031994	0.068164	0.024409
-4.2	0.414127	1.67E-16	0.849227	1.12E-15	0.068739	1.26E-16
-4.1	0.400323	0.027748	0.834429	0.029746	0.079013	0.020652
-4	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
-3.9	0.448762	0.03481	0.883367	0.034312	0.040179	0.028704
-3.8	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
-3.7	0.400323	0.027748	0.834429	0.029746	0.079013	0.020652
-3.6	0.393421	0.031789	0.827029	0.034078	0.084151	0.02366
-3.5	0.400348	0.041671	0.833857	0.04349	0.078439	0.03216
-3.4	0.400323	0.027748	0.834429	0.029746	0.079013	0.020652
-3.3	0.421054	0.020886	0.856055	0.020587	0.063027	0.017222
-3.2	0.345106	0.043873	0.773664	0.049566	0.118651	0.030387
-3.1	0.379617	0.034684	0.812231	0.037183	0.094425	0.025816
-3	0.331302	0.041621	0.758081	0.047808	0.128195	0.028091
-2.9	0.345106	0.031023	0.77445	0.035057	0.119381	0.021499
-2.8	0.345106	0.031023	0.77445	0.035057	0.119381	0.021499
-2.7	0.372714	0.033984	0.804832	0.036431	0.099562	0.025294
-2.6	0.365812	0.044418	0.796647	0.04925	0.103969	0.031611
-2.5	0.276085	0.053733	0.690075	0.068072	0.161096	0.030411
-2.4	0.276085	0.043873	0.69118	0.055603	0.162124	0.024874

-2.3	0.255378	0.031789	0.66552 2	0.04278 5	0.174317	0.015562
-2.2	0.22777	0.031789	0.62836 3	0.04278 5	0.187832	0.015562
-2.1	0.282987	0.020811	0.70157 5	0.02467 7	0.159774	0.013287
-2	0.303693	0.033984	0.72612 8	0.04029 7	0.146553	0.021698
-1.9	0.282987	0.037356	0.70047	0.04662 9	0.158745	0.021859
-1.8	0.207064	0.062045	0.5942	0.08715 2	0.192114	0.02807
-1.7	0.186357	0.062432	0.56063 6	0.10161	0.196953	0.018067
-1.6	0.241574	0.055927	0.64473 2	0.07115 8	0.179018	0.03126
-1.5	0.186357	0.076306	0.55717 7	0.11929 1	0.193735	0.024562
-1.4	0.220868	0.041621	0.61734 4	0.05962 2	0.189602	0.017518
-1.3	0.138042	0.043873	0.48361 9	0.08108 1	0.209452	0.007774
-1.2	0.179455	0.033984	0.55641 7	0.05425 5	0.205048	0.008715
-1.1	0.055217	0.074713	0.26546	0.22412 3	0.126725	0.104108
-1	0.041413	0.033984	0.20801 7	0.17070 1	0.121373	0.0996
-0.9	-0.03451	0.034684	0.17334 8	0.17422 1	0.101144	0.101654
-0.8	0.020706	0.054179	0.24268 7	0.15967 6	0.141602	0.093167
-0.7	-0.04141	0.046014	0.27735 6	0.13937 7	0.16183	0.081323
-0.6	0.013804	0.027748	0.06933 9	0.13937 7	0.040458	0.081323
-0.5	0.075923	0.020811	0.36105 6	0.04329 9	0.203626	0.004034
-0.4	0.034511	0.034684	0.17334 8	0.17422 1	0.101144	0.101654
-0.3	0.034511	0.034684	0.17334 8	0.17422 1	0.101144	0.101654
-0.2	-0.08973	0.076306	0.32216 8	0.23020 6	0.143414	0.094546
-0.1	-0.07592	0.020811	0.36105 6	0.04329 9	0.203626	0.004034
0	-0.04141	0.033984	0.20801 7	0.17070 1	0.121373	0.0996
0.1	0.041413	0.033984	0.20801 7	0.17070 1	0.121373	0.0996

0.2	-0.05522	0.027748	0.27735 6	0.13937 7	0.16183	0.081323
0.3	-0.11734	0.069715	0.39991 9	0.21177 7	0.167657	0.084555
0.4	-0.07592	0.020811	0.36105 6	0.04329 9	0.203626	0.004034
0.5	0.013804	0.027748	0.06933 9	0.13937 7	0.040458	0.081323
0.6	-0.04141	0.033984	0.20801 7	0.17070 1	0.121373	0.0996
0.7	0.027608	0.033984	0.13867 8	0.17070 1	0.080915	0.0996
0.8	0.034511	0.034684	0.17334 8	0.17422 1	0.101144	0.101654
0.9	-0.04141	0.033984	0.20801 7	0.17070 1	0.121373	0.0996
1	0.069021	0.043873	0.30607 8	0.16365 2	0.164506	0.082832
1.1	0.075923	0.020811	0.36105 6	0.04329 9	0.203626	0.004034
1.2	0.110434	0.033984	0.43285 9	0.07070 7	0.210316	0.006588
1.3	0.158749	0.062432	0.51494 7	0.10676 3	0.202533	0.014987
1.4	0.186357	0.031789	0.56743 6	0.05075 1	0.203278	0.008152
1.5	0.144945	0.037356	0.49797 9	0.06690 7	0.21079	0.007572
1.6	0.179455	0.055495	0.55295 8	0.08258 3	0.201831	0.020135
1.7	0.200161	0.037356	0.58774 5	0.05621 9	0.19813	0.013363
1.8	0.158749	0.031789	0.52335 9	0.05075 1	0.210358	0.008152
1.9	0.200161	0.037356	0.58774 5	0.05621 9	0.19813	0.013363
2	0.317498	0.046014	0.74171 2	0.05292 4	0.137009	0.030968
2.1	0.276085	0.053733	0.68945 1	0.07418 7	0.160515	0.025427
2.2	0.248476	0.063578	0.65229 2	0.08544	0.174031	0.03199
2.3	0.331302	0.027748	0.75886 6	0.03290 2	0.128925	0.017716
2.4	0.303693	0.033984	0.72612 8	0.04029 7	0.146553	0.021698
2.5	0.3244	0.031789	0.75068 2	0.03769 4	0.133332	0.020297
2.6	0.338204	0.037356	0.76626 5	0.04272	0.123788	0.025402

2.7	0.35891	0.041621	0.78924 8	0.04623 1	0.109107	0.029556
2.8	0.345106	0.043873	0.77366 4	0.04956 6	0.118651	0.030387
2.9	0.365812	0.031789	0.79743 2	0.03407 8	0.1047	0.02366
3	0.35891	0.027748	0.79003 3	0.02974 6	0.109837	0.020652
3.1	0.352008	0.020811	0.78263 4	0.02231	0.114974	0.015489
3.2	0.386519	0.033984	0.81963	0.03643 1	0.089288	0.025294
3.3	0.3244	0.076306	0.74611 6	0.09123 8	0.129085	0.048325
3.4	0.386519	0.033984	0.81963	0.03643 1	0.089288	0.025294
3.5	0.414127	1.67E-16	0.84922 7	1.12E- 15	0.068739	1.26E-16
3.6	0.407225	0.020811	0.84182 8	0.02231	0.073876	0.015489
3.7	0.434908	0.031904	0.86971 1	0.03144 7	0.051603	0.026308
3.8	0.427981	0.027848	0.86288 3	0.02744 9	0.057315	0.022963
3.9	0.386519	0.033984	0.81963	0.03643 1	0.089288	0.025294
4	0.379617	0.034684	0.81223 1	0.03718 3	0.094425	0.025816
4.1	0.386519	0.033984	0.81963	0.03643 1	0.089288	0.025294
4.2	0.434908	0.031904	0.86971 1	0.03144 7	0.051603	0.026308
4.3	0.372714	0.033984	0.80483 2	0.03643 1	0.099562	0.025294
4.4	0.414127	1.67E-16	0.84922 7	1.12E- 15	0.068739	1.26E-16
4.5	0.386519	0.033984	0.81963	0.03643 1	0.089288	0.025294
4.6	0.407225	0.020811	0.84182 8	0.02231	0.073876	0.015489
4.7	0.427981	0.027848	0.86288 3	0.02744 9	0.057315	0.022963
4.8	0.414127	1.67E-16	0.84922 7	1.12E- 15	0.068739	1.26E-16
4.9	0.386519	0.033984	0.81963	0.03643 1	0.089288	0.025294
5	0.421054	0.020886	0.85605 5	0.02058 7	0.063027	0.017222
5.1	0.372714	0.033984	0.80483 2	0.03643 1	0.099562	0.025294

5.2	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
5.3	0.421054	0.020886	0.856055	0.020587	0.063027	0.017222
5.4	0.414152	0.031079	0.848656	0.031994	0.068164	0.024409
5.5	0.414127	1.67E-16	0.849227	1.12E-15	0.068739	1.26E-16
5.6	0.414127	1.67E-16	0.849227	1.12E-15	0.068739	1.26E-16
5.7	0.427981	0.027848	0.862883	0.027449	0.057315	0.022963
5.8	0.414127	1.67E-16	0.849227	1.12E-15	0.068739	1.26E-16
5.9	0.421054	0.020886	0.856055	0.020587	0.063027	0.017222
6	0.400348	0.041671	0.833857	0.04349	0.078439	0.03216
6.1	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
6.2	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
6.3	0.421079	0.03744	0.855484	0.038149	0.062452	0.029762
6.4	0.379617	0.034684	0.812231	0.037183	0.094425	0.025816
6.5	0.414127	1.67E-16	0.849227	1.12E-15	0.068739	1.26E-16
6.6	0.393421	0.031789	0.827029	0.034078	0.084151	0.02366
6.7	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
6.8	0.407225	0.020811	0.841828	0.02231	0.073876	0.015489
6.9	0.434908	0.031904	0.869711	0.031447	0.051603	0.026308
7	0.372714	0.033984	0.804832	0.036431	0.099562	0.025294

140 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_\infty$	STD $U_\infty$	Avg $U_\infty(U_\infty\max-U_\infty)$	STD $U_\infty(U_\infty\max-U_\infty)$
-7	15.76893	0.033984	5.24032	0.005645	0.16779	0.029416
-6.9	15.81034	0.062045	5.247189	0.010296	0.13189	0.053766
-6.8	15.82414	0.041621	5.249485	0.006904	0.119954	0.03608
-6.7	15.82414	0.027748	5.249487	0.004599	0.119968	0.024071
-6.6	15.85175	0.046014	5.254061	0.007633	0.096004	0.039886
-6.5	15.82414	0.060474	5.24948	0.010026	0.119928	0.052453
-6.4	15.94848	0.09318	5.270051	0.01539	0.011855	0.081129
-6.3	15.88626	0.065443	5.259772	0.010844	0.066013	0.056793
-6.2	15.96226	0.041722	5.272345	0.006891	-4.7E-05	0.036326
-6.1	15.74822	0.057622	5.236872	0.009582	0.185674	0.049825
-6	15.80344	0.065443	5.246043	0.010852	0.137865	0.056751
-5.9	15.85865	0.031789	5.255208	0.005269	0.090029	0.027577
-5.8	15.88631	0.095436	5.259768	0.015803	0.065904	0.082878
-5.7	15.6792	0.084676	5.225373	0.014126	0.245245	0.072982
-5.6	15.82414	0.060474	5.24948	0.010035	0.119928	0.052408
-5.5	15.78963	0.062432	5.243752	0.010369	0.149827	0.054054
-5.4	15.80344	0.057622	5.246045	0.009572	0.137878	0.049882
-5.3	15.70681	0.063955	5.22998	0.010644	0.221454	0.055258
-5.2	15.80344	0.057622	5.246045	0.009562	0.137878	0.04993
-5.1	15.78273	0.070743	5.242603	0.011753	0.155788	0.06123
-5	15.87939	0.098138	5.25862	0.016271	0.071913	0.085116
-4.9	15.77583	0.046534	5.241464	0.007736	0.161802	0.04025
-4.8	15.74822	0.037356	5.236877	0.006211	0.1857	0.032308

-4.7	15.66539	0.057622	5.22308 3	0.00960 4	0.257208	0.049709
-4.6	15.76202	0.069715	5.23916 3	0.01158 7	0.173711	0.060316
-4.5	15.66539	0.150228	5.22303 2	0.02506 9	0.25694	0.129445
-4.4	15.54806	0.134511	5.20344 6	0.02247 5	0.358011	0.115751
-4.3	15.93468	0.115347	5.26775 8	0.01907 3	0.023804	0.100311
-4.2	15.65159	0.076306	5.22077 4	0.01273 1	0.269077	0.065762
-4.1	15.46523	0.098102	5.18959	0.01647 7	0.429195	0.083971
-4	15.0303	0.440035	5.11557 1	0.07537 8	0.796362	0.36889
-3.9	15.75512	0.067967	5.23801 6	0.01129 6	0.179686	0.058808
-3.8	15.33409	0.156503	5.16749 9	0.02635 2	0.541101	0.13361
-3.7	15.32712	0.322495	5.16610 6	0.05441 6	0.545907	0.274721
-3.6	15.03715	0.523725	5.11651 4	0.08940 3	0.789399	0.440797
-3.5	14.84382	0.507077	5.08354 1	0.08734 8	0.952239	0.422568
-3.4	15.62408	0.426653	5.21571 8	0.07122 7	0.290325	0.36747
-3.3	14.13963	1.081156	4.95843	0.19486 1	1.518933	0.856013
-3.2	14.16724	0.953896	4.96422 9	0.16855 9	1.501428	0.772643
-3.1	13.82896	0.778971	4.90547 6	0.13820 4	1.780758	0.628108
-3	13.90488	0.849361	4.91853 6	0.15184	1.717398	0.679022
-2.9	14.1396	0.920402	4.95947 4	0.16572 7	1.524482	0.729445
-2.8	13.33183	0.517824	4.81749 9	0.09306 3	2.182644	0.411145
-2.7	13.92556	0.53752	4.92360 4	0.09509 6	1.708106	0.434743
-2.6	13.26286	0.627163	4.80455 1	0.11481 7	2.234488	0.487052
-2.5	13.40783	0.613427	4.83086 1	0.11010 5	2.120745	0.487825
-2.4	13.31112	0.995323	4.81131 8	0.17988	2.186113	0.785208
-2.3	12.39977	0.379018	4.64637 3	0.07068 7	2.903553	0.287406

-2.2	13.23518	0.995441	4.79743 3	0.18308 8	2.24517	0.768744
-2.1	12.69664	0.767969	4.70008 3	0.14185 2	2.669755	0.589731
-2	12.3308	0.482915	4.63309	0.09039 2	2.953635	0.364438
-1.9	12.19951	0.550809	4.60806 4	0.10409 3	3.050322	0.410479
-1.8	11.35032	0.84315	4.44281 6	0.16678 7	3.657903	0.589369
-1.7	12.04769	0.569816	4.57918 1	0.10866	3.162434	0.419676
-1.6	11.28823	0.469846	4.43279 3	0.09194 8	3.71319	0.333564
-1.5	11.75087	1.036609	4.51927 5	0.20061 7	3.363484	0.748797
-1.4	11.62653	0.469771	4.49877 1	0.09111 6	3.47191	0.337735
-1.3	10.99131	1.050426	4.36986 8	0.21369	3.898497	0.703532
-1.2	10.84637	0.577613	4.34455 3	0.11632 3	4.017444	0.392771
-1.1	10.04545	0.799799	4.17936	0.16428	4.541259	0.527226
-1	9.555325	1.544204	4.06523 8	0.33944 5	4.793105	0.902304
-0.9	8.623239	0.746367	3.87144 6	0.17100 1	5.394555	0.398825
-0.8	10.16971	1.55033	4.19629 6	0.31982 5	4.414154	1.01555
-0.7	8.03636	1.900329	3.71284 4	0.46034 7	5.580382	0.894766
-0.6	6.821238	0.71019	3.44205 9	0.17739 1	6.268798	0.302476
-0.5	8.098504	1.371732	3.74210 8	0.31759 5	5.626452	0.719768
-0.4	6.634831	0.623282	3.39519 2	0.16506 9	6.346319	0.21638
-0.3	7.753273	1.431805	3.65932 4	0.33541 4	5.791188	0.733202
-0.2	6.42084	1.264694	3.32840 8	0.32309 2	6.366869	0.506197
-0.1	6.048001	1.457902	3.22185 9	0.39181 8	6.454389	0.493249
0	6.282748	1.384286	3.28604	0.38020 1	6.38397	0.433736
0.1	5.792548	0.546788	3.17244 4	0.15275 4	6.638717	0.14889
0.2	8.284936	0.933539	3.79206 4	0.22054	5.565168	0.465975



0.3	7.649816	0.785507	3.64505 4	0.18921 7	5.896118	0.370888
0.4	6.793629	0.713189	3.43468 5	0.18472 8	6.277999	0.271641
0.5	8.209062	1.364484	3.76736	0.32218 9	5.567052	0.681675
0.6	7.525553	0.641245	3.61688 4	0.15442 9	5.963999	0.303009
0.7	9.134146	0.858904	3.98391	0.18862 9	5.097782	0.501815
0.8	7.684252	1.24282	3.64664 6	0.29095	5.844543	0.632253
0.9	9.679588	0.638838	4.10347 6	0.13527 8	4.778308	0.399769
1	9.009833	0.877888	3.95625 6	0.19673 4	5.168467	0.492535
1.1	9.845263	1.107281	4.13388 7	0.23810 1	4.65013	0.674393
1.2	10.37688	0.710399	4.24842	0.14859 3	4.328203	0.454177
1.3	11.17775	0.598903	4.41037 9	0.11965 6	3.787421	0.412374
1.4	11.33654	0.853669	4.44001 7	0.16940 3	3.66714	0.593949
1.5	11.14324	0.914389	4.40152 9	0.17994 6	3.800862	0.644154
1.6	12.35838	0.527581	4.63809 5	0.09909 1	2.931988	0.396463
1.7	11.8544	0.629931	4.54197 6	0.12079 7	3.302872	0.460204
1.8	12.19271	0.633048	4.6064	0.11981 8	3.053396	0.470839
1.9	12.17203	1.295953	4.59732 6	0.24966 5	3.041572	0.941433
2	12.70359	1.067753	4.69928 2	0.1999	2.653423	0.805868
2.1	12.31002	0.871119	4.62716 6	0.16440 6	2.95859	0.650406
2.2	13.14542	0.441229	4.78393 1	0.07950 3	2.330281	0.34923
2.3	12.95214	1.097245	4.74492 5	0.20435 5	2.461224	0.833996
2.4	13.26278	0.842697	4.80342 2	0.15493	2.228668	0.650828
2.5	13.49751	1.046933	4.84463 5	0.18775	2.037198	0.833535
2.6	13.51134	0.646505	4.84934 2	0.11616 6	2.037927	0.513485
2.7	12.80024	1.259782	4.71581 3	0.22970 9	2.57226	0.983522

2.8	14.38818	0.523175	5.00480 8	0.09187 8	1.330612	0.426779
2.9	14.80933	0.704373	5.07693 2	0.12161 7	0.977452	0.585511
3	13.42849	0.788221	4.83373 2	0.14293 1	2.09991	0.619208
3.1	14.7679	0.506555	5.07053 3	0.08657 8	1.015873	0.42569
3.2	15.03025	0.10779	5.11608	0.01835 5	0.799131	0.090938
3.3	14.20867	0.526452	4.97346 1	0.09291	1.47794	0.426999
3.4	14.88528	0.35548	5.09101 7	0.06105 1	0.919451	0.297181
3.5	14.77485	0.669932	5.07113 9	0.11623 8	1.006964	0.553888
3.6	15.30636	0.427783	5.16239 4	0.07197 3	0.562481	0.365503
3.7	15.52735	0.100285	5.20000 1	0.01678 8	0.375908	0.086131
3.8	14.58151	0.549739	5.03826 4	0.09556 6	1.170319	0.453609
3.9	15.54116	0.057622	5.20233	0.00963 7	0.364148	0.049538
4	15.61708	0.060474	5.21502 1	0.01010 1	0.298843	0.052058
4.1	15.21666	0.343032	5.14741 8	0.05784 2	0.639737	0.292431
4.2	15.63088	0.088836	5.21731 4	0.01483 6	0.286893	0.076481
4.3	15.59637	0.037356	5.21156 9	0.00624 2	0.3167	0.032146
4.4	15.57567	0.186653	5.20801 9	0.03128 8	0.334042	0.160089
4.5	15.6723	0.062045	5.22423 2	0.01035	0.251246	0.053482
4.6	15.51352	0.275897	5.19750 4	0.04673 8	0.386824	0.234047
4.7	15.6861	0.041621	5.22653 8	0.00693 5	0.239364	0.035921
4.8	15.63779	0.077557	5.21847 1	0.01295 8	0.280972	0.066743
4.9	15.61708	0.027748	5.21502 9	0.00463	0.298883	0.023911
5	15.78273	0.033984	5.24261 3	0.00564 5	0.155841	0.029416
5.1	15.61708	0.060474	5.21502 1	0.01010 1	0.298843	0.052058
5.2	15.80344	0.095366	5.24603	0.01584 1	0.137799	0.082558

5.3	15.81034	0.031023	5.24719 7	0.00514 8	0.13193	0.026883
5.4	15.78963	0.062432	5.24375 2	0.01036 9	0.149827	0.054054
5.5	15.83105	0.076306	5.25061 9	0.01266 3	0.113914	0.066118
5.6	15.76893	0.033984	5.24032	0.00564 5	0.16779	0.029416
5.7	15.6723	0.043873	5.22423 7	0.00731 2	0.251273	0.03785
5.8	15.65159	0.044418	5.22078 5	0.00740 6	0.26913	0.038304
5.9	15.76893	0.033984	5.24032	0.00564 5	0.16779	0.029416
6	15.77583	0.063955	5.24145 9	0.01062	0.161776	0.055381
6.1	15.77583	0.034684	5.24146 6	0.00576 2	0.161815	0.030023
6.2	15.76202	0.054179	5.23916 8	0.00900 9	0.173738	0.046853
6.3	15.81724	0.037356	5.24834 1	0.00619 7	0.125942	0.03238
6.4	15.74132	0.053733	5.23572 6	0.00893 6	0.191648	0.04646
6.5	15.74822	0.065443	5.23687	0.01088 3	0.18566	0.056585
6.6	15.76202	0.076306	5.23916	0.01267 7	0.173698	0.066044
6.7	15.71371	0.033984	5.23113 7	0.00565 8	0.215533	0.029351
6.8	15.78273	0.033984	5.24261 3	0.00564 5	0.155841	0.029416
6.9	15.62398	0.044418	5.21617 8	0.00740 5	0.292922	0.038312
7	15.6861	0.027748	5.22654	0.00462	0.239378	0.023965

240 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_\infty$	STD $U_\infty$	Avg $U_\infty(U_\infty\max-U_\infty)$	STD $U_\infty(U_\infty\max-U_\infty)$
-7	53.27911	0.069715	9.632418	0.006301	0.234016	0.060562
-6.9	53.45856	0.088019	9.648626	0.00794	0.07801	0.076605
-6.8	53.54829	0.116903	9.656717	0.010537	-0.00011	0.101826
-6.7	53.23769	0.078788	9.628674	0.007125	0.269972	0.068398
-6.6	53.38264	0.060474	9.641773	0.005461	0.144056	0.052583
-6.5	53.08575	0.065538	9.614924	0.005933	0.401804	0.056834
-6.4	53.2515	0.082371	9.629922	0.00745	0.257984	0.071507
-6.3	53.25835	0.213213	9.630525	0.019287	0.251877	0.185056
-6.2	52.98907	0.178993	9.606153	0.016224	0.485468	0.155034
-6.1	52.79571	0.397485	9.588556	0.036187	0.652269	0.342762
-6	53.09955	0.467984	9.616083	0.042389	0.38896	0.405638
-5.9	53.24447	0.379787	9.629229	0.034295	0.263529	0.330212
-5.8	52.80951	0.129592	9.58987	0.011766	0.640917	0.112063
-5.7	53.04424	0.30571	9.611126	0.027656	0.437423	0.265313
-5.6	52.68528	0.072423	9.578588	0.006583	0.748325	0.062554
-5.5	52.98217	0.302802	9.605502	0.027435	0.491202	0.26239
-5.4	52.69908	0.069715	9.579843	0.006335	0.736404	0.060227
-5.3	52.65077	0.103822	9.575448	0.009438	0.778101	0.089657
-5.2	52.19515	0.376228	9.53387	0.034441	1.170032	0.322602
-5.1	52.56794	0.103822	9.567913	0.009452	0.849579	0.089522
-5	52.3539	0.205965	9.548401	0.018754	1.033898	0.177574
-4.9	52.4368	0.121148	9.55597	0.011035	0.962619	0.104416
-4.8	52.79573	0.440009	9.588543	0.039981	0.652103	0.380181

-4.7	52.34012	0.664451	9.54697 2	0.06069 5	1.04409	0.571005
-4.6	52.48509	0.537283	9.56025 1	0.04893 9	0.919868	0.463076
-4.5	52.16754	0.381574	9.53134 7	0.03491 5	1.193742	0.32733
-4.4	52.347	0.670503	9.54759 5	0.06127 9	1.038135	0.575903
-4.3	52.96146	0.381884	9.60360 2	0.03464 7	0.508911	0.330462
-4.2	52.05698	0.955414	9.52090 6	0.08753 1	1.285457	0.818559
-4.1	51.93967	0.689096	9.51036 2	0.06327 8	1.387926	0.588977
-4	51.74631	0.862333	9.49252 3	0.07927 9	1.552391	0.736165
-3.9	50.73143	0.874282	9.39895 4	0.08097 2	2.416208	0.740618
-3.8	50.77974	0.973056	9.40334 5	0.09027 7	2.374472	0.822773
-3.7	51.3873	1.06873	9.45935 4	0.09871 3	1.857283	0.907921
-3.6	49.92363	2.031932	9.32225 3	0.18984 4	3.082275	1.705411
-3.5	49.91673	1.090083	9.32296 7	0.10226 9	3.101186	0.910784
-3.4	51.29062	1.601527	9.44982 6	0.14718 6	1.933639	1.367733
-3.3	49.30914	2.201015	9.26427 5	0.20885 6	3.592504	1.816562
-3.2	48.77065	1.936529	9.21408 3	0.18229	4.04557	1.612238
-3.1	49.19871	1.288536	9.25543	0.12179 3	3.699401	1.067855
-3	48.99162	1.927553	9.23495 1	0.18178 9	3.862276	1.601435
-2.9	49.40582	2.189705	9.27343 6	0.20530 3	3.512604	1.830813
-2.8	48.03883	1.719309	9.14499 2	0.16482	4.652825	1.402619
-2.7	44.66272	1.165434	8.81844 7	0.11641 2	7.378828	0.905474
-2.6	44.80076	2.313205	8.82987 8	0.22931 6	7.248826	1.814527
-2.5	45.40835	2.479825	8.88918 3	0.24479 4	6.763426	1.954927
-2.4	44.5039	2.212258	8.80080 5	0.21943 2	7.48505	1.733861
-2.3	43.54425	1.457529	8.70688 3	0.14509 4	8.249255	1.137244

-2.2	42.69504	1.802031	8.62085 7	0.18145 8	8.8974	1.386063
-2.1	43.88941	1.524654	8.74121 3	0.15216 3	7.979696	1.18585
-2	42.24628	1.206413	8.57644 9	0.12226 3	9.250064	0.920311
-1.9	41.44539	1.892944	8.49342 2	0.19419 4	9.843022	1.421354
-1.8	42.13577	1.971652	8.5638	0.19887 8	9.320364	1.513282
-1.7	40.3614	1.411269	8.38251 6	0.14655 9	10.65975	1.04258
-1.6	38.92541	1.560164	8.23165 8	0.16490 5	11.70368	1.124666
-1.5	40.45116	2.688191	8.3885	0.27924 9	10.56124	1.985088
-1.4	36.30876	1.696972	7.94956 3	0.18738 2	13.53637	1.145859
-1.3	36.92315	1.866484	8.01618 3	0.20365 4	13.10976	1.284431
-1.2	36.20513	1.738642	7.93811 9	0.19098 2	13.60632	1.183764
-1.1	33.40212	2.211287	7.62278 4	0.24960 3	15.44255	1.441258
-1	32.26983	2.479856	7.49103 1	0.28625 5	16.1421	1.55555
-0.9	31.66917	1.752938	7.42348 2	0.20734	16.53582	1.051046
-0.8	30.13645	3.615289	7.23177 9	0.42975 6	17.35377	2.150909
-0.7	24.96527	4.880475	6.56187 5	0.64967 2	19.89011	2.259883
-0.6	26.58081	3.548367	6.78789 7	0.46483 6	19.25934	1.707363
-0.5	25.66946	3.540575	6.67016 3	0.46199 7	19.7095	1.71958
-0.4	25.9802	3.409516	6.71194 1	0.44195 4	19.57179	1.673542
-0.3	23.77085	6.146164	6.38033 1	0.83327 7	20.21702	2.722525
-0.2	23.76397	3.281684	6.41824 4	0.43831 2	20.59512	1.499487
-0.1	25.4969	5.637207	6.62051 2	0.75925 2	19.53053	2.507674
0	25.35879	3.228926	6.63207 9	0.42269 7	19.88275	1.546253
0.1	22.45907	3.064399	6.23952 2	0.42637 3	21.14169	1.240803
0.2	25.80067	3.79842	6.68469 1	0.49826 7	19.62129	1.818452

0.3	22.59024	3.463721	6.25383 9	0.48151 2	21.05152	1.390218
0.4	24.8272	3.114653	6.56256 4	0.41240 1	20.1372	1.458139
0.5	32.71169	2.333981	7.54271 4	0.27269 2	15.8717	1.432997
0.6	29.08013	2.238771	7.11111 1	0.27344 1	18.02806	1.259663
0.7	28.75563	3.025234	7.06649 4	0.37804 4	18.16231	1.625473
0.8	32.32504	2.069584	7.49901 6	0.24118 6	16.12305	1.276133
0.9	32.64957	2.150277	7.53638 9	0.24785 1	15.9188	1.352251
1	34.69314	1.807131	7.77016 7	0.20421	14.61752	1.175417
1.1	33.12594	4.19051	7.58034 5	0.47771 3	15.51369	2.690775
1.2	35.44572	2.114267	7.85325 6	0.23298 4	14.1093	1.432758
1.3	34.67939	1.519952	7.76943 1	0.17045	14.63437	1.00107
1.4	36.9163	1.618442	8.01611 3	0.17479 7	13.12102	1.130802
1.5	38.29022	2.762734	8.16058 5	0.29439 6	12.12351	1.968981
1.6	38.60784	1.96158	8.19707	0.20625 8	11.92271	1.424697
1.7	41.21757	1.966523	8.46986 1	0.20165 7	10.01224	1.477415
1.8	42.15655	2.027608	8.56573 2	0.20658 8	9.302832	1.536191
1.9	42.21175	0.904306	8.57331 5	0.09211 6	9.279944	0.685326
2	42.85382	1.25899	8.63783 7	0.12730 7	8.784872	0.963157
2.1	44.93888	1.91502	8.84444	0.18860 4	7.148919	1.513805
2.2	44.08277	1.978115	8.75961	0.19508 1	7.820629	1.561199
2.3	45.51188	1.893392	8.90068 7	0.18795 7	6.694216	1.482535
2.4	43.5235	1.555967	8.70461 8	0.15613 5	8.263528	1.202143
2.5	45.52576	1.265519	8.90315 9	0.12361	6.693922	1.010222
2.6	45.93308	1.577466	8.94242 7	0.15473 7	6.363782	1.252977
2.7	44.98722	1.732287	8.84951 4	0.17297	7.113735	1.346618

2.8	45.38762	2.381811	8.88750 9	0.23134 7	6.783361	1.913989
2.9	47.81098	1.766968	9.12317 5	0.17015 8	4.838929	1.434081
3	47.67289	1.108622	9.11094 3	0.10647 7	4.961289	0.902461
3.1	48.31499	1.896217	9.17097 3	0.17964	4.422795	1.567588
3.2	48.47379	1.630093	9.1865	0.15395 6	4.296187	1.352215
3.3	49.47489	1.264355	9.28141 4	0.11886 8	3.469357	1.054002
3.4	51.02829	1.655911	9.42553	0.15310 1	2.155857	1.405367
3.5	50.38622	1.260057	9.36653	0.11806	2.704251	1.054346
3.6	51.63588	0.68374	9.48251	0.06288 8	1.648008	0.583426
3.7	51.02142	1.154858	9.42552 5	0.10693 4	2.167787	0.978549
3.8	50.52431	0.919404	9.37971 1	0.08516 3	2.591058	0.778738
3.9	52.17439	0.632902	9.53186 2	0.05781 7	1.186789	0.543848
4	52.36773	0.582421	9.54953 3	0.05325 5	1.020748	0.499999
4.1	52.25032	0.645572	9.53878 9	0.05879 9	1.121465	0.556438
4.2	52.74744	0.387604	9.58417 6	0.03520 8	0.694021	0.335001
4.3	52.47819	0.428247	9.55966 7	0.03909 2	0.926251	0.368276
4.4	52.02938	0.398874	9.51871	0.03654 4	1.312327	0.34173
4.5	52.49202	0.294484	9.56096 9	0.02674 9	0.914737	0.254528
4.6	52.69908	0.054179	9.57984 4	0.00492 5	0.736412	0.04679
4.7	52.70598	0.219802	9.58045 2	0.01997 9	0.730263	0.189844
4.8	52.89924	0.060474	9.59801 9	0.00548 8	0.563354	0.052315
4.9	52.54033	0.087746	9.56540 2	0.00798 3	0.873405	0.075711
5	52.85098	0.186856	9.59362 6	0.01695 5	0.604985	0.161678
5.1	52.74049	0.048558	9.58360 7	0.00441 2	0.700637	0.04196
5.2	52.78881	0.176039	9.58798 4	0.01599 2	0.658761	0.152133



5.3	52.9269	0.226342	9.60050 8	0.02052 8	0.53922	0.195931
5.4	52.94758	0.072474	9.60240 3	0.00657 1	0.521504	0.062752
5.5	52.80266	0.198231	9.58923 8	0.01799 4	0.64675	0.171445
5.6	53.04434	0.103229	9.61117	0.00935 6	0.437673	0.08942
5.7	52.89924	0.060474	9.59801 9	0.00548 7	0.563354	0.052329
5.8	52.84402	0.055495	9.59300 9	0.00503 7	0.611129	0.048005
5.9	53.11338	0.164397	9.61741 6	0.01488 8	0.377751	0.142526
6	53.09268	0.069469	9.61555 1	0.00629 2	0.395796	0.060218
6.1	53.19628	0.083531	9.62492 7	0.00755 7	0.305916	0.072493
6.2	53.08575	0.057731	9.61492 4	0.00522 8	0.401808	0.050052
6.3	53.36193	0.176721	9.63989 1	0.01596 8	0.161944	0.153552
6.4	53.34123	0.178751	9.63802 1	0.01614 5	0.179938	0.155382
6.5	52.92687	0.27444	9.60049 5	0.02497	0.539141	0.236797
6.6	53.14106	0.054179	9.61993 3	0.00490 3	0.35384	0.047002
6.7	53.17558	0.041621	9.62305 6	0.00376 6	0.323905	0.036113
6.8	53.28601	0.097116	9.63304	0.00878	0.228002	0.084335
6.9	53.23769	0.078788	9.62867 4	0.00712 5	0.269972	0.068398
7	53.12721	0.064036	9.61867 8	0.00579 8	0.365852	0.055532

340 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_{\infty}$	STD $U_{\infty}$	Avg $U_{\infty}(U_{\infty\max}-U_{\infty})$	STD $U_{\infty}(U_{\infty\max}-U_{\infty})$
-7	112.7096	0.291527	14.00997	0.018128	-0.00033	0.253711
-6.9	112.2885	0.503427	13.98375	0.031341	0.365697	0.437615
-6.8	111.6603	0.328482	13.94459	0.020533	0.91119	0.284375
-6.7	112.1919	0.30559	13.97775	0.01903	0.449989	0.265563
-6.6	112.4542	0.320686	13.99408	0.019957	0.221945	0.278871
-6.5	111.8121	0.667198	13.95402	0.041651	0.778938	0.578365
-6.4	112.2125	0.495631	13.97902	0.03093	0.431727	0.429795
-6.3	111.9986	0.374653	13.9657	0.023382	0.617757	0.324865
-6.2	112.4266	0.362162	13.99236	0.02253	0.24588	0.315052
-6.1	111.9364	0.529447	13.9618	0.033032	0.67144	0.459233
-6	111.7224	0.644088	13.94843	0.040204	0.856796	0.558398
-5.9	111.6119	0.444515	13.94156	0.02774	0.952992	0.385465
-5.8	111.4463	0.368232	13.93122	0.023007	1.096545	0.318932
-5.7	111.2529	0.833917	13.91905	0.052167	1.262812	0.721386
-5.6	110.8731	0.519678	13.89533	0.032584	1.591849	0.4485
-5.5	110.9007	0.907923	13.89698	0.056957	1.566917	0.783148
-5.4	110.597	0.900668	13.87794	0.056596	1.829104	0.775571
-5.3	111.1907	0.36619	13.91524	0.022914	1.3177	0.316687
-5.2	111.4669	0.82349	13.93244	0.051478	1.077582	0.712873
-5.1	110.3899	0.606851	13.86501	0.038079	2.008477	0.523328
-5	111.1562	0.479755	13.91306	0.030003	1.347334	0.415132
-4.9	111.0871	0.57888	13.90873	0.036268	1.406841	0.499991
-4.8	111.0389	0.364643	13.90573	0.022818	1.448952	0.315336

-4.7	109.4026	1.152435	13.8027 2	0.07278 1	2.855301	0.987263
-4.6	109.948	1.321391	13.8370 3	0.08332 7	2.386075	1.133755
-4.5	110.7696	0.798509	13.8887 9	0.05013 8	1.680529	0.688143
-4.4	109.8376	1.089844	13.8301 6	0.06866	2.482146	0.935998
-4.3	110.5693	0.631594	13.8762 6	0.03964 4	1.853751	0.544482
-4.2	110.2932	0.756498	13.8589	0.04755 2	2.091397	0.651208
-4.1	108.3532	2.227247	13.7358 2	0.14221 6	3.745573	1.886288
-4	110.0791	1.63205	13.8451 5	0.10267 3	2.271498	1.403767
-3.9	108.0218	3.045723	13.7141 8	0.19356 7	4.019409	2.592234
-3.8	108.291	2.150717	13.7319 4	0.13676 6	3.799363	1.829324
-3.7	107.7111	1.695047	13.6953 7	0.10761 3	4.297037	1.444232
-3.6	107.7594	1.829522	13.6983 8	0.11592 7	4.254968	1.56195
-3.5	105.702	1.716296	13.5670 2	0.11028 5	5.997507	1.443814
-3.4	106.6064	2.484568	13.6244 6	0.15880 8	5.227307	2.101961
-3.3	103.6445	1.206551	13.4345 4	0.07802 1	7.72455	1.008114
-3.2	104.1831	1.141902	13.4694 3	0.07382 3	7.275407	0.954325
-3.1	103.9345	2.674309	13.4524 5	0.17278 8	7.470427	2.236567
-3	101.0831	2.811287	13.2664 4	0.18482 3	9.830096	2.306484
-2.9	99.9647	1.665193	13.1936 6	0.11010 1	10.75808	1.357384
-2.8	96.85087	5.072991	12.9824 7	0.34448	13.22195	4.009311
-2.7	97.96248	2.020286	13.0606 3	0.13425 5	12.3811	1.637419
-2.6	97.8451	3.508438	13.0514	0.23424 5	12.45628	2.828364
-2.5	96.46423	1.945068	12.9603 9	0.13143 4	13.58587	1.545945
-2.4	96.6369	5.10414	12.9680 9	0.34533 1	13.39309	4.051444
-2.3	94.91773	4.233049	12.8535 7	0.28643	14.78258	3.360137

-2.2	97.54131	3.481643	13.0311 3	0.23380 8	12.70126	2.78774
-2.1	86.68806	5.219764	12.2810 9	0.37431 3	21.09378	3.846941
-2	90.54746	4.136659	12.5540 7	0.28454 9	18.19724	3.218616
-1.9	85.21056	4.087674	12.1781 2	0.29198 4	22.2241	3.028212
-1.8	83.61569	4.414178	12.0628 7	0.31906 8	23.38684	3.21771
-1.7	83.10484	3.380467	12.0276 5	0.24535 3	23.78306	2.450188
-1.6	80.36387	2.261909	11.8289 1	0.16632 4	25.77211	1.609016
-1.5	79.16255	4.461488	11.7365 8	0.33523 4	26.57055	3.073944
-1.4	76.9463	3.520445	11.5727	0.26891	28.13416	2.364442
-1.3	76.08336	3.621422	11.5074 5	0.27488 4	28.72278	2.455963
-1.2	76.3802	5.607906	11.5254 1	0.42407 7	28.45748	3.82843
-1.1	68.06763	2.699472	10.8853 9	0.21403 2	33.96686	1.702746
-1	65.36816	3.310205	10.6660 1	0.27046 1	35.59429	1.976797
-0.9	66.57635	2.382996	10.7658 6	0.19205 5	34.88913	1.459329
-0.8	66.04471	7.737982	10.7063 9	0.6257	34.98182	4.717807
-0.7	56.80701	10.03078	9.90492 5	0.90992 8	39.84045	4.839386
-0.6	52.13986	4.187741	9.52158 8	0.37460 2	42.59758	2.049651
-0.5	53.94184	5.935246	9.67721 2	0.54049 4	41.63979	2.769663
-0.4	53.70709	8.374599	9.64075 9	0.76844 6	41.53789	3.850075
-0.3	51.09046	8.211457	9.40234 1	0.75749 7	42.75442	3.704603
-0.2	53.18235	10.68078	9.57046 2	1.01568 2	41.46683	4.463652
-0.1	55.77832	6.226544	9.84056 9	0.54958 2	40.73024	3.151756
0	47.83169	6.188188	9.10775 1	0.59111 4	44.30225	2.508959
0.1	44.56604	4.492026	8.79842 3	0.44698 9	45.65558	1.569255
0.2	49.56462	6.761019	9.26797 6	0.65096 2	43.52916	2.677673

0.3	54.45279	5.027985	9.72755 4	0.45185 9	41.45528	2.432384
0.4	58.36736	8.832223	10.0509 7	0.79302 1	39.1692	4.331712
0.5	56.13731	8.680484	9.85883 3	0.75504	40.36096	4.561011
0.6	58.94732	7.688546	10.1097 1	0.67282	38.98229	3.979669
0.7	60.19012	5.619704	10.2272 6	0.47352 9	38.46477	3.156304
0.8	65.49932	6.065565	10.6686 1	0.49778 9	35.40233	3.591449
0.9	63.22093	3.622192	10.4883 7	0.30301 3	36.84492	2.063377
1	69.96629	3.149528	11.0355 2	0.24815 7	32.76364	2.008812
1.1	67.52219	4.755539	10.8372 3	0.37842 1	34.24193	2.983428
1.2	75.51716	4.830947	11.4619 9	0.36650 8	29.0719	3.279618
1.3	76.13855	5.136354	11.5081 7	0.39483 2	28.63676	3.414518
1.4	78.7345	3.313044	11.7069 4	0.24744 2	26.90078	2.303268
1.5	77.3468	3.35477	11.6031 7	0.25201 2	27.86359	2.312443
1.6	85.16914	4.499003	12.1743 6	0.32363 5	22.24363	3.301791
1.7	89.07686	3.10731	12.4529 8	0.21821 5	19.34196	2.354563
1.8	87.38532	1.612763	12.3355 3	0.11365 5	20.64225	1.2163
1.9	86.86061	2.233916	12.2979 6	0.15737	21.02965	1.685663
2	91.56923	3.530662	12.6256 5	0.24048 9	17.42066	2.779658
2.1	90.42315	2.648425	12.5473 1	0.18392 8	18.31895	2.035428
2.2	95.22157	3.796128	12.8747 9	0.25514 3	14.55071	3.036503
2.3	96.01551	2.438526	12.9298 3	0.16456 9	13.93918	1.941126
2.4	97.43772	2.652831	13.0250 8	0.17821 4	12.79685	2.123163
2.5	97.24446	3.2597	13.0115 3	0.21954	12.94355	2.601099
2.6	99.30182	3.315219	13.1484 6	0.22087 1	11.2792	2.679203
2.7	103.0508	2.964149	13.3948 7	0.19230 3	8.202578	2.467874

2.8	101.5595	2.33008	13.2980 7	0.15289 6	9.443681	1.915785
2.9	101.5802	2.265327	13.2994 8	0.14891 1	9.427181	1.858765
3	100.1787	3.764806	13.2059 4	0.24748 6	10.55736	3.089294
3.1	104.1071	3.82576	13.4624 6	0.24792	7.310018	3.18932
3.2	103.7619	1.666346	13.4419 5	0.10774 4	7.623817	1.392396
3.3	106.7928	1.981881	13.6367	0.12689 1	5.074175	1.673663
3.4	104.4109	2.779581	13.4831 5	0.18063 1	7.070907	2.310007
3.5	106.7514	4.120123	13.6320 9	0.26546 9	5.081564	3.456143
3.6	108.9607	2.261842	13.7742 7	0.14301 9	3.226261	1.935264
3.7	108.1184	2.731126	13.7205 6	0.17490 5	3.940542	2.305802
3.8	108.5534	1.621715	13.7488 6	0.10273 5	3.579539	1.384851
3.9	108.291	1.360914	13.7323 4	0.08627 8	3.80505	1.161245
4	110.3968	1.156112	13.8653	0.07272 6	2.000653	0.994437
4.1	108.94	1.335644	13.7734 4	0.08470 5	3.250667	1.139284
4.2	110.2173	0.834488	13.8541 1	0.05239 5	2.156532	0.719178
4.3	110.5901	1.490796	13.8773 1	0.09380 1	1.832261	1.282031
4.4	110.024	2.502499	13.8411 5	0.15933 6	2.311539	2.125769
4.5	111.4669	0.438061	13.9325	0.02741	1.07857	0.378853
4.6	111.0113	0.540592	13.9039 8	0.03387 9	1.472497	0.466779
4.7	111.2598	0.729864	13.9195	0.04578 4	1.257153	0.629599
4.8	110.9214	0.541225	13.8983 5	0.03390 8	1.550121	0.467471
4.9	111.4116	0.526665	13.9290 3	0.03290 8	1.126276	0.456134
5	111.5635	0.569217	13.9385 2	0.03555 1	0.994605	0.493205
5.1	111.1079	0.32254	13.9100 6	0.02019 3	1.389329	0.278785
5.2	110.9215	0.733833	13.8983 2	0.04607 1	1.549593	0.632492

5.3	111.7155	0.416877	13.9480 3	0.02600 9	0.863225	0.361596
5.4	111.8673	0.428912	13.9575	0.02673 6	0.731596	0.37236
5.5	111.7016	0.390622	13.9471 7	0.02438	0.875275	0.338687
5.6	111.5981	0.139507	13.9407 2	0.00871 3	0.965298	0.120874
5.7	111.895	0.377564	13.9592 4	0.02355 6	0.707638	0.327494
5.8	111.4531	0.265206	13.9316 5	0.01656 7	1.09076	0.229736
5.9	111.7777	0.25021	13.9519 3	0.01562 8	0.809541	0.216788
6	111.6602	0.167294	13.9446	0.01044 2	0.911454	0.14505
6.1	111.9917	0.330501	13.9652 7	0.02063 7	0.623808	0.286438
6.2	112.1228	0.124091	13.9734 6	0.00773 3	0.510112	0.107767
6.3	112.3092	0.381438	13.9850 5	0.02376 6	0.347929	0.331304
6.4	112.2471	0.097116	13.9812	0.00604 9	0.402198	0.084375
6.5	112.0745	0.142333	13.9704 5	0.00887 3	0.552057	0.123556
6.6	111.7361	0.13245	13.9493 4	0.00826 6	0.845642	0.114845
6.7	112.0055	0.201233	13.9661 4	0.01255 3	0.611959	0.174576
6.8	112.6406	0.077669	14.0056 9	0.00482 9	0.059916	0.067605
6.9	112.5163	0.299347	13.9979 5	0.01862 5	0.167914	0.260364
7	112.0676	0.041621	13.9700 2	0.00259 4	0.558086	0.036137

440 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_{\infty}$	STD $U_{\infty}$	Avg $U_{\infty}(U_{\infty\max}-U_{\infty})$	STD $U_{\infty}(U_{\infty\max}-U_{\infty})$
-7	191.6789	0.975446	18.27018	0.046485	0.550746	0.848012
-6.9	192.2934	0.536409	18.29948	0.02552	0.016875	0.46711
-6.8	192.3141	0.83859	18.30044	0.039899	-0.00158	0.730212
-6.7	192.2727	0.867547	18.29846	0.041312	0.034403	0.754776
-6.6	191.2992	0.765047	18.25209	0.036499	0.881098	0.664359
-6.5	192.0862	0.919385	18.28958	0.043754	0.196597	0.800354
-6.4	191.8999	0.609099	18.28074	0.028997	0.359239	0.530064
-6.3	191.5062	1.369552	18.26189	0.065317	0.699753	1.189693
-6.2	192.1829	0.980423	18.29418	0.046678	0.112302	0.853136
-6.1	191.9344	0.787493	18.28237	0.037499	0.328962	0.685142
-6	192.0793	0.731348	18.28928	0.034825	0.202929	0.63631
-5.9	190.4707	0.964396	18.2125	0.046133	1.599388	0.835197
-5.8	190.5673	1.193314	18.21709	0.057044	1.515085	1.034181
-5.7	190.6364	1.272969	18.22038	0.060821	1.454992	1.103785
-5.6	190.7192	0.780241	18.2244	0.037263	1.384309	0.676837
-5.5	190.3188	1.018976	18.20523	0.048697	1.730885	0.883328
-5.4	190.3188	0.51945	18.20528	0.02484	1.731714	0.450025
-5.3	190.1738	1.74285	18.19817	0.083318	1.854155	1.510347
-5.2	190.3119	0.875093	18.20492	0.04185	1.73715	0.758072
-5.1	189.5179	0.839008	18.16691	0.040207	2.424196	0.7253
-5	190.5052	1.252108	18.21411	0.059895	1.568778	1.0844
-4.9	189.8424	1.136794	18.18242	0.054406	2.14293	0.984024
-4.8	189.7388	0.86545	18.17749	0.041442	2.233122	0.748744



-4.7	190.5259	1.447305	18.2150 7	0.06929 8	1.55023	1.252252
-4.6	189.4834	1.036291	18.1652 3	0.04967 4	2.45362	0.895615
-4.5	188.3787	1.16662	18.1121 8	0.05608 8	3.406591	1.005195
-4.4	187.7573	2.421741	18.082	0.11670 3	3.936289	2.081673
-4.3	189.1657	1.331981	18.1499 5	0.06399	2.727196	1.148554
-4.2	186.7148	2.091411	18.0318 2	0.10106 2	4.833509	1.792636
-4.1	186.5768	2.409148	18.0250 6	0.11627 5	4.950232	2.067568
-4	188.1785	2.003708	18.1023 9	0.09648 9	3.575978	1.723602
-3.9	185.403	2.172891	17.9683 4	0.10518 4	5.956248	1.8591
-3.8	184.6367	1.650489	17.9313	0.08010 6	6.612809	1.408293
-3.7	185.9347	4.389663	17.9931 3	0.21363 6	5.484145	3.734973
-3.6	180.2388	2.11362	17.7163 3	0.10371 7	10.33759	1.782728
-3.5	177.8569	4.213183	17.5979 5	0.20894 7	12.31918	3.513383
-3.4	179.217	3.721855	17.6653 9	0.18399 2	11.18483	3.114468
-3.3	177.2976	4.744685	17.5699 4	0.23441	12.78046	3.972999
-3.2	175.9582	5.6428	17.5027 1	0.28333 7	13.88284	4.641844
-3.1	175.3783	4.262498	17.4748	0.21500 2	14.382	3.488495
-3	176.1585	4.457015	17.5135 5	0.22180 4	13.73242	3.702808
-2.9	172.1402	4.721124	17.3124 1	0.23778 9	17.0491	3.870172
-2.8	171.0494	5.084459	17.2572	0.25655 4	17.93825	4.159542
-2.7	170.9183	5.907137	17.2498 8	0.29997 7	18.03282	4.798191
-2.6	168.9712	5.943204	17.1513	0.30141 8	19.61929	4.834235
-2.5	172.4026	4.162686	17.3259 8	0.20871 5	16.84037	3.42972
-2.4	159.1674	6.592861	16.6453 2	0.34414 3	27.43267	5.183815
-2.3	161.5494	4.397118	16.7714 1	0.22909 4	25.59201	3.465051

-2.2	154.0308	3.838309	16.3767 3	0.20463 2	31.4626	2.939677
-2.1	158.7462	4.430783	16.6251 9	0.23290 6	27.79767	3.453931
-2	148.3211	8.414993	16.0651 3	0.45741 2	35.70339	6.28493
-1.9	150.1714	4.120506	16.1699 9	0.22247 7	34.40024	3.104433
-1.8	143.3639	5.771986	15.7975 4	0.31843 9	39.43917	4.224964
-1.7	145.2764	9.343167	15.8975 9	0.51238 9	37.93957	6.895599
-1.6	143.6194	7.093555	15.8099 8	0.39194 7	39.22195	5.181423
-1.5	134.0917	3.926792	15.2795 8	0.22436	46.10755	2.73262
-1.4	128.9412	7.269435	14.9788	0.42831 8	49.57247	4.823407
-1.3	118.0879	8.392028	14.3312 5	0.51323 4	56.62259	5.223166
-1.2	127.9194	4.990006	14.9225 5	0.29171 7	50.32244	3.352162
-1.1	122.3133	4.721216	14.5919 7	0.28139 1	54.03548	3.072732
-1	113.2206	7.936048	14.0329 8	0.49719 9	59.64041	4.725583
-0.9	99.10171	9.470007	13.1227 9	0.61470 6	67.57105	5.263171
-0.8	107.7594	4.722384	13.6955 3	0.30367 5	62.97535	2.668194
-0.7	95.85671	5.921187	12.9140 4	0.40002 9	69.40174	2.996812
-0.6	95.10411	11.99755	12.8429 8	0.82752 6	69.41204	5.773229
-0.5	94.79346	11.78374	12.8226 5	0.81572 1	69.58097	5.64232
-0.4	90.6648	9.971048	12.5464 8	0.69271 9	71.71683	4.697303
-0.3	88.95258	8.30949	12.4329 9	0.57572 7	72.62173	3.939705
-0.2	74.08112	5.940134	11.3491 9	0.45550 7	78.68563	2.011406
-0.1	79.2385	7.072667	11.7352 8	0.52610 6	76.76994	2.694142
0	81.17857	7.797493	11.8761 9	0.57340 3	75.97008	3.096532
0.1	90.94094	10.11053	12.5647 3	0.70896 4	71.56998	4.669161
0.2	84.67892	9.153947	12.1253 9	0.66661 6	74.4349	3.769078

0.3	99.42616	11.08231	13.1378 9	0.74035 2	67.28232	5.77615
0.4	89.61538	8.642089	12.4779 1	0.60596 6	72.28945	3.970528
0.5	98.50788	6.899142	13.0896 7	0.45847 9	67.99908	3.628795
0.6	93.5093	6.815221	12.7521 1	0.47840 2	70.52631	3.121907
0.7	101.7321	9.610466	13.2953 5	0.63251 3	66.14827	5.167591
0.8	113.9524	6.583544	14.0811 9	0.40678 7	59.24818	4.023018
0.9	119.5447	6.125269	14.4239 4	0.36571 8	55.78192	3.975257
1	121.975	8.39253	14.5659 4	0.50068 9	54.14827	5.4543
1.1	124.0393	4.390856	14.6949 8	0.26076	52.91483	2.874572
1.2	127.5604	7.537692	14.8979 3	0.44192 3	50.49702	5.041391
1.3	146.2706	7.2049	15.9553 1	0.39287 3	37.26448	5.358198
1.4	142.6114	6.116811	15.7555 1	0.34233	39.98055	4.389119
1.5	148.2451	2.420434	16.0669 2	0.13181 3	35.8685	1.802881
1.6	149.1081	6.351194	16.1105 1	0.34456 2	35.16329	4.755788
1.7	144.8276	5.040852	15.8788	0.27583 7	38.37736	3.731083
1.8	149.6674	4.367065	16.1426 5	0.23523 4	34.77758	3.300495
1.9	152.1805	7.553145	16.2743 5	0.40436 4	32.81134	5.754737
2	163.3444	6.566522	16.8625 5	0.33712 7	24.13397	5.266753
2.1	155.5704	6.8288	16.4556 9	0.36254 6	30.22645	5.257759
2.2	170.1035	6.046917	17.2086 3	0.30433 6	18.69674	4.961263
2.3	168.4949	8.158714	17.1247 5	0.41488	19.96295	6.616763
2.4	166.4236	4.576854	17.0225 3	0.23344 7	21.6993	3.698495
2.5	168.8815	4.167332	17.1480 8	0.21094 1	19.71666	3.397139
2.6	163.1511	2.360944	16.8554 6	0.12213 6	24.34095	1.87637
2.7	167.8045	5.347761	17.0924 3	0.27292 9	20.57395	4.31852

2.8	177.3598	4.933793	17.5728 8	0.24408 8	12.7262	4.125282
2.9	175.5164	4.024649	17.4818 5	0.20106 9	14.27042	3.329182
3	182.1443	5.780564	17.8077 9	0.28437 3	8.692935	4.862958
3.1	177.4702	4.720115	17.5785	0.23368 5	12.63657	3.943495
3.2	178.9477	3.773292	17.6520 8	0.18680 8	11.41028	3.152494
3.3	180.584	5.584074	17.7314 9	0.27373 1	10.01403	4.715418
3.4	182.1029	3.20097	17.8073 2	0.15692 3	8.756628	2.702699
3.5	184.2362	4.554523	17.9106 4	0.22267	6.932352	3.856842
3.6	184.9474	2.869502	17.9460 2	0.13975	6.341111	2.439677
3.7	186.3903	1.630554	18.0162 6	0.07866 7	5.113729	1.399918
3.8	185.7552	4.221566	17.9845 3	0.20677 5	5.639191	3.567779
3.9	189.9184	2.777451	18.1856 5	0.13296 4	2.06989	2.403561
4	187.7021	0.862234	18.0796 6	0.04152	3.989787	0.741715
4.1	189.8907	1.5407	18.1846 6	0.07381 6	2.099892	1.33221
4.2	188.5444	1.792176	18.1200 3	0.08607 1	3.261626	1.545875
4.3	188.7861	1.754661	18.1316 5	0.08432 9	3.053368	1.512427
4.4	190.6985	0.606856	18.2234 3	0.02898 8	1.402514	0.526316
4.5	191.0575	0.920057	18.2405 4	0.04389 6	1.090568	0.798938
4.6	189.877	1.305122	18.1840 5	0.06271 1	2.112547	1.125191
4.7	190.8504	0.693257	18.2306 8	0.03313 2	1.270701	0.600949
4.8	190.298	0.708388	18.2042 7	0.03387 4	1.749429	0.613716
4.9	190.5397	0.562686	18.2158 4	0.02688 2	1.540273	0.48795
5	189.5455	0.684198	18.1682 5	0.03282 6	2.400601	0.590766
5.1	191.5684	0.693976	18.2649 4	0.03307 5	0.647304	0.60325
5.2	190.3326	0.63354	18.2059 3	0.03030 4	1.719607	0.548709

5.3	190.2981	0.484791	18.2042 9	0.02317 4	1.749689	0.420148
5.4	190.4155	0.465468	18.2099 1	0.02224 3	1.648023	0.40354
5.5	189.801	0.365108	18.1805 1	0.01748	2.180033	0.315937
5.6	190.3049	0.409545	18.2046 2	0.01958 1	1.743852	0.354868
5.7	190.8711	0.821738	18.2316 5	0.03924 6	1.25252	0.71281
5.8	190.2774	0.917362	18.2032 7	0.04398 1	1.766928	0.792675
5.9	190.6916	0.607307	18.2231	0.02900 6	1.408562	0.526783
6	190.2014	0.628685	18.1996 6	0.03008 1	1.833233	0.544327
6.1	190.9678	0.522096	18.2362 9	0.02492 3	1.169101	0.453109
6.2	190.084	0.421841	18.1940 5	0.02018 5	1.935131	0.365234
6.3	191.4234	0.574056	18.2580 3	0.02739 8	0.773456	0.498296
6.4	190.1945	0.386077	18.1993 4	0.01846	1.839533	0.334512
6.5	190.3326	0.31617	18.2059 5	0.01511 7	1.719994	0.273941
6.6	190.084	0.235926	18.1940 6	0.01128 3	1.935271	0.204374
6.7	190.2429	0.371403	18.2016 6	0.01777 3	1.797642	0.321522
6.8	191.0714	0.355564	18.2412 5	0.01698 4	1.079336	0.308388
6.9	191.0851	0.620648	18.2418 9	0.02962 7	1.067128	0.538645
7	190.8918	0.654241	18.2326 6	0.03123 4	1.23486	0.567737

540 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_\infty$	STD $U_\infty$	Avg $U_\infty(U_\infty\max-U_\infty)$	STD $U_\infty(U_\infty\max-U_\infty)$
-7	293.7009	1.335832	22.61562	0.051458	0.629185	1.161099
-6.9	293.1762	0.602672	22.59546	0.023217	1.086344	0.523825
-6.8	293.9357	1.215892	22.62467	0.046804	0.425222	1.057614
-6.7	294.4121	1.276506	22.64299	0.049082	0.010479	1.111599
-6.6	293.3627	1.287168	22.6026	0.049529	0.923361	1.120052
-6.5	291.3121	0.824666	22.5235	0.03188	2.703183	0.714242
-6.4	292.3409	0.618319	22.56324	0.023856	1.811652	0.536588
-6.3	291.395	1.12111	22.52668	0.04332	2.630994	0.971449
-6.2	291.9818	1.147134	22.54935	0.044324	2.12235	0.994028
-6.1	292.189	0.940464	22.55736	0.036311	1.943053	0.815561
-6	292.6585	1.071134	22.57547	0.041315	1.535411	0.929824
-5.9	291.616	1.136715	22.53522	0.0439	2.439527	0.985498
-5.8	292.762	1.541699	22.57942	0.059457	1.444619	1.3385
-5.7	290.7046	1.454897	22.49995	0.056319	3.228033	1.258379
-5.6	291.6919	1.542761	22.53812	0.059648	2.372921	1.33603
-5.5	290.318	1.385381	22.48499	0.053683	3.562557	1.197008
-5.4	290.3871	0.68198	22.48771	0.026402	3.503881	0.589819
-5.3	288.4676	2.012724	22.41315	0.078388	5.158097	1.730099
-5.2	288.9992	0.883985	22.4339	0.03432	4.702252	0.762305
-5.1	290.8772	0.831779	22.50667	0.032189	3.079765	0.719639
-5	290.3524	1.101181	22.48635	0.042638	3.533271	0.952179
-4.9	288.3917	1.611382	22.41025	0.062615	5.224635	1.388338
-4.8	289.4687	2.100324	22.45199	0.081495	4.294397	1.812312
-4.7	291.036	1.867662	22.51273	0.07213	2.940198	1.619182

-4.6	288.4953	1.871748	22.4142 4	0.07259 3	5.134699	1.615813
-4.5	288.0189	2.537399	22.3956 3	0.09872 9	5.542875	2.183226
-4.4	285.706	1.488167	22.3056 7	0.05813 9	7.533553	1.275107
-4.3	286.0788	1.932471	22.3201 6	0.07534 7	7.212588	1.659195
-4.2	285.6853	4.808369	22.3041 4	0.18869 8	7.535114	4.100834
-4.1	286.2307	1.988386	22.3260 8	0.07742 8	7.082088	1.709448
-4	286.4447	3.233354	22.3342 1	0.12602	6.89337	2.77725
-3.9	279.368	5.231223	22.0559 8	0.20692	12.9172	4.42471
-3.8	288.8612	3.486647	22.4281 6	0.13577 9	4.812644	2.997369
-3.7	274.7837	8.293017	21.8727	0.33346 6	16.75056	6.891958
-3.6	278.5258	4.34405	22.023	0.17217 9	13.63718	3.666281
-3.5	283.6555	6.450512	22.2241 1	0.25489 6	9.257637	5.461781
-3.4	268.4733	6.716625	21.6209	0.27061 8	22.03819	5.569232
-3.3	274.3556	3.34467	21.8577 7	0.13312 3	17.15793	2.810286
-3.2	264.1928	4.051418	21.4488 9	0.16419 3	25.59757	3.337504
-3.1	272.1256	10.63198	21.7650 4	0.42574 3	18.94159	8.875268
-3	259.3185	8.616152	21.2478 3	0.35210 7	29.53337	7.03259
-2.9	266.119	6.717306	21.5258 8	0.27077 5	23.98642	5.566911
-2.8	261.8178	5.409049	21.3517 6	0.22011	27.53418	4.435775
-2.7	255.5834	9.662256	21.0932 9	0.40439 5	32.53843	7.670111
-2.6	254.9413	5.738585	21.0693	0.23593 1	33.11344	4.651413
-2.5	258.9043	5.309666	21.2326 4	0.21787 8	29.91058	4.313217
-2.4	250.6469	5.624125	20.8910 9	0.23439 6	36.55661	4.486889
-2.3	245.6691	8.518803	20.6808 1	0.35875 3	40.46382	6.712411
-2.2	231.4673	11.42733	20.0711 3	0.49364 6	51.39032	8.723868

-2.1	238.475	7.860131	20.3760 6	0.33498 2	46.09153	6.103526
-2	230.1555	6.988543	20.0179 1	0.30228 6	52.46959	5.326062
-1.9	228.4916	12.85073	19.9397 9	0.56341 4	53.59835	9.623206
-1.8	230.3143	8.673459	20.0235 3	0.37817 6	52.32056	6.543515
-1.7	215.9745	7.306599	19.3908 3	0.32865 5	62.96615	5.282445
-1.6	213.9792	10.20595	19.2982	0.46721 4	64.34332	7.196648
-1.5	212.4326	7.739718	19.2307 5	0.3502	65.50938	5.549411
-1.4	195.0895	8.223294	18.4280 1	0.38839 4	77.53483	5.527026
-1.3	191.1887	5.848464	18.2447 5	0.27879 1	80.17821	3.873148
-1.2	181.4056	6.900528	17.7707 2	0.33670 1	86.48155	4.393828
-1.1	173.2104	7.749834	17.3633 9	0.39181 2	91.52964	4.625173
-1	175.6544	9.468682	17.4835 4	0.47277 2	89.99411	5.786056
-0.9	167.1486	14.38968	17.0445	0.75730 4	94.86535	7.933936
-0.8	152.8364	13.45309	16.2982 3	0.72918 4	102.8912	6.932601
-0.7	160.2445	12.24495	16.6930 4	0.63715 2	98.93029	6.912415
-0.6	155.6533	11.90834	16.4523 4	0.62332 7	101.4754	6.631353
-0.5	129.6869	5.993086	15.0241 8	0.34609	114.3563	2.600682
-0.4	126.0553	15.24762	14.7902 7	0.88095 9	115.3839	6.629062
-0.3	145.8632	18.24215	15.9083	0.97509 5	106.2052	9.707124
-0.2	127.3395	14.18313	14.8691 8	0.81917 9	114.9343	6.176483
-0.1	128.168	11.02029	14.9270 2	0.62266 5	114.8011	5.100546
0	124.4328	18.83481	14.6771 7	1.13518 1	115.6483	7.184779
0.1	130.4118	10.75812	15.0570 7	0.62897 2	113.8386	4.514504
0.2	129.4245	17.67876	14.9808 7	0.98540 4	113.8324	8.513411
0.3	131.6408	8.793798	15.1325 9	0.50459 5	113.4083	3.89429



0.4	142.0314	8.343814	15.7204 5	0.46034 9	108.6246	4.10984
0.5	141.1753	7.132015	15.6746 8	0.39671 7	109.0791	3.440716
0.6	163.2823	14.90917	16.8449 6	0.77675	97.07988	8.393386
0.7	149.6674	14.39593	16.1256 7	0.78020 1	104.5026	7.417534
0.8	163.9796	7.80281	16.8939	0.40227 1	96.97392	4.480981
0.9	175.8064	11.06528	17.4887 5	0.55378 9	89.8475	6.737141
1	176.5658	12.57473	17.5244 2	0.61730 8	89.33268	7.927444
1.1	191.5408	8.92652	18.2587 2	0.42665 4	79.88135	5.885817
1.2	188.3649	10.5862	18.1044 8	0.51039 7	81.91968	6.881283
1.3	209.6849	6.928955	19.1065 3	0.31561 1	67.4817	4.920621
1.4	201.5932	6.242515	18.7345 9	0.28780 1	73.1509	4.354699
1.5	219.9374	9.856591	19.5658	0.44060 3	60.02666	7.191214
1.6	213.1576	9.234217	19.2621 3	0.42171 2	64.95741	6.534753
1.7	223.2376	14.79623	19.7063 6	0.65062 6	57.4624	11.0394
1.8	233.3383	7.278777	20.1556 9	0.31415 2	50.0469	5.562438
1.9	231.5433	5.900107	20.0788 4	0.25415 4	51.43262	4.520038
2	241.8511	4.763888	20.5215 5	0.20178 6	43.50654	3.727083
2.1	240.7878	3.94065	20.4766 9	0.16791 7	44.34234	3.060295
2.2	244.6887	9.841245	20.6383 8	0.41807 9	41.2105	7.673251
2.3	241.8097	8.692945	20.5175 1	0.36782 6	43.4872	6.81092
2.4	242.6381	12.31719	20.5492 6	0.52497 1	42.76339	9.564136
2.5	253.7262	6.27106	21.0187 4	0.26004 6	34.08467	5.032646
2.6	260.9686	3.163447	21.3178 4	0.12922 7	28.24496	2.582869
2.7	262.8741	5.103463	21.3949 1	0.20854 2	26.67171	4.165573
2.8	263.9581	7.34395	21.4379 1	0.29970 8	25.75767	6.003086

2.9	265.622	5.532259	21.50629	0.224493	24.4085	4.551045
3	270.9933	7.053322	21.722	0.28326	19.93874	5.869281
3.1	276.4752	6.807818	21.94079	0.271311	15.34645	5.712492
3.2	270.586	7.567659	21.70541	0.302407	20.27243	6.331616
3.3	279.2714	4.531269	22.05241	0.17899	13.00455	3.838161
3.4	268.2386	6.858676	21.61137	0.277161	22.231	5.668456
3.5	277.2899	4.594068	21.974	0.182443	14.67984	3.869411
3.6	285.6231	2.94852	22.30221	0.115202	7.599666	2.526155
3.7	285.6853	2.881844	22.30465	0.112524	7.546623	2.470693
3.8	284.6635	2.690217	22.26476	0.105324	8.422809	2.300009
3.9	283.2205	4.994665	22.20765	0.195814	9.642513	4.264146
4	288.1293	1.027795	22.4001	0.039955	5.451851	0.885154
4.1	287.653	2.042951	22.38147	0.079506	5.859551	1.757434
4.2	286.6794	2.317633	22.34353	0.090288	6.695677	1.99164
4.3	290.1108	1.066454	22.47699	0.041326	3.7422	0.921415
4.4	288.4193	2.639024	22.41117	0.102712	5.197529	2.270022
4.5	291.1947	0.855533	22.51896	0.033067	2.804822	0.741113
4.6	289.6828	1.598611	22.46036	0.061979	4.110956	1.380508
4.7	291.3605	0.904973	22.52536	0.03497	2.66119	0.784131
4.8	289.5378	0.707005	22.4548	0.027416	4.237682	0.610437
4.9	289.9037	1.612218	22.46892	0.062475	3.920076	1.392964
5	292.5687	1.09417	22.57201	0.042219	1.613304	0.949465
5.1	291.181	1.432582	22.51838	0.055434	2.815682	1.239558
5.2	291.5952	0.695502	22.53444	0.02688	2.45809	0.60254
5.3	290.9877	0.958506	22.51094	0.037068	2.983949	0.829858

5.4	291.6435	0.696526	22.5363 1	0.02693 1	2.416243	0.603155
5.5	291.5607	0.508961	22.5331 2	0.01966 8	2.488204	0.440972
5.6	293.3489	0.493009	22.6021 1	0.01899 7	0.936396	0.428392
5.7	293.0451	1.025084	22.5903 8	0.03954 8	1.199789	0.889645
5.8	292.8103	0.660804	22.5813 5	0.02548	1.404144	0.57381
5.9	292.5618	0.31228	22.5717 7	0.01204 9	1.620151	0.271002
6	293.0727	0.728063	22.5914 6	0.02807 4	1.17619	0.632199
6.1	293.4455	0.475799	22.6058 4	0.01832 8	0.852417	0.413581
6.2	294.0462	0.681983	22.6289 5	0.02625 6	0.329835	0.593127
6.3	293.8736	0.63613	22.6223 1	0.0245	0.480029	0.553036
6.4	293.4318	0.41682	22.6053 1	0.01605 1	0.864412	0.362425
6.5	293.9772	0.486712	22.6263	0.01872 8	0.390038	0.423516
6.6	292.9691	0.735101	22.5874 7	0.02832 7	1.266137	0.638729
6.7	294.4259	0.710576	22.6435 6	0.02731 8	-0.00074	0.618871
6.8	293.5836	0.543763	22.6111 5	0.02094 6	0.73229	0.472646
6.9	293.8528	0.45479	22.6215 2	0.01750 2	0.49823	0.395689
7	293.8666	0.822372	22.6220 4	0.03165	0.485878	0.715463

640 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_\infty$	STD $U_\infty$	Avg $U_\infty(U_\infty\max-U_\infty)$	STD $U_\infty(U_\infty\max-U_\infty)$
-7	417.6919	1.489993	26.97021	0.048138	1.174783	1.294369
-6.9	418.2788	2.297034	26.98909	0.074179	0.66286	1.996345
-6.8	418.0026	0.928966	26.98026	0.029976	0.90532	0.808001
-6.7	416.684	1.272712	26.93766	0.041146	2.050781	1.104876
-6.6	416.0833	2.39392	26.91816	0.077468	2.570006	2.076223
-6.5	419.0451	1.651485	27.01385	0.05324	-0.00281	1.437788
-6.4	416.5114	0.879782	26.9321	0.028431	2.201091	0.764087
-6.3	414.5505	1.823019	26.86858	0.059047	3.899906	1.579625
-6.2	415.1305	1.670199	26.88738	0.054074	3.397734	1.447846
-6.1	415.89	2.123725	26.91193	0.068668	2.738368	1.843389
-6	415.7174	1.423779	26.90639	0.046103	2.889361	1.234042
-5.9	413.8463	1.400439	26.84577	0.045384	4.510221	1.212804
-5.8	413.66	1.625295	26.83971	0.052713	4.671096	1.406407
-5.7	414.0673	1.820077	26.85291	0.059051	4.318286	1.574391
-5.6	414.5644	0.970521	26.86907	0.03145	3.889129	0.840529
-5.5	413.6875	1.459608	26.84062	0.047316	4.647502	1.263662
-5.4	415.0477	1.339809	26.88471	0.043376	3.470007	1.161469
-5.3	413.8049	1.053766	26.84444	0.034158	4.546499	0.912365
-5.2	413.1283	2.394418	26.8224	0.077732	5.129229	2.06995
-5.1	413.4114	1.150105	26.83167	0.037326	4.886792	0.994551
-5	414.5022	1.324584	26.86704	0.042912	3.942565	1.147498
-4.9	412.3412	1.452262	26.79691	0.047167	5.811257	1.254896
-4.8	414.6541	2.033077	26.87192	0.065901	3.809792	1.760278

-4.7	411.4023	1.772039	26.7663 6	0.05767 3	6.621202	1.527973
-4.6	410.5876	1.12446	26.7398 8	0.03661 2	7.324621	0.969169
-4.5	412.3206	1.751661	26.7962 2	0.05692 8	5.828612	1.512594
-4.4	409.0825	4.687915	26.6904 2	0.15312 3	8.609449	4.027401
-4.3	409.5313	3.646308	26.7052 2	0.11890 7	8.227985	3.137784
-4.2	410.0283	3.91117	26.7213 9	0.12776 6	7.798962	3.35972
-4.1	404.0356	5.145961	26.5251 6	0.16916 8	12.93425	4.391698
-4	404.2842	2.60299	26.5337 2	0.08548 5	12.73252	2.223736
-3.9	408.3576	2.813	26.6670 3	0.09194 6	9.240268	2.414936
-3.8	401.1428	6.152346	26.4297 9	0.20345 6	15.39565	5.217981
-3.7	397.7046	6.066042	26.3163	0.20010 9	18.31739	5.158131
-3.6	398.1809	6.048329	26.3320 6	0.19995 7	17.91352	5.131407
-3.5	398.5399	6.829807	26.3437 2	0.22517 6	17.60349	5.811059
-3.4	389.6337	11.69199	26.0457	0.39403 3	25.06254	9.717326
-3.3	392.4781	5.087697	26.1430 2	0.16916 6	22.73799	4.290294
-3.2	375.563	12.4713	25.5705 4	0.42165 3	36.73023	10.32821
-3.1	380.0714	4.017949	25.7266 7	0.13593 1	33.09666	3.325108
-3	384.6627	8.343897	25.8804 5	0.28036 4	29.25526	6.957018
-2.9	373.4021	5.111678	25.4997 1	0.17505 8	38.57994	4.172916
-2.8	373.264	5.07913	25.495	0.17387	38.69324	4.148259
-2.7	360.7468	16.31051	25.0581 2	0.56607 9	48.68966	13.11329
-2.6	357.8263	13.63311	24.9583 2	0.47465 8	51.07956	10.92014
-2.5	351.9993	4.736744	24.7581 5	0.16656 8	55.81962	3.749296
-2.4	345.544	11.68648	24.5271 1	0.4175	60.82008	9.074316
-2.3	340.6352	9.616254	24.3533 4	0.34486 5	64.67453	7.430528

-2.2	343.9836	14.26162	24.4699 5	0.5086	61.99318	11.09711
-2.1	340.5592	11.46604	24.3495 8	0.41269 3	64.70524	8.819403
-2	327.607	9.381991	23.8830 1	0.34386 2	74.65695	7.050326
-1.9	329.7957	7.690484	23.9635 1	0.27866 1	73.02012	5.865256
-1.8	315.8286	12.1963	23.4478 3	0.45243 9	83.4128	9.018433
-1.7	303.5255	10.11369	22.9876	0.38671 5	92.40574	7.16726
-1.6	295.9517	12.04821	22.6975 7	0.45914 9	97.76035	8.579396
-1.5	295.5237	7.08087	22.6841 3	0.27261 9	98.1425	4.967052
-1.4	282.9374	11.72516	22.1925 9	0.46471 2	106.7826	7.869161
-1.3	259.8156	11.20553	21.2662 2	0.45678 3	122.0238	7.17781
-1.2	256.8951	12.22182	21.1453 7	0.49866 1	123.845	7.815869
-1.1	268.8807	9.157566	21.6358 8	0.36785 3	116.2232	6.011963
-1	227.0832	9.435787	19.8818 1	0.41459 9	141.6277	5.234137
-0.9	238.2955	14.18571	20.3623	0.60237 6	135.0817	8.434137
-0.8	213.489	13.57148	19.2720 4	0.61253 5	148.8291	7.094464
-0.7	218.453	13.91068	19.4946 6	0.62440 7	146.1982	7.364201
-0.6	207.6343	18.78814	18.9962 4	0.85881	151.5744	9.547356
-0.5	200.6818	30.18057	18.6413 5	1.41417 2	154.0949	14.40587
-0.4	189.0691	10.64322	18.1384 1	0.50735 7	160.7316	4.835232
-0.3	176.8074	18.50986	17.5241 7	0.90273 6	165.492	7.873456
-0.2	189.725	20.76561	18.1505 9	0.98218 9	159.9184	9.702806
-0.1	164.4767	12.66157	16.9124	0.63604 6	170.4393	4.884971
0	166.6653	15.91004	17.0170 7	0.81691 3	169.4553	5.676301
0.1	171.8572	19.39368	17.2730 9	0.96565 5	167.3299	7.715035
0.2	171.0494	16.37589	17.2394 2	0.82775 8	167.8272	6.19537

0.3	172.9135	17.11131	17.3324 7	0.84564 5	167.0943	6.991442
0.4	182.7174	11.96561	17.8284 9	0.58628 7	163.4209	5.013201
0.5	198.4863	15.97657	18.5771 6	0.74224 7	156.1844	7.801794
0.6	201.7728	14.30378	18.7333 7	0.66703 1	154.6809	6.906156
0.7	220.4069	10.7987	19.5857 2	0.48185 1	145.2555	5.790883
0.8	213.2336	16.60025	19.2559	0.74428 4	148.8379	8.809981
0.9	233.939	8.333399	20.1808 3	0.36205 1	137.7663	4.733264
1	224.9705	12.79912	19.7852 6	0.56932 2	142.6986	6.918604
1.1	259.5325	11.35201	21.2543 8	0.46825 8	122.1969	7.120378
1.2	267.7622	15.90238	21.584	0.65795 6	116.7694	9.927386
1.3	285.1468	9.131154	22.2810 5	0.35789 2	105.3249	6.234203
1.4	282.6959	11.83473	22.1831 6	0.46222 9	106.9486	8.124606
1.5	290.5665	20.82949	22.4801 3	0.81275 8	101.2646	14.32968
1.6	304.1469	14.21644	23.0080 7	0.54022 7	91.87641	10.16666
1.7	305.8937	8.839517	23.0779 6	0.33285	90.72263	6.402773
1.8	318.0517	10.01716	23.5316 5	0.37116 8	81.80559	7.418314
1.9	339.4684	18.94536	24.3046 3	0.67857 5	65.39069	14.66468
2	337.2175	8.518075	24.2313 3	0.30841 2	67.3301	6.502669
2.1	329.7473	9.298052	23.961	0.33719 5	73.03675	7.083511
2.2	343.2794	7.175902	24.4487 9	0.25563 7	62.64803	5.591046
2.3	356.991	8.940813	24.9316 4	0.31650 8	51.81369	7.020405
2.4	348.3125	3.827085	24.6283 3	0.13542 6	58.73322	3.00634
2.5	363.1356	10.28482	25.1448	0.35652 4	46.87113	8.27995
2.6	347.8568	7.601864	24.6111 3	0.26833 2	59.06233	5.990056
2.7	371.5656	8.241561	25.4359 6	0.28246 5	40.05617	6.722034

2.8	376.6677	11.60402	25.6085 3	0.39637 2	35.83271	9.501097
2.9	374.6103	14.90588	25.5365 1	0.50886 3	37.4699	12.21326
3	380.1336	6.401368	25.7282 2	0.21699 2	33.03038	5.286044
3.1	383.7513	7.690465	25.8499 8	0.25932 1	30.01942	6.387513
3.2	383.0126	9.016735	25.8246 1	0.30369 4	30.62045	7.49856
3.3	390.8557	6.856828	26.0884 7	0.22883 3	24.08996	5.759451
3.4	400.7217	5.850854	26.4159 9	0.19240 8	15.75636	4.991454
3.5	398.7816	6.464702	26.3518	0.21459 7	17.40076	5.461058
3.6	403.4556	7.795892	26.5054 1	0.25743 4	13.41081	6.622175
3.7	402.351	6.994475	26.4693 4	0.23066 3	14.36011	5.949597
3.8	404.6501	5.22614	26.5453 1	0.17125 7	12.40855	4.474864
3.9	402.7653	4.72755	26.4835 1	0.15536 8	14.02141	4.035791
4	406.0585	6.043617	26.5912 8	0.19844 5	11.19765	5.164
4.1	408.7166	3.453789	26.6786 7	0.11280 4	8.929501	2.967401
4.2	411.3816	2.236905	26.7656 5	0.07278 7	6.638058	1.929218
4.3	412.4725	1.82932	26.8011 5	0.05945 9	5.697223	1.579477
4.4	410.6567	1.747732	26.7420 9	0.05690 4	7.264165	1.50641
4.5	411.2158	3.149432	26.7601 6	0.1025	6.778426	2.715705
4.6	412.9488	1.346472	26.8166 5	0.04370 6	5.286457	1.164163
4.7	412.1618	1.011154	26.7911	0.03287 8	5.966803	0.872724
4.8	410.5048	1.196133	26.7371 8	0.03892 9	7.39591	1.031411
4.9	412.7348	1.113039	26.8097 1	0.03615 7	5.471734	0.961588
5	410.5462	1.13647	26.7385 3	0.03702 5	7.360295	0.978934
5.1	410.8706	1.25649	26.7490 9	0.04087 9	7.080511	1.083818
5.2	412.217	1.167381	26.7928 8	0.03793 8	5.918965	1.008105



5.3	409.4001	1.150189	26.7011 8	0.03751 5	8.347242	0.989578
5.4	412.5484	1.928013	26.8036 1	0.06260 7	5.631444	1.666311
5.5	414.4885	1.762927	26.8665 7	0.05718 5	3.953765	1.525276
5.6	413.722	1.04366	26.8417 6	0.03385 4	4.618212	0.902956
5.7	413.0525	1.658395	26.82	0.05384 3	5.196387	1.433528
5.8	413.0938	1.00172	26.8213 7	0.03252 4	5.161527	0.865864
5.9	411.7268	0.710488	26.7769 7	0.02310 4	6.342558	0.613168
6	412.2308	1.646368	26.7933 1	0.05353 5	5.906289	1.4209
6.1	414.806	1.224243	26.8768 9	0.03963 5	3.679596	1.061266
6.2	413.6737	0.803891	26.8402	0.02608 4	4.660242	0.695314
6.3	413.2733	1.06528	26.8271 9	0.03458 3	5.006326	0.920917
6.4	412.9419	0.64684	26.8164 5	0.02100 3	5.293177	0.559083
6.5	413.6323	1.534244	26.8388 2	0.04974 1	4.695195	1.328135
6.6	412.9557	0.845296	26.8168 9	0.02743 6	5.281068	0.730898
6.7	413.3079	0.741658	26.8283 3	0.02407	4.976707	0.641357
6.8	414.661	1.925709	26.8721 5	0.06238 3	3.804016	1.668337
6.9	415.4274	1.359938	26.8970 1	0.04400 2	3.140905	1.179613
7	413.5564	0.715072	26.8363 9	0.02319 4	4.761813	0.618699

740 RPM						
Avg y position	Avg model pressure	STD Pressure	Avg $U_{\infty}$	STD $U_{\infty}$	Avg $U_{\infty}(U_{\infty\max}-U_{\infty})$	STD $U_{\infty}(U_{\infty\max}-U_{\infty})$
-7	559.102	0.910804	31.20343	0.025418	1.755879	0.791559
-6.9	560.9799	1.727258	31.25576	0.048123	0.121462	1.503635
-6.8	560.3102	2.44882	31.23706	0.068277	0.703228	2.130219
-6.7	556.9203	1.997705	31.14245	0.05584	3.649031	1.733392
-6.6	559.3782	2.0744	31.21109	0.057876	1.514461	1.803314
-6.5	561.1248	3.049055	31.25972	0.084919	-0.00714	2.655261
-6.4	559.1849	2.937906	31.20565	0.081817	1.680867	2.558676
-6.3	555.9675	2.81124	31.11575	0.078714	4.473623	2.435095
-6.2	556.1402	1.59679	31.12065	0.044699	4.326082	1.383481
-6.1	555.9054	2.258474	31.11405	0.063202	4.528555	1.957385
-6	555.4635	1.316205	31.10172	0.036843	4.912752	1.140425
-5.9	556.0296	1.765043	31.11755	0.049411	4.421671	1.52919
-5.8	553.0885	2.855414	31.03508	0.080119	6.965527	2.468095
-5.7	557.0101	2.508937	31.14493	0.070117	3.570278	2.177389
-5.6	555.9123	0.858566	31.1143	0.024029	4.524273	0.744006
-5.5	554.2967	2.602448	31.06897	0.072885	5.921102	2.253695
-5.4	554.0965	1.578998	31.06342	0.044258	6.096017	1.366278
-5.3	551.6732	1.550091	30.99542	0.043549	8.190421	1.338101
-5.2	550.5133	1.838989	30.9628	0.051721	9.190849	1.585748
-5.1	552.7019	2.306861	31.02426	0.064783	7.300758	1.99223
-5	551.2658	2.356423	30.98393	0.066256	8.540799	2.032484
-4.9	553.1644	1.421862	31.03729	0.039907	6.902279	1.228624
-4.8	552.3014	1.299341	31.01307	0.036476	7.64816	1.122523

-4.7	550.1956	1.7922	30.9538 7	0.05042 2	9.464829	1.544874
-4.6	554.8145	2.314909	31.0835	0.06481 8	5.473424	2.005133
-4.5	548.7044	2.861173	30.9118 3	0.08058 1	10.74755	2.463694
-4.4	547.3374	3.271792	30.8732 7	0.09234 4	11.92271	2.811043
-4.3	548.7596	4.244639	30.9132 6	0.11983 8	10.69612	3.64578
-4.2	546.9852	6.449602	30.8629 4	0.18232 7	12.21304	5.53229
-4.1	547.441	6.729556	30.8757 4	0.19043 6	11.81974	5.766381
-4	540.0052	7.004062	30.6652 8	0.19875	18.18976	5.984506
-3.9	541.7796	8.200214	30.7153 8	0.23280 9	16.66595	7.002898
-3.8	543.7955	12.00991	30.7714 8	0.34088 2	14.9089	10.25915
-3.7	533.4394	6.84609	30.4782 9	0.19595 9	23.7787	5.796689
-3.6	526.6319	10.94145	30.2821 8	0.31594 7	29.50326	9.177978
-3.5	534.5579	12.26259	30.5088 5	0.35155 4	22.78604	10.36569
-3.4	523.4423	16.43902	30.1882 4	0.47659 1	32.12132	13.7304
-3.3	519.1755	5.450486	30.0682 5	0.15739 7	35.80095	4.571647
-3.2	513.1275	10.3597	29.8914 8	0.30326 1	40.80767	8.561523
-3.1	517.0283	8.119888	30.0054 9	0.23645 7	37.57843	6.749002
-3	503.7586	10.96039	29.6171 1	0.32268 1	48.54639	9.000691
-2.9	498.691	8.563027	29.4684 2	0.25305	52.72344	7.002088
-2.8	496.8614	5.731074	29.4149	0.16948 7	54.23672	4.682416
-2.7	484.3028	10.32548	29.0396 2	0.31024 8	64.37567	8.283556
-2.6	456.6312	9.018745	28.1980 3	0.27814 3	86.25704	7.011567
-2.5	472.7177	13.53958	28.6888 8	0.41208 7	73.58656	10.69765
-2.4	459.7449	10.95719	28.2933 9	0.33650 3	83.81547	8.563138
-2.3	442.3051	13.86804	27.7500 8	0.43833 6	97.20255	10.44879

-2.2	454.3045	9.263181	28.1260 1	0.28648 3	88.05752	7.176284
-2.1	447.4141	7.423311	27.9123 8	0.23249 6	93.37874	5.659913
-2	436.8646	11.9765	27.5797 5	0.37627 4	101.3525	9.094877
-1.9	421.4063	8.332812	27.0885 9	0.26804 6	112.9189	6.132344
-1.8	422.9943	5.56634	27.1403 1	0.17972 4	111.7702	4.075517
-1.7	415.9383	6.235711	26.9128 3	0.20146	116.947	4.561811
-1.6	390.904	12.95125	26.0875	0.43408 5	134.7438	8.986377
-1.5	377.9726	8.301091	25.6543 5	0.28251 2	143.7232	5.625065
-1.4	382.0529	19.11766	25.7860 2	0.64471 4	140.7334	13.1422
-1.3	355.5411	11.12523	24.8799 6	0.38745 8	158.5796	7.263365
-1.2	348.2987	12.29315	24.6244 3	0.43371	163.2041	7.852806
-1.1	328.0351	18.12219	23.8921 2	0.65687 7	175.6005	11.02955
-1	312.7633	13.42951	23.3328 1	0.49759 7	184.712	7.83435
-0.9	303.6291	12.05796	22.9902 5	0.45732 4	189.9103	6.704627
-0.8	298.7341	14.06775	22.8023 5	0.53818 5	192.5612	7.67832
-0.7	288.4953	18.41119	22.4031 1	0.71352 8	197.9116	9.762772
-0.6	265.2836	15.46626	21.4846 9	0.62715	209.6242	7.334938
-0.5	270.6965	12.15965	21.7066 2	0.48220 3	207.1354	6.107789
-0.4	261.3621	17.9493	21.3217	0.73671 1	211.3582	8.251894
-0.3	227.815	10.87359	19.9125 2	0.47445 4	225.7286	4.106253
-0.2	235.1403	19.74786	20.2182 6	0.84679 3	222.5293	7.928122
-0.1	254.3337	28.77382	21.0116 7	1.19862 8	213.9064	12.70367
0	236.0171	24.00574	20.2468	1.04534	221.8946	9.170396
0.1	246.8497	17.16847	20.7213 4	0.71448 9	217.8641	7.57106
0.2	232.0542	17.07219	20.0887 3	0.74971 1	223.8546	6.310909

0.3	262.7498	21.44785	21.3733 5	0.86970 2	210.5561	10.17916
0.4	248.2167	18.59451	20.7764 3	0.77842 2	217.2055	8.065135
0.5	252.366	19.0522	20.9492 1	0.78896 8	215.3808	8.537842
0.6	285.6577	12.43082	22.2985 4	0.48927 2	199.5843	6.354145
0.7	266.485	15.95577	21.5325 3	0.65417 8	209.0274	7.348015
0.8	290.1385	17.47043	22.4681 6	0.67197 6	197.0833	9.431922
0.9	304.4991	9.668854	23.0248 5	0.36171 2	189.4771	5.532222
1	331.0315	13.03449	24.0052 1	0.48047 9	173.9176	7.68158
1.1	335.8437	15.07702	24.1778	0.54370 9	170.9326	9.264479
1.2	360.4775	15.55332	25.0492 3	0.54481 2	155.2742	10.05742
1.3	373.6713	8.865022	25.5077 2	0.30235 1	146.63	5.987085
1.4	370.7854	13.72549	25.4065 1	0.46928 3	148.4917	9.234298
1.5	399.7136	18.66441	26.3763 5	0.61479 2	128.4314	13.29047
1.6	399.0577	21.68898	26.3521 4	0.71681 6	128.8167	15.36788
1.7	415.2617	8.219308	26.8903 7	0.26676 4	117.4231	5.974866
1.8	409.3725	12.962	26.6970 2	0.42091 2	121.6351	9.416299
1.9	435.6357	10.12906	27.5416 1	0.32167 2	102.3003	7.584476
2	452.7511	20.3849	28.0723 1	0.6307	89.08414	15.7862
2.1	436.9682	12.64849	27.5826 8	0.40116 3	101.2635	9.487517
2.2	468.0851	8.726333	28.5496 4	0.26594 8	77.30176	6.883315
2.3	462.1406	15.44061	28.3650 5	0.47601 2	81.88331	12.00982
2.4	468.0022	17.19204	28.5436	0.52304 9	77.25707	13.58992
2.5	492.284	13.54948	29.2768 6	0.40083 9	57.89292	11.06643
2.6	483.9231	12.05832	29.0276 5	0.36129 7	64.66266	9.70543
2.7	495.9017	8.549346	29.3858 8	0.25398	55.00063	6.949342

2.8	477.813	14.80082	28.8425 2	0.45195 5	69.51609	11.64813
2.9	503.5584	8.182418	29.612	0.24050 3	48.73516	6.73142
3	503.4962	7.187306	29.6103 9	0.21134 4	48.7932	5.909884
3.1	523.5941	11.36664	30.1945 6	0.32946 1	32.05459	9.496257
3.2	523.1315	6.192652	30.1824 8	0.17859 2	32.48238	5.201671
3.3	530.2428	7.814404	30.3866 4	0.22395 4	26.4804	6.60793
3.4	529.0484	9.199463	30.3520 8	0.26366 9	27.48006	7.778393
3.5	525.5066	18.12157	30.2469 5	0.52386 8	30.36166	15.18254
3.6	538.7487	4.356509	30.6299 7	0.12377 2	19.27413	3.717619
3.7	532.3969	11.26772	30.4474 1	0.32408 9	24.62884	9.491805
3.8	541.9384	6.542706	30.7202	0.18596 1	16.54004	5.580833
3.9	545.2178	8.512704	30.8126 3	0.24150 7	13.71839	7.27517
4	542.8359	4.040287	30.7459 8	0.11445 1	15.78271	3.458329
4.1	548.5249	4.841923	30.9065 8	0.13639	10.89606	4.168529
4.2	553.0954	2.843339	31.0352 7	0.07982	6.959562	2.456408
4.3	552.0875	1.822536	31.0070 4	0.05123 9	7.832342	1.572148
4.4	550.1888	3.446644	30.9535 7	0.09688 1	9.467273	2.973723
4.5	549.4431	5.281397	30.9323 8	0.14917 1	10.10346	4.534346
4.6	553.8825	0.889289	31.0574 4	0.02493 6	6.281794	0.769157
4.7	551.7492	1.893979	30.9975 4	0.05320 5	8.124365	1.635112
4.8	548.4972	3.320548	30.9059 6	0.09354 4	10.92478	2.858443
4.9	552.7156	0.875661	31.0247 1	0.02457 8	7.290664	0.75663
5	551.9217	2.020254	31.0023 8	0.05674 7	7.975161	1.744313
5.1	553.8618	1.705824	31.0568 3	0.04781 5	6.298877	1.475956
5.2	551.3141	3.968284	30.9851 6	0.11145 5	8.495071	3.426564

5.3	552.7295	1.1767	31.0250 9	0.03303 9	7.278471	1.016393
5.4	552.0598	1.36307	31.0062 8	0.03828 2	7.856786	1.177046
5.5	553.1783	2.593733	31.0376 2	0.07286	6.888428	2.239294
5.6	551.1415	1.32636	30.9804 9	0.03726 7	8.649528	1.144853
5.7	550.0438	1.089408	30.9496 2	0.03065 2	9.596511	0.938987
5.8	553.1852	1.491201	31.0378 6	0.04181 8	6.884279	1.289648
5.9	554.7041	1.966824	31.0804 3	0.05511 6	5.56959	1.702231
6	552.6536	2.118156	31.0229 2	0.05940 9	7.342861	1.831567
6.1	556.5268	1.217336	31.1314 8	0.03404 1	3.991326	1.055827
6.2	553.3094	1.355768	31.0413 6	0.03802 6	6.776997	1.172342
6.3	554.5728	1.930795	31.0767 5	0.05412 6	5.683274	1.670454
6.4	554.7317	0.953326	31.0812 4	0.02670 6	5.546889	0.825366
6.5	556.8167	1.950837	31.1395 6	0.05456 3	3.73897	1.691673
6.6	555.284	1.856701	31.0966 7	0.05201 2	5.067596	1.607479
6.7	554.8352	1.718265	31.0841 1	0.04815 1	5.456412	1.487102
6.8	555.8985	1.526291	31.1138 9	0.04273 4	4.535615	1.322118
6.9	556.4577	2.316354	31.1295	0.06475 5	4.04971	2.009607
7	553.7997	2.205012	31.0550 7	0.06176 2	6.351871	1.909297

340 RPM - 18cm						
Avg y position	Avg model pressure	STD Pressure	Avg $U_{\infty}$	STD $U_{\infty}$	Avg $U_{\infty}(U_{\infty\max}-U_{\infty})$	STD $U_{\infty}(U_{\infty\max}-U_{\infty})$
-7	111.0389	0.155306	13.90575	0.009722	1.752542	0.134039
-6.9	111.1493	0.355807	13.91265	0.022261	1.657031	0.307266
-6.8	110.9353	0.316178	13.89925	0.019807	1.841768	0.272684
-6.7	111.3426	0.632232	13.9247	0.039506	1.489612	0.546663
-6.6	110.9353	0.221204	13.89926	0.013848	1.841911	0.190912
-6.5	111.0734	0.277196	13.9079	0.017374	1.722659	0.23894
-6.4	111.0044	0.37979	13.90357	0.023809	1.782102	0.327305
-6.3	110.597	0.390598	13.87803	0.024526	2.13322	0.336075
-6.2	110.7557	0.317709	13.888	0.019952	1.996554	0.273317
-6.1	110.1827	0.385673	13.85202	0.024216	2.489569	0.331836
-6	110.0101	0.291463	13.84117	0.018335	2.637976	0.250302
-5.9	110.1482	0.382842	13.84985	0.024078	2.519251	0.32884
-5.8	110.5625	0.302745	13.87588	0.018988	2.163055	0.260783
-5.7	110.1137	0.340558	13.84768	0.021397	2.548965	0.292834
-5.6	110.2242	0.281443	13.85464	0.017664	2.454048	0.242265
-5.5	109.8168	0.325749	13.829	0.020498	2.803882	0.279662
-5.4	110.0515	0.501309	13.84375	0.031518	2.602101	0.430754
-5.3	109.3542	0.226925	13.79985	0.014321	3.200445	0.194231
-5.2	109.727	0.363288	13.82335	0.022882	2.880839	0.311583
-5.1	109.3474	0.585375	13.79938	0.036961	3.205727	0.50078
-5	109.2507	0.466709	13.7933	0.029459	3.288723	0.39939
-4.9	109.2507	0.724604	13.79325	0.045724	3.288107	0.620288
-4.8	109.3887	0.414249	13.80201	0.026132	3.170679	0.354723



-4.7	109.5406	0.752582	13.8115 4	0.04749 8	3.039782	0.644109
-4.6	109.5752	0.599727	13.8137 5	0.03778 7	3.010562	0.514186
-4.5	110.0584	0.952647	13.8441	0.05990 1	2.594871	0.818483
-4.4	109.0849	0.73832	13.7827 8	0.04662 8	3.429838	0.63149
-4.3	109.3819	0.511862	13.8015 7	0.03228 1	3.176344	0.43843
-4.2	109.727	0.709041	13.8232 9	0.04466	2.8801	0.608101
-4.1	109.4371	0.572588	13.8050 5	0.03612	3.128886	0.490318
-4	109.4164	0.582012	13.8037 4	0.03671	3.14664	0.498446
-3.9	110.0171	0.617716	13.8415 7	0.03886 7	2.631438	0.530359
-3.8	109.1817	1.01472	13.7888 2	0.06414 8	3.346137	0.866998
-3.7	109.3405	1.822965	13.7985 2	0.11533 3	3.205606	1.556332
-3.6	109.7547	1.086565	13.8249 4	0.06846 1	2.855026	0.931584
-3.5	109.1057	1.382237	13.7838 9	0.08752 5	3.409347	1.178988
-3.4	107.3245	1.936272	13.6706 4	0.12371 4	4.922015	1.636073
-3.3	108.2703	1.076675	13.7311 3	0.06823 4	4.123712	0.917549
-3.2	107.8353	2.219868	13.7029 7	0.14095 7	4.486092	1.887979
-3.1	103.8792	2.52012	13.4489 9	0.16333 8	7.81164	2.096847
-3	102.8022	4.155234	13.3773 2	0.27233 6	8.6816	3.415335
-2.9	103.9138	2.961295	13.4508 2	0.19418 1	7.777155	2.432451
-2.8	102.4156	2.986764	13.3534 7	0.19514 7	9.020167	2.463218
-2.7	103.396	4.837755	13.4149 6	0.31609 5	8.175758	3.989608
-2.6	95.84289	4.820431	12.9151 9	0.32496 9	14.31651	3.835471
-2.5	101.4076	5.065954	13.2847 9	0.33599 4	9.811917	4.108563
-2.4	96.93372	3.663712	12.9902 2	0.24712 1	13.4697	2.913134
-2.3	94.28943	3.794876	12.8115 1	0.25948 7	15.56695	2.96783

-2.2	89.05618	4.303419	12.4498 3	0.30078 5	19.6055	3.275504
-2.1	88.06883	4.379301	12.3803 6	0.31013 3	20.35007	3.275862
-2	85.2727	3.286951	12.1837 8	0.23472	22.46114	2.430772
-1.9	84.4511	4.031807	12.1237 4	0.29015 4	23.04936	2.950231
-1.8	82.8355	4.409194	12.0065 1	0.31543 6	24.21799	3.253939
-1.7	80.861	3.770176	11.8634 4	0.27558 9	25.6489	2.699045
-1.6	75.09604	4.540385	11.4305 2	0.34828 3	29.61376	3.021606
-1.5	70.06985	2.932215	11.044	0.23373 7	32.94307	1.827516
-1.4	64.51205	4.72617	10.5923	0.38732 1	36.2836	2.796906
-1.3	64.38086	4.160446	10.5831 5	0.33879 7	36.38379	2.494075
-1.2	55.73693	2.947371	9.84878 4	0.25661 5	41.13231	1.533419
-1.1	55.10862	3.771433	9.79087 1	0.33088 8	41.41388	1.927065
-1	48.59112	4.173728	9.19046 9	0.39549	44.33914	1.722012
-0.9	52.57479	4.840992	9.55849 1	0.44066 2	42.56573	2.25934
-0.8	42.1427	3.180465	8.56080 1	0.32190 6	46.73344	1.025609
-0.7	45.33238	4.359737	8.87485 2	0.42828 1	45.58545	1.59153
-0.6	39.33962	6.125648	8.25166 1	0.65019 4	47.27712	1.580203
-0.5	36.21899	2.039184	7.93876 7	0.22463 8	48.32112	0.400368
-0.4	32.71169	5.595155	7.51673 8	0.68519 7	48.50712	0.540641
-0.3	36.23972	4.906276	7.92544 9	0.54803 2	48.09814	0.885866
-0.2	32.2491	4.328265	7.47750 8	0.49993 8	48.76224	0.56528
-0.1	32.93956	3.902257	7.56016 7	0.45709 8	48.71968	0.424516
0	30.99951	4.271947	7.32979 5	0.51105 1	48.86567	0.356522
0.1	28.67278	5.551051	7.03260 4	0.69268 9	48.74747	0.514063
0.2	34.43772	5.45317	7.71936 8	0.62225	48.34457	0.81925

0.3	38.44209	3.657736	8.17322 2	0.38120 8	47.73949	1.03139
0.4	38.68372	4.218163	8.19531 2	0.45291	47.62867	1.000507
0.5	42.18411	5.049446	8.55554 1	0.51711 5	46.58752	1.555701
0.6	41.16232	5.004662	8.45119 9	0.51232 5	46.90282	1.545407
0.7	43.64783	4.41956	8.70742 1	0.44021 4	46.16965	1.535322
0.8	47.70745	3.020172	9.11031	0.28945 3	44.75324	1.200622
0.9	59.09229	4.736216	10.1365 4	0.39899 5	39.32676	2.653654
1	60.88739	3.06955	10.2940 2	0.25866 3	38.41043	1.71672
1.1	64.75367	2.915883	10.6164 5	0.23978	36.20181	1.714278
1.2	67.18391	4.41628	10.8108 1	0.35482 2	34.69675	2.712838
1.3	66.70754	5.313374	10.7696	0.43141 4	34.94817	3.201375
1.4	73.01792	4.303036	11.2716 4	0.33043	31.00332	2.858392
1.5	80.63315	4.618766	11.8450 3	0.34059	25.78738	3.265423
1.6	77.62293	3.546328	11.6236	0.26456 9	27.92252	2.46384
1.7	81.48231	5.680015	11.9048 8	0.41690 3	25.14848	4.043124
1.8	87.95147	3.622296	12.3733 3	0.25570 4	20.45588	2.720848
1.9	85.01034	3.562037	12.1646	0.25587 7	22.6488	2.613108
2	90.09868	4.317947	12.5224 9	0.30240 2	18.80959	3.27735
2.1	97.09944	3.155161	13.0019 2	0.21349 3	13.34518	2.499217
2.2	96.58851	3.685338	12.9670 9	0.24581	13.74624	2.968984
2.3	95.40105	4.590365	12.8857 3	0.31034 2	14.6725	3.639717
2.4	99.35018	3.0027	13.1520 3	0.19766 3	11.53194	2.45581
2.5	102.6089	4.210017	13.3646 6	0.27577 8	8.840601	3.462236
2.6	100.6965	2.952819	13.2409	0.19473 4	10.43449	2.409879
2.7	105.1842	2.221799	13.5334 5	0.14251	6.724188	1.869616

2.8	108.3324	3.644558	13.73328	0.233345	4.045638	3.072783
2.9	107.9527	2.233236	13.71042	0.14195	4.386163	1.897301
3	107.8216	2.876741	13.70159	0.183783	4.490731	2.431112
3.1	108.7812	1.569537	13.76331	0.099112	3.685469	1.342578
3.2	109.3888	1.161592	13.80185	0.073257	3.16828	0.994953
3.3	109.2368	1.770634	13.792	0.111818	3.294718	1.514527
3.4	110.307	0.653919	13.85979	0.041101	2.382169	0.562059
3.5	109.0367	1.250533	13.77958	0.079406	3.469017	1.063555
3.6	110.0308	1.152416	13.8423	0.07228	2.617762	0.992679
3.7	110.3208	1.168726	13.86052	0.073451	2.368462	1.004656
3.8	110.3346	0.991748	13.86145	0.062149	2.357359	0.855029
3.9	110.1551	0.73784	13.85023	0.046389	2.512532	0.633994
4	110.9145	0.666453	13.8979	0.041696	1.859016	0.575534
4.1	110.3484	0.556893	13.86241	0.034999	2.346808	0.478706
4.2	110.7075	0.705742	13.88491	0.044231	2.037382	0.608385
4.3	110.9284	0.492673	13.8988	0.030833	1.847463	0.425328
4.4	110.6108	0.657134	13.87886	0.041269	2.12076	0.56529
4.5	110.8386	0.477944	13.89318	0.029914	1.924877	0.412571
4.6	110.1828	0.659298	13.85198	0.04143	2.488981	0.566807
4.7	111.1424	0.572054	13.91219	0.035765	1.662663	0.49436
4.8	110.1896	0.727105	13.8524	0.045734	2.482904	0.624492
4.9	110.6937	0.677066	13.88406	0.042464	2.04933	0.583247
5	110.9145	0.504405	13.89793	0.031587	1.859365	0.435185
5.1	111.6257	0.384843	13.94243	0.024018	1.245326	0.333178
5.2	111.46	0.605878	13.93205	0.037862	1.388158	0.523848

5.3	111.1907	0.79438	13.9151 7	0.04974 1	1.620311	0.685429
5.4	111.9088	0.854035	13.9600 2	0.05329 1	0.999087	0.739509
5.5	110.9284	0.707627	13.8987 6	0.04425 7	1.846959	0.611296
5.6	110.666	0.782863	13.8823	0.04911 1	2.072829	0.674213
5.7	110.7626	0.569677	13.8884	0.03571	1.990189	0.490994
5.8	111.4185	0.488477	13.9294 7	0.03050 2	1.424293	0.422669
5.9	111.0527	0.387885	13.9065 9	0.02429 9	1.740426	0.334524
6	111.9571	0.582396	13.9630 9	0.03631 8	0.957986	0.504621
6.1	111.8673	0.645741	13.9574 7	0.04024 7	1.035652	0.559802
6.2	112.2884	0.517554	13.9837 4	0.03227 8	0.670855	0.448385
6.3	111.6464	0.7228	13.9436 7	0.04512 4	1.226706	0.625554
6.4	112.0468	0.61551	13.9686 7	0.03831 6	0.880217	0.534245
6.5	111.7569	0.572193	13.9505 9	0.03571 3	1.131445	0.495333
6.6	112.4749	0.462849	13.9953 5	0.02881 6	0.509075	0.401696
6.7	111.8398	0.327595	13.9558	0.02046 8	1.060116	0.283295
6.8	112.0884	0.336019	13.9713	0.02091 9	0.8447	0.291627
6.9	112.2333	0.662794	13.9802 8	0.04123 2	0.718392	0.575676
7	113.0618	0.656954	14.0317 9	0.04073 7	-0.00164	0.572447

340 RPM - 36.8cm						
Avg y position	Avg model pressure	STD Pressure	Avg $U_\infty$	STD $U_\infty$	Avg $U_\infty(U_\infty\max-U_\infty)$	STD $U_\infty(U_\infty\max-U_\infty)$
-7	99.57108	0.290781	13.1681	0.01921 2	0.754999	0.252295
-6.9	99.35706	0.072423	13.1539 5	0.00479 3	0.940608	0.062728
-6.8	99.66093	0.077658	13.1740 5	0.00513 4	0.677255	0.067341
-6.7	99.26728	0.40076	13.1479 8	0.02657 7	1.017997	0.346421
-6.6	99.23285	0.397449	13.1457	0.02632	1.047809	0.344053
-6.5	99.39855	0.397498	13.1566 7	0.02630 3	0.904344	0.344363
-6.4	99.52969	0.340228	13.1653 6	0.02248 2	0.790808	0.295154
-6.3	99.17761	0.557918	13.1420 2	0.03695 5	1.095276	0.482852
-6.2	99.7368	0.411919	13.1790 4	0.02721 5	0.61108	0.357414
-6.1	99.06024	0.21677	13.1342 8	0.01437 4	1.197364	0.18739
-6	99.5711	0.212289	13.1681 1	0.01405 1	0.755062	0.183865
-5.9	100.082	0.904298	13.2017 2	0.05957 5	0.309883	0.786903
-5.8	99.61256	0.444082	13.1708 2	0.02935 8	0.718783	0.385077
-5.7	99.85419	0.466537	13.1867 9	0.03083 7	0.509094	0.404628
-5.6	99.28799	0.573398	13.1493 3	0.03795 8	0.999707	0.496541
-5.5	99.59876	0.694706	13.1698 6	0.04591 1	0.730133	0.602608
-5.4	99.52284	0.667875	13.1648 5	0.04424 6	0.796025	0.577901
-5.3	99.33635	0.514375	13.1525 4	0.03406 8	0.957973	0.445207
-5.2	98.87374	0.656419	13.1218 5	0.04359 8	1.357712	0.566528
-5.1	99.76446	0.69456	13.1808 2	0.04594 5	0.5864	0.601913
-5	99.24663	0.609121	13.1465 8	0.04034	1.035418	0.527252
-4.9	98.83933	0.246716	13.1196 3	0.01639 3	1.38825	0.212845
-4.8	98.01077	2.899093	13.0630 8	0.19578 6	2.083272	2.459467
-4.7	98.74262	1.022553	13.1130	0.06795	1.469582	0.882051

			4	1		
-4.6	98.82547	1.048312	13.1185 4	0.06966	1.397928	0.904315
-4.5	97.3549	1.500341	13.0203 6	0.10085 4	2.660453	1.278985
-4.4	97.87268	0.915962	13.0551 8	0.06108 1	2.219327	0.787286
-4.3	97.65179	1.475931	13.0402 1	0.09873 5	2.406026	1.264484
-4.2	94.48279	1.949617	12.8265 7	0.13243 4	5.09911	1.64374
-4.1	97.49302	1.79273	13.0294 3	0.11970 4	2.539952	1.538866
-4	97.00967	2.436773	12.9966 2	0.16326 6	2.947746	2.084342
-3.9	97.71396	2.17316	13.0439 4	0.14481 9	2.34702	1.869225
-3.8	94.8142	2.864057	12.8482 5	0.19518 4	4.808788	2.406344
-3.7	94.02715	3.606416	12.7939 3	0.24612 4	5.460996	3.02549
-3.6	94.97294	3.126241	12.8587	0.21483 6	4.670457	2.603252
-3.5	94.81417	3.311834	12.8477 8	0.22438 9	4.802565	2.799971
-3.4	93.32984	2.223682	12.7478 5	0.15149	6.065845	1.868982
-3.3	92.3839	1.909301	12.6833	0.13065 9	6.859501	1.596983
-3.2	92.33564	1.427886	12.6802 8	0.09788 2	6.903592	1.192126
-3.1	92.25964	1.758742	12.6748 6	0.12081 9	6.964316	1.464909
-3	90.86504	2.755076	12.5778 1	0.19226 2	8.109421	2.255425
-2.9	92.91556	2.975612	12.7188 1	0.20289 3	6.403261	2.49879
-2.8	90.01585	2.925349	12.5187 1	0.20368	8.80657	2.400689
-2.7	89.97441	3.522303	12.5151	0.24466 9	8.830997	2.89835
-2.6	87.4889	1.868343	12.3426 6	0.13238 8	10.8788	1.502847
-2.5	86.97797	3.108111	12.3053 2	0.22021 3	11.27469	2.500439
-2.4	86.66042	2.618971	12.2833 8	0.18639 3	11.53757	2.095881
-2.3	84.19567	2.770912	12.1072	0.19892 6	13.49983	2.19473

-2.2	86.71569	3.400349	12.28637	0.240466	11.48083	2.741602
-2.1	83.38787	1.738786	12.04994	0.1258	14.14928	1.364327
-2	83.17383	2.943627	12.03324	0.213587	14.30113	2.301621
-1.9	81.37878	3.675537	11.90151	0.269942	15.68492	2.831043
-1.8	78.15457	4.128955	11.66234	0.306374	18.1367	3.13959
-1.7	80.19122	3.258694	11.81495	0.239506	16.6083	2.507784
-1.6	72.99719	2.13892	11.27364	0.164873	21.97726	1.544487
-1.5	69.15849	4.914755	10.96754	0.389274	24.61387	3.412209
-1.4	71.15375	4.09244	11.12702	0.319299	23.24847	2.904923
-1.3	68.35072	3.154268	10.90718	0.253275	25.22239	2.144898
-1.2	71.14	5.14689	11.12326	0.40297	23.22262	3.636957
-1.1	64.68467	8.283559	10.59177	0.681908	27.43514	5.425408
-1	63.75952	3.341546	10.5337	0.277004	28.27828	2.155927
-0.9	59.03707	5.438981	10.12907	0.463521	31.15086	3.345302
-0.8	59.87248	4.715821	10.20315	0.403735	30.67575	2.873752
-0.7	59.08538	5.335325	10.13358	0.455546	31.12638	3.270815
-0.6	57.54579	4.858849	10.00207	0.417194	32.06827	2.949167
-0.5	48.44615	7.080173	9.162188	0.652453	36.80705	3.718076
-0.4	54.74276	4.910386	9.75346	0.452193	33.66161	2.578687
-0.3	52.91997	4.741963	9.590524	0.426343	34.68102	2.620281
-0.2	56.01995	5.915827	9.863366	0.522813	32.89099	3.395476
-0.1	50.9731	5.4516	9.407709	0.515137	35.6536	2.689057
0	52.93385	5.242064	9.589893	0.467346	34.6485	2.952077
0.1	56.82084	3.491175	9.942794	0.305104	32.54674	2.045914
0.2	48.8397	4.45133	9.212956	0.419119	36.79314	2.213371



0.3	54.43204	5.55798	9.72307 6	0.50562 3	33.80088	2.997297
0.4	51.76014	4.720988	9.48437 2	0.43227 6	35.2969	2.506834
0.5	54.24565	6.567896	9.70152 9	0.59208	33.84049	3.618431
0.6	54.47342	6.261392	9.72374 6	0.56151 2	33.73766	3.484265
0.7	60.57669	3.898572	10.2655 3	0.33461 2	30.27442	2.366802
0.8	67.27369	3.517304	10.8200 4	0.28641 1	25.94553	2.338595
0.9	58.60211	6.887509	10.0842 5	0.60403 1	31.31556	4.014562
1	66.58328	3.035765	10.7653 9	0.24334 7	26.42502	2.068789
1.1	69.46234	2.37357	10.9968 7	0.18770 8	24.47268	1.651262
1.2	71.65781	5.360986	11.1631 9	0.41751 3	22.84899	3.815744
1.3	68.47501	2.883594	10.9175 7	0.23179 1	25.14336	1.956504
1.4	74.50918	3.784124	11.3872 8	0.29262	20.84715	2.721021
1.5	72.62438	4.725655	11.2399 4	0.37093 9	22.1809	3.327881
1.6	75.75884	3.524373	11.4831	0.26505 9	19.93818	2.63317
1.7	77.62293	3.950671	11.6228 4	0.29623 4	18.54012	2.962588
1.8	79.79777	3.436094	11.7856 2	0.25391 9	16.90557	2.625781
1.9	83.87117	2.672302	12.0839 5	0.19246 2	13.75735	2.108504
2	85.24509	3.683652	12.1812 7	0.26170 3	12.65183	2.954431
2.1	84.06448	3.357073	12.0969 7	0.24294 6	13.59293	2.633775
2.2	82.18656	2.815042	11.9617 3	0.20558 4	15.07463	2.183466
2.3	84.00234	3.733469	12.0919 7	0.26798 6	13.63506	2.958077
2.4	87.37157	3.05583	12.3332	0.21649 2	10.95805	2.458613
2.5	87.83416	2.674461	12.3662 9	0.18742 9	10.59004	2.178905
2.6	89.71203	2.41713	12.4980 6	0.16955	9.062615	1.967019
2.7	88.86975	5.27362	12.4349 2	0.37065 6	9.694316	4.28298

2.8	89.51872	2.075692	12.4848 9	0.14516 9	9.225066	1.694909
2.9	92.5289	2.92501	12.6923 2	0.20253	6.726244	2.415369
3	91.25163	2.405719	12.6049 3	0.16537 4	7.794754	2.002404
3.1	93.28835	2.992854	12.7442 7	0.20532 1	6.090745	2.496686
3.2	94.62089	1.733149	12.8360 8	0.11729 7	4.984491	1.466939
3.3	92.31488	3.173781	12.6773 4	0.21965 6	6.90092	2.622191
3.4	93.17102	3.372795	12.7357 6	0.23396 1	6.182555	2.779717
3.5	92.6118	1.686403	12.6990 8	0.11542 3	6.671354	1.410309
3.6	94.62776	1.535443	12.8366 6	0.10400 7	4.980184	1.29839
3.7	93.83382	2.141747	12.7822 9	0.14600 6	5.643678	1.798928
3.8	93.74402	3.190951	12.7751 6	0.21752 7	5.705818	2.680419
3.9	97.11325	2.185119	13.0037 5	0.14695 8	2.861665	1.861769
4	96.00864	2.731339	12.9291 1	0.18380 6	3.798118	2.325749
4.1	97.51372	2.720023	13.0300 9	0.18276 3	2.51261	2.319912
4.2	98.38359	1.959408	13.0887 1	0.13112 6	1.772947	1.678071
4.3	97.33419	1.439504	13.0190 1	0.09608 3	2.67867	1.236113
4.4	96.87163	1.673256	12.9879 1	0.11225 7	3.072868	1.42929
4.5	98.10745	1.465772	13.0706 1	0.09817	2.014488	1.254271
4.6	99.03944	1.490561	13.1325 4	0.0991	1.210562	1.285133
4.7	100.013	0.974992	13.1971 4	0.06440 2	0.36961	0.846173
4.8	99.6332	1.211188	13.1719 8	0.07985 3	0.698151	1.053162
4.9	99.4123	0.649792	13.1575 4	0.04304 3	0.891852	0.562322
5	99.03949	1.44597	13.1325 7	0.09584 1	1.210835	1.250571
5.1	99.24663	1.183373	13.1464 1	0.07870 4	1.033144	1.019907
5.2	99.1707	0.723228	13.1415 3	0.04779	1.10079	0.627438

5.3	99.14997	0.904423	13.1401	0.05986 8	1.118078	0.783243
5.4	98.70811	0.549054	13.1108 8	0.03648 2	1.501012	0.473668
5.5	99.63322	0.650523	13.1721 5	0.04298 2	0.70038	0.56441
5.6	100.1924	0.504015	13.2090 9	0.03332 6	0.215123	0.436975
5.7	100.441	0.562749	13.2254 6	0.03705 5	-0.00136	0.489932
5.8	99.64015	0.849749	13.1725 6	0.05603 1	0.693731	0.738773
5.9	100.3168	0.46957	13.2172 9	0.03091 1	0.107014	0.408929
6	99.9785	0.406354	13.195	0.02680 1	0.40125	0.353192
6.1	99.59881	0.279653	13.1699 3	0.01850 4	0.730967	0.242278
6.2	100.0406	0.433349	13.1990 9	0.02860 4	0.347271	0.376359
6.3	99.99228	0.178399	13.1959 3	0.01177 5	0.389567	0.154949
6.4	99.42618	0.585823	13.1584 7	0.03873 5	0.880004	0.507897
6.5	99.68161	0.413755	13.1753 9	0.02734 6	0.658958	0.358875
6.6	99.99921	0.184057	13.1963 9	0.01214 4	0.383544	0.159919
6.7	99.96472	0.286845	13.1941	0.01889 7	0.413399	0.249604
6.8	99.95089	0.112069	13.1932	0.00739 6	0.425562	0.097345
6.9	99.97162	0.408159	13.1945 5	0.02689 8	0.407222	0.35505
7	100.227	0.369793	13.2113 9	0.02438 1	0.185277	0.32153

140 RPM - 36.8cm						
Avg y position	Avg model pressure	STD Pressure	Avg $U_{\infty}$	STD $U_{\infty}$	Avg $U_{\infty}(U_{\infty\max}-U_{\infty})$	STD $U_{\infty}(U_{\infty\max}-U_{\infty})$
-7	14.29155	0.05383	4.98879 7	0.00939 5	0.19742	0.046499
-6.9	14.35374	0.020811	4.99964 8	0.00362 8	0.143674	0.017999
-6.8	14.35374	0.020811	4.99964 8	0.00362 8	0.143674	0.017999
-6.7	14.46418	0.046534	5.01883 9	0.00806 7	0.047858	0.040474
-6.6	14.34684	0.051911	4.99843 9	0.00904	0.149615	0.044944
-6.5	14.25701	0.046646	4.98276 8	0.00815 8	0.227245	0.040211
-6.4	14.36065	0.031023	5.00084 8	0.00540 2	0.13769	0.026864
-6.3	14.25006	0.034106	4.98155 6	0.00596	0.233258	0.029426
-6.2	14.32608	0.064036	4.99481 8	0.01116 8	0.167551	0.05536
-6.1	14.40206	0.033984	5.00805 3	0.00591	0.1018	0.029463
-6	14.40206	0.063578	5.00804 5	0.01105 3	0.101757	0.05514
-5.9	14.33994	0.054179	4.99723 6	0.00943 5	0.155584	0.046907
-5.8	14.41586	0.041621	5.01045 1	0.00723 3	0.089818	0.036114
-5.7	14.38135	0.062432	5.00444 4	0.01086	0.119709	0.054113
-5.6	14.32611	0.063996	4.99482 2	0.01115 1	0.16753	0.055372
-5.5	14.38135	0.031789	5.00445 2	0.00552 8	0.119753	0.02756
-5.4	14.45727	0.083243	5.01762 7	0.01444 1	0.053784	0.072351
-5.3	14.51939	0.098347	5.02838 7	0.01703 4	-0.00029	0.085617
-5.2	14.46418	0.071082	5.01883	0.01233 2	0.047815	0.061775
-5.1	14.17414	0.167287	4.96818 5	0.02941 3	0.298241	0.143425
-5	14.34684	0.051911	4.99843 9	0.00904	0.149615	0.044944
-4.9	14.42967	0.07599	5.01283 7	0.0132	0.077778	0.065961
-4.8	14.47798	0.031789	5.02123 7	0.00551 5	0.035875	0.027627

-4.7	13.89103	0.384837	4.91793 4	0.06831 9	0.538584	0.326648
-4.6	14.00149	0.407945	4.93739 1	0.07260 3	0.444066	0.34535
-4.5	14.29155	0.198747	4.98868 6	0.03480 5	0.19686	0.171102
-4.4	14.29848	0.048637	4.99000 8	0.00848 8	0.191444	0.042019
-4.3	14.0429	0.263602	4.94499 9	0.04668 4	0.4102	0.22431
-4.2	14.16726	0.317733	4.96674 8	0.05644 3	0.302993	0.269511
-4.1	13.8013	0.421496	4.90192 3	0.07510 8	0.614334	0.356361
-4	13.60802	0.411013	4.86748 2	0.07423 5	0.777749	0.342491
-3.9	13.31112	0.440846	4.81397 8	0.08056 5	1.025735	0.36266
-3.8	13.61497	0.374741	4.86883 4	0.06663 9	0.772442	0.317525
-3.7	13.67011	0.532979	4.87819 2	0.09647 7	0.723468	0.443095
-3.6	13.62187	0.378854	4.87005 2	0.06783 9	0.766546	0.318699
-3.5	12.68973	0.822105	4.69844 1	0.15353	1.526897	0.659864
-3.4	13.06953	0.734368	4.76887 6	0.13445 1	1.219681	0.603034
-3.3	13.55282	0.210589	4.85801 3	0.03802 5	0.82625	0.175534
-3.2	13.2283	0.659876	4.79816 1	0.11985 9	1.090439	0.546493
-3.1	13.44229	0.649518	4.83688 9	0.11780 1	0.912519	0.53883
-3	12.04771	1.11468	4.57550 6	0.21408 5	2.026788	0.865952
-2.9	12.52406	0.476899	4.66929 8	0.08887 1	1.668875	0.383644
-2.8	12.85548	0.365584	4.73104 9	0.06746 2	1.402216	0.297465
-2.7	12.42745	0.511793	4.65112 2	0.09534 5	1.745709	0.411922
-2.6	12.4136	0.595117	4.64814 4	0.11266 8	1.75486	0.469928
-2.5	12.53794	0.630028	4.67126 9	0.11714 2	1.654612	0.508228
-2.4	12.38602	0.782742	4.64203 3	0.14669 3	1.772168	0.625655
-2.3	12.31697	0.639894	4.62978 3	0.12162 4	1.83081	0.50283

-2.2	12.25483	0.549211	4.61848 8	0.10483	1.882237	0.429403
-2.1	12.27556	0.748558	4.62145 8	0.14049 7	1.861067	0.597226
-2	12.41362	0.76687	4.64726 2	0.14496 6	1.750384	0.606629
-1.9	12.82785	0.676182	4.72483	0.12387 8	1.419065	0.554826
-1.8	11.99247	0.905289	4.56670 7	0.17294 4	2.078747	0.707477
-1.7	11.72324	0.672598	4.51654 1	0.12881 5	2.295348	0.523688
-1.6	10.77035	0.572234	4.32932 1	0.11514 5	3.013357	0.417713
-1.5	10.56333	0.780149	4.28593 9	0.16319 1	3.155723	0.538371
-1.4	10.74279	0.822875	4.32208 5	0.16739	3.024962	0.591626
-1.3	9.85219	0.64503	4.13995 5	0.13478 6	3.660085	0.445855
-1.2	9.030564	1.119215	3.95797 1	0.24791 2	4.175831	0.70383
-1.1	8.374688	1.410191	3.80571 5	0.31898 4	4.55241	0.85321
-1	9.734805	0.69872	4.11468 3	0.14965 1	3.737432	0.464486
-0.9	10.03162	1.694569	4.16431 9	0.35975 2	3.470128	1.145421
-0.8	9.368917	0.789989	4.03561 7	0.17233 4	3.977038	0.509621
-0.7	8.851059	0.996273	3.91992 8	0.22006	4.297138	0.629885
-0.6	7.44958	1.069331	3.59348 8	0.24618 4	5.096293	0.627354
-0.5	6.496764	0.930689	3.35525 4	0.23811 6	5.557655	0.427605
-0.4	7.822344	1.005128	3.68324 1	0.23794 4	4.898448	0.555893
-0.3	7.912122	1.259093	3.70029 1	0.29559 8	4.827839	0.709145
-0.2	8.091627	1.120959	3.74472 1	0.26270 5	4.73865	0.63449
-0.1	7.27	0.938679	3.55075 2	0.23047 1	5.194131	0.477232
0	5.751061	1.369307	3.14110 8	0.38755	5.779456	0.457333
0.1	8.21589	0.900419	3.77672 7	0.21079 2	4.683191	0.508835
0.2	8.333251	1.765018	3.78887 2	0.39757 5	4.53988	1.08121

0.3	9.320603	1.09803	4.0218	0.23909 7	3.991697	0.710725
0.4	8.2504	1.817509	3.76740 9	0.41970 1	4.576235	1.061889
0.5	7.021449	0.709033	3.4925	0.17416 9	5.334056	0.360564
0.6	8.271107	0.47144	3.79368 6	0.10898 5	4.67231	0.273315
0.7	9.058198	0.910987	3.96680 8	0.19832 5	4.172143	0.590237
0.8	9.755536	0.573107	4.11993 6	0.12316 5	3.727744	0.378787
0.9	8.457539	0.819378	3.83338 7	0.18429 5	4.547275	0.500582
1	10.03857	2.016161	4.16020 2	0.41984 3	3.43732	1.405529
1.1	9.141048	0.772826	3.98642 3	0.16580 8	4.126494	0.512726
1.2	9.527716	1.134694	4.06624 9	0.24156 2	3.854525	0.763573
1.3	10.16286	1.002103	4.20195 8	0.20543 5	3.430841	0.712996
1.4	11.34342	0.627614	4.44289	0.12253 7	2.586437	0.476895
1.5	11.10185	0.561866	4.39564 5	0.10895	2.769562	0.430786
1.6	10.92925	0.613713	4.36094 3	0.12325 2	2.895649	0.449224
1.7	11.36418	0.838561	4.44561 8	0.16441 1	2.56401	0.634474
1.8	11.79226	0.616579	4.53010 3	0.11862	2.243348	0.47739
1.9	11.34347	0.795468	4.44183 2	0.15684 1	2.581029	0.597104
2	11.49534	0.749426	4.47186 2	0.14615 3	2.467557	0.570347
2.1	12.10293	1.13258	4.58604 6	0.21312 9	1.983629	0.901364
2.2	11.45388	1.234455	4.45977 5	0.23973 7	2.478984	0.944928
2.3	12.1651	0.603185	4.60130 1	0.11493 6	1.952074	0.472535
2.4	12.71742	0.60637	4.70471 7	0.11252 6	1.510244	0.490196
2.5	13.0004	0.644243	4.75658 7	0.12136 5	1.278259	0.511723
2.6	12.35836	0.313453	4.63876 3	0.05933 8	1.803891	0.247505
2.7	13.28352	0.46565	4.80891 9	0.08427 3	1.048375	0.387184

2.8	12.5655	0.415177	4.67721 9	0.07756 5	1.636538	0.332992
2.9	13.2282	0.063578	4.79961 1	0.01153 3	1.097904	0.052727
3	13.11086	0.41456	4.77768 8	0.07632 1	1.191999	0.338181
3.1	13.53892	0.483151	4.85490 8	0.08630 9	0.834851	0.407411
3.2	13.00738	0.623885	4.75800 9	0.11548 3	1.273259	0.505844
3.3	13.03491	0.471473	4.76365 7	0.08632 6	1.253708	0.387006
3.4	13.02116	0.56304	4.76081	0.10320 1	1.263344	0.46164
3.5	13.02119	0.677926	4.7603	0.12486 7	1.260739	0.552731
3.6	13.23515	0.679882	4.79930 2	0.12394 3	1.084242	0.560886
3.7	13.68394	0.354871	4.88119 7	0.06332 9	0.714495	0.299566
3.8	13.44229	0.788072	4.83619 6	0.14369 2	0.909035	0.650032
3.9	14.47103	0.199207	5.01991 6	0.03463 3	0.041339	0.172765
4	13.60799	0.579204	4.86692 9	0.10444 2	0.77501	0.483505
4.1	13.57343	0.725195	4.86006 9	0.13234	0.800702	0.597589
4.2	14.51249	0.080897	5.02720 1	0.01401 9	0.005768	0.070385
4.3	13.78747	0.380097	4.89957	0.06792 7	0.626584	0.320365
4.4	14.11204	0.309091	4.95708 1	0.05444 8	0.350538	0.264486
4.5	14.26392	0.117013	4.98393 9	0.02045 8	0.221114	0.100901
4.6	14.42967	0.069369	5.01284	0.01205 8	0.077792	0.060171
4.7	14.18107	0.279667	4.96924 6	0.04903 2	0.29151	0.240481
4.8	14.43657	0.109462	5.01401 8	0.01901	0.071693	0.095037
4.9	14.38825	0.063578	5.00564 4	0.01106	0.113725	0.055102
5	14.34679	0.111047	4.99840 1	0.01931 6	0.149513	0.096254
5.1	14.45727	0.070743	5.01763 3	0.01229 8	0.053813	0.061358
5.2	14.25014	0.116995	4.98153 1	0.02051 9	0.233001	0.100564



5.3	14.38133	0.069772	5.00443 6	0.01215 8	0.119716	0.060372
5.4	14.24313	0.054278	4.98034	0.00948 4	0.239205	0.046836
5.5	14.31923	0.033984	4.99363 2	0.00592 4	0.173522	0.029392
5.6	14.41586	0.074713	5.01044	0.01298 5	0.08976	0.064815
5.7	14.39516	0.034684	5.00685 3	0.00603 2	0.107784	0.030071
5.8	14.39516	0.034684	5.00685 3	0.00603 2	0.107784	0.030071
5.9	14.38135	0.044418	5.00444 9	0.00773	0.119738	0.03848
6	14.2777	0.06807	4.98637 3	0.01187 2	0.209359	0.058845
6.1	14.44347	0.041621	5.01524 7	0.00722 7	0.065853	0.036143
6.2	14.40206	0.046014	5.00805	0.00799 6	0.101786	0.039924
6.3	14.40206	0.033984	5.00805 3	0.00591	0.1018	0.029463
6.4	14.33304	0.033984	4.99603 8	0.00592 4	0.161583	0.029392
6.5	14.36755	0.057622	5.00204 3	0.01003 2	0.131677	0.0499
6.6	14.32611	0.055974	4.99482 5	0.00975 8	0.167545	0.04841
6.7	14.38135	0.062432	5.00444 4	0.01086	0.119709	0.054113
6.8	14.24316	0.062538	4.98034 1	0.01093 1	0.239169	0.05394
6.9	14.42276	0.037356	5.01165 1	0.00649 1	0.083834	0.032417
7	14.33994	0.044418	4.99723 9	0.00773 7	0.155599	0.038446

140 RPM - 18cm						
Avg y position	Avg model pressure	STD Pressure	Avg $U_{\infty}$	STD $U_{\infty}$	Avg $U_{\infty}(U_{\infty\max}-U_{\infty})$	STD $U_{\infty}(U_{\infty\max}-U_{\infty})$
-7	15.85175	0.046014	5.254061	0.007633	0.167784	0.039782
-6.9	15.81034	0.043873	5.247194	0.00728	0.203603	0.037919
-6.8	15.78273	0.070743	5.242603	0.011753	0.227411	0.061069
-6.7	15.90007	0.044418	5.262063	0.007352	0.12594	0.03849
-6.6	15.85865	0.031789	5.255208	0.005269	0.161825	0.027505
-6.5	15.98994	0.055602	5.276911	0.009177	0.047912	0.048317
-6.4	15.9415	0.037407	5.268917	0.006182	0.090008	0.032465
-6.3	15.92082	0.077331	5.265486	0.012775	0.107889	0.06714
-6.2	15.81724	0.057622	5.248336	0.009562	0.197617	0.049805
-6.1	15.87939	0.069419	5.258632	0.011487	0.143822	0.06017
-6	15.95536	0.048655	5.271203	0.008038	0.077968	0.042242
-5.9	15.86556	0.051911	5.256347	0.008607	0.155826	0.044905
-5.8	15.83795	0.046014	5.251773	0.007633	0.179728	0.039786
-5.7	15.92773	0.062504	5.266632	0.010336	0.10193	0.054214
-5.6	15.78963	0.069715	5.243749	0.011576	0.221453	0.060216
-5.5	15.78963	0.031789	5.243759	0.005281	0.221506	0.027444
-5.4	15.84485	0.055927	5.252915	0.009271	0.173743	0.048391
-5.3	15.83105	0.112069	5.250602	0.018592	0.185555	0.096888
-5.2	15.89316	0.041621	5.260921	0.006889	0.131925	0.036066
-5.1	15.79654	0.067967	5.244896	0.011271	0.215494	0.058784
-5	15.86556	0.051911	5.256347	0.008597	0.155827	0.044958
-4.9	15.88626	0.057622	5.259774	0.009541	0.137884	0.049915
-4.8	15.92082	0.08891	5.265481	0.014699	0.107863	0.077137

-4.7	15.80344	0.048558	5.24604 8	0.00805 9	0.209561	0.041964
-4.6	15.83795	0.063578	5.25176 8	0.01054 2	0.179701	0.054993
-4.5	15.94158	0.090284	5.26891 2	0.01492 2	0.089851	0.078348
-4.4	15.87248	0.072474	5.25748 8	0.01199 3	0.149794	0.062815
-4.3	16.03828	0.088116	5.28487	0.01452 4	0.005799	0.076679
-4.2	15.89316	0.041621	5.26092 1	0.00688 9	0.131925	0.036066
-4.1	15.83105	0.054179	5.25062 7	0.00898 9	0.185687	0.046834
-4	15.83112	0.228137	5.25051 1	0.03799 1	0.184943	0.196474
-3.9	15.98994	0.070851	5.27690 6	0.01169 4	0.047886	0.061567
-3.8	16.03138	0.080975	5.28373 6	0.01332 6	0.011823	0.070575
-3.7	15.72061	0.069715	5.23227 6	0.01158 6	0.281001	0.060162
-3.6	15.693	0.388865	5.22728 5	0.06556 4	0.302698	0.330633
-3.5	15.85865	0.069715	5.25519 8	0.01155 1	0.161772	0.060349
-3.4	15.84485	0.071082	5.25291	0.01178 3	0.173716	0.061503
-3.3	15.86563	0.261084	5.25618 7	0.04365 9	0.15485	0.223891
-3.2	15.40306	0.432691	5.17866 1	0.07328 8	0.550589	0.366128
-3.1	15.62398	0.138911	5.21613 2	0.02316	0.363942	0.119484
-3	15.20976	0.710338	5.14514 7	0.12174 2	0.710072	0.59356
-2.9	14.95428	0.677924	5.10187 1	0.11553 3	0.926222	0.569985
-2.8	14.30535	0.700639	4.98975 5	0.12132 5	1.463651	0.578914
-2.7	14.72643	0.267031	5.06393	0.04643 8	1.122447	0.219557
-2.6	13.58733	0.998705	4.86105 7	0.17962 5	2.03376	0.790069
-2.5	13.64943	1.23232	4.87031 4	0.22473	1.974555	0.958837
-2.4	13.62177	1.25748	4.86521 3	0.22805 8	1.995759	0.98508
-2.3	14.18112	0.891932	4.96704 4	0.15679 3	1.55996	0.724706

-2.2	13.35254	1.286651	4.816304	0.238148	2.206083	0.98326
-2.1	12.49645	0.872231	4.66215	0.163448	2.882065	0.655156
-2	12.04771	1.006152	4.576254	0.197284	3.209477	0.710038
-1.9	12.28243	1.150871	4.619891	0.215549	3.031384	0.865789
-1.8	11.48154	1.156979	4.465508	0.23333	3.610044	0.78442
-1.7	12.26178	0.931041	4.617538	0.179105	3.05492	0.675399
-1.6	10.47356	0.879416	4.266976	0.180389	4.315965	0.578469
-1.5	10.58401	0.811026	4.289988	0.167139	4.24525	0.529717
-1.4	8.93391	0.77718	3.94073	0.170278	5.272666	0.453854
-1.3	9.002981	1.019426	3.953587	0.21903	5.220341	0.618168
-1.2	7.974266	0.966112	3.71987	0.223485	5.776378	0.503489
-1.1	7.235465	0.862064	3.543361	0.212904	6.129946	0.378239
-1	7.152689	0.71115	3.525011	0.175331	6.177095	0.313431
-0.9	7.725715	0.554659	3.665607	0.132434	5.922385	0.266173
-0.8	6.365598	0.806687	3.323126	0.206654	6.48062	0.314959
-0.7	6.407036	1.051815	3.328806	0.278273	6.43848	0.368933
-0.6	5.578532	0.754936	3.11002	0.20738	6.724785	0.219677
-0.5	5.219498	0.569008	3.010548	0.162536	6.824223	0.136178
-0.4	4.591255	0.833366	2.815923	0.258339	6.889493	0.108509
-0.3	4.901925	0.957934	2.908933	0.274552	6.840122	0.226775
-0.2	4.390994	1.069696	2.744635	0.338929	6.861413	0.13865
-0.1	3.327818	0.80787	2.389344	0.295257	6.834818	0.169695
0	3.831798	1.066936	2.557633	0.364379	6.846734	0.149407
0.1	4.411676	0.507476	2.76726	0.15903	6.944989	0.057194
0.2	5.530218	0.814254	3.094738	0.231937	6.728145	0.198982
0.3	5.323054	0.732024	3.03728	0.21269	6.78522	0.162887

			6	7		
0.4	6.766071	0.906854	3.42428 1	0.24026 6	6.31792	0.312915
0.5	6.089389	0.983656	3.24618 8	0.25956 1	6.554936	0.347894
0.6	6.835092	0.724446	3.44526 9	0.18305	6.308664	0.294885
0.7	6.56581	0.486144	3.37909 9	0.12632 1	6.427832	0.179094
0.8	7.594574	0.701432	3.63294 5	0.16627 5	5.97811	0.343533
0.9	7.794736	1.044764	3.67610 6	0.24716 2	5.857686	0.515589
1	7.66362	1.043165	3.64434 1	0.25560 5	5.918108	0.470638
1.1	8.975347	0.538379	3.95171 1	0.11977	5.258548	0.304854
1.2	8.782038	0.941129	3.90520 5	0.20830 6	5.349356	0.538843
1.3	10.72903	0.699552	4.32029 5	0.13944 8	4.152907	0.48123
1.4	9.865995	0.634793	4.14291 2	0.13308 9	4.718206	0.402235
1.5	10.7152	1.501047	4.30938	0.30044 4	4.119291	1.026521
1.6	10.71518	0.716947	4.31733	0.14471 5	4.161362	0.484086
1.7	11.90957	1.20235	4.5483	0.23144 5	3.302281	0.87109
1.8	11.33657	1.242746	4.43689	0.23828 2	3.711227	0.905387
1.9	12.6552	0.431152	4.69384 5	0.08016 2	2.773152	0.327117
2	14.14651	0.820678	4.96130 8	0.14570 5	1.589911	0.659066
2.1	14.11895	0.512958	4.95778 4	0.08977 3	1.619276	0.4188
2.2	13.43539	1.169855	4.83251	0.21095 4	2.147468	0.923161
2.3	12.97972	0.627551	4.75295 9	0.11491 2	2.520481	0.485593
2.4	13.55282	1.257479	4.85291 4	0.22684 4	2.050815	0.991406
2.5	14.29843	1.108678	4.98615 6	0.19696 6	1.456693	0.889875
2.6	14.92669	1.093567	5.09505 4	0.18718 7	0.938224	0.915096
2.7	13.91176	0.636113	4.92079 1	0.11287 5	1.784537	0.511227

2.8	15.58252	0.331401	5.20896 2	0.05576 6	0.398244	0.282348
2.9	15.83117	0.246435	5.25049 6	0.04100 2	0.184781	0.21242
3	15.60325	0.44103	5.21219 7	0.07430 7	0.379243	0.375259
3.1	15.74822	0.220349	5.23675 3	0.03681 4	0.256587	0.18913
3.2	15.78273	0.083243	5.24259 8	0.01383	0.227385	0.071859
3.3	15.78281	0.312184	5.24237 5	0.05175	0.226079	0.27011
3.4	16.01065	0.065538	5.28032 4	0.01079 7	0.029891	0.057057
3.5	15.77583	0.278003	5.24126 4	0.04665 2	0.232353	0.237533
3.6	16.03831	0.062504	5.28488 4	0.01029 6	0.005829	0.054423
3.7	15.73442	0.109462	5.23455 4	0.01822 7	0.269003	0.094275
3.8	16.04519	0.088918	5.28600 6	0.01463 4	-0.00021	0.077492
3.9	15.85175	0.033984	5.25406 4	0.00563 3	0.167797	0.029404
4	15.79651	0.251722	5.24473 6	0.04222 9	0.214689	0.21514
4.1	15.78963	0.044418	5.24375 7	0.00737 4	0.221492	0.038374
4.2	15.90699	0.055545	5.26320 6	0.00918 7	0.11992	0.048169
4.3	15.88626	0.048558	5.25977 7	0.00803 9	0.137897	0.042066
4.4	15.94155	0.078883	5.26891 2	0.01303 3	0.089899	0.068479
4.5	15.86556	0.074713	5.25634	0.01238 5	0.155787	0.064645
4.6	15.77583	0.034684	5.24146 6	0.00576 2	0.233423	0.029944
4.7	15.73442	0.057622	5.23457 7	0.00959 3	0.269123	0.049641
4.8	15.76202	0.098347	5.23915	0.01634 8	0.245221	0.084852
4.9	15.78963	0.062432	5.24375 2	0.01036 1	0.221466	0.053957
5	15.91395	0.077658	5.26434 8	0.01284 1	0.113853	0.067358
5.1	15.90012	0.098407	5.26205 1	0.01629 7	0.125792	0.085225
5.2	15.83795	0.055495	5.25177 1	0.00919 8	0.179715	0.04802

5.3	15.693	0.076306	5.22767 7	0.01270 5	0.304769	0.065724
5.4	15.92773	0.062504	5.26663 2	0.01033 6	0.10193	0.054214
5.5	15.89321	0.080975	5.26091 7	0.01339 6	0.131816	0.070204
5.6	15.86556	0.060474	5.25634 5	0.01002 3	0.155813	0.052334
5.7	15.81724	0.037356	5.24834 1	0.00619 7	0.197644	0.032295
5.8	15.87246	0.065443	5.25748 6	0.01084 4	0.149828	0.056643
5.9	15.81724	0.037356	5.24834 1	0.00619 7	0.197644	0.032295
6	15.85178	0.099121	5.25404 6	0.01642 9	0.167657	0.085769
6.1	15.81724	0.037356	5.24834 1	0.00619 7	0.197644	0.032295
6.2	15.86556	0.067967	5.25634 2	0.01126 2	0.1558	0.058833
6.3	15.88629	0.065493	5.25977 6	0.01083 6	0.137849	0.056773
6.4	15.90014	0.10321	5.26205 3	0.01708 8	0.125757	0.08941
6.5	15.87939	0.076036	5.25863	0.01259	0.143808	0.065862
6.6	15.92773	0.054262	5.26663 5	0.00896 7	0.101943	0.047097
6.7	15.96919	0.044527	5.27348 8	0.00735 4	0.065963	0.038669
6.8	15.78963	0.044418	5.24375 7	0.00737 4	0.221492	0.038374
6.9	15.78273	0.055495	5.24260 8	0.00922	0.227438	0.047907
7	15.83795	0.055495	5.25177 1	0.00920 8	0.179715	0.04797