

MAE 4273: EXPERIMENTAL FLUID DYNAMICS

Lab Report

Fall 2019

Wind Tunnel Performance Characterization

School of Mechanical and Aerospace Engineering

Oklahoma State University

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ABSTRACT

The Oklahoma State University Endeavor Wind Tunnel allows for evaluation of test articles in low velocity (<36m/s) airflows. Quality of a wind tunnel's flow in terms of constant velocity throughout the cross section can vary, and presence of boundary layer effects may be prevalent. This laboratory will not only calibrate the wind tunnel's pressure transducer to properly obtain velocity measurements, but also create a velocity profile to determine if any velocity gradients or unsteadiness occurs. A pitot probe and traverse were used to take pressure measurements at four different flow speeds ranging from 3-18m/s and spanning a quadrant of the wind tunnel test section, approximately 0.093m². These results not only calibrated the tunnel's pressure transducer for calculating velocity measurements, but also determined that while some velocity variances do occur throughout the test section, they are less than 10% of the slowest observed flow speed of 3.1m/s and less than 1% at the highest observed flow speed of 18m/s. With these findings, the Endeavor Wind Tunnel flow may be assumed to be uniform at elevated flow velocities of 18m/s. At lower velocities (<5m/s), the velocity gradient introduces more flow variance and resulting tests done in this flow realm should consider such gradients.

1. INTRODUCTION

Wind tunnels accelerate air either through an open or closed-loop system to simulate elevated flow velocities, often external flows over an object such as an aircraft wing or even internal flows through a jet engine. Flow speeds can reach hundreds of kilometers per hour, depending on the system, but the quality of this flow is vital to performing experiments and understanding quantities like drag coefficient and drag force. Evaluating the quality of the flow to find velocity gradients and pressure fluctuations is a necessary part of running wind tunnel tests.

NASA has worked on transonic wind tunnels and discovered that stream turbulences in the flow can be expected from the tunnel drive system and test section contraction [1]. Acoustical disturbances also come from the drive system as well as tunnel walls and diffuser. Given each of these effects on flow, properly characterizing the specific wind tunnel of interest is a necessary procedure.

Timely testing of a wind tunnel is also vital because operational parts wear down with time. Lindgren and Johansson state “it is commonly known that the maximum speed of a wind-tunnel is usually decreasing with time,” but they were able to determine their wind tunnel of interest was still operating nominally after ten years of operation [2].

The objectives for this lab are as stated:

1. Calibrate the OSU Endeavor Wind Tunnel’s pressure transducer using a manometer to obtain corrected pressure measurements and calculate velocity given the tunnel fan’s rotational speed between 0 and 720 RPM.
2. Determine the presence and magnitude (in percentage of flow velocity) of velocity gradients in the test section’s flow to assess flow uniformity and quality throughout the test section for free stream speeds less than 19m/s.

2. EXPERIMENTAL ARRANGEMENTS

Materials:

This laboratory primarily used test equipment and did not measure samples, other than the air in the closed-circuit wind tunnel. The inclined manometer used a red gage fluid, with a specific gravity of 0.827. The wind tunnel and manometer equipment are discussed in the following subsection.

Facilities and Equipment:

The equipment used for this laboratory exercise was the Aerolab closed-circuit wind tunnel (Aerolab, LLC, Jessup, MD, USA) and LabView 2018 (National Instruments, Austin, TX, USA) software suite located in Endeavor 140 at Oklahoma State University. The tunnel is capable of fan speeds of 880 RPM to generate airflow velocities up to 133 km/h in a closed-loop system [3]. Due to the closed-loop nature of the tunnel, it utilizes a M1-3A refrigerant system (Advantage Engineering, Greenwood, IN, USA) to maintain the air at a constant temperature throughout wind tunnel operation. The test section features clear panes for viewing test articles and measures 1.22m in length (x -direction), 0.61 m in depth (y -direction), and 0.61m in height (z -direction). Due to a manufacturer-installed load cell section that raised concerns about flow behavior, a portion of the tunnel was removed and replaced with an acrylic cover to maximize the test section volume and mitigate unwanted air flow patterns. The cover induces a slight cross-section change in the test section by ramping up at 6° from the test section entrance and ramping back down at the test section exit. This assembly with the pitot-static probe in its calibration starting position is shown in Figure 1. This starting position is discussed further in the following subsection.

The wind tunnel is controlled and operated by a virtual instrument (VI) coded in LabView that Aerolab provided with the tunnel. Their included traverse system is integrated into the VI and allows for motion control of an instrument (in this case, a pitot-static probe) inside the test section, and data acquisition during tunnel operation. This VI interface can be seen in Figure 2. The interface allows monitoring of the traverse and live data, as well as buttons for operating the tunnel and data acquisition on

the far right. Data may be collected continuously or manually in bursts to record traverse position, fan RPM, static pressure, and many flow properties. These data are written to a .CSV file which can be opened in Excel and manipulated like any other spreadsheet for data analysis.

In addition to the data collection being handled by the VI, an inclined tube differential manometer was also installed with the pitot-static probe to provide a manual measurement reading for calibration and validation purposes (discussed later). It measured change in pressure by hundredths of an inch.

The pitot-static probe was 5mm in diameter with a tapered head and static slots 2.54cm from the head tip and an overall length of 31.75cm. The Aerolab VI had built-in displacement limits to prevent the probe from extending too close to any of the test section walls. The probe was connected to the manometer and a digital pressure transducer.

Experimental protocols:

This laboratory exercise was divided into two procedures: calibration of pressure transducer and free stream velocity, and tunnel flow quality assessment. They are each addressed separately below.

I. Calibration of Pressure Transducer and Free Stream Velocity

The pitot-static probe's initial position in the tunnel was recorded using cartesian coordinates in relation to the test section entrance ramp up (x -direction), far back wall of the wind tunnel test section (y -direction) and test section base (z -direction). Its initial location is as follows: (747.8mm, 285.75mm, 320.675mm) in the (x , y , z) directions, respectively. With the tunnel fan turned off and zero airspeed, the ambient conditions were recorded using the Aerolab VI. A burst of 50 samples was recorded for one second to represent the tunnel airspeed at zero. The manometer fluid position was also recorded by manually reading the gage and typing its position into a spreadsheet.

Beginning with 75 RPM fan speed control input via VI, the fan speed indicator was allowed to reach steady state, 50 data samples recorded, manometer reading recorded, and CSV file name changed to reflect the current fan speed. This process is repeated in intervals of 75 RPM, all the way up to 675 RPM. After recording data at 675 RPM, the same intervals are repeated by decreasing the fan speed 75 RPM

each time until 0 RPM is reached and the tunnel shut back off, at which point the final data recordings take place.

To study repeatability and hysteresis, this entire ramp up-ramp down process was completed a second time for additional data points and validating the digital data and manometer readings, as studying the ticks on the manometer took some operator practice.

II. Tunnel Flow Quality Assessment

Flow quality of the wind tunnel was evaluated by 3 different pitot-static probe positions along the y axis, probing the x - z plane. A .CSV file script was pre-programmed and loaded into the Aerolab VI to dictate the probe position and record samples throughout, effectively automating the entire profile for a given RPM. The laboratory operators defined 4 fan RPMs (120, 360, 540, and 720) at which to run each of the three x - z planes, for a total of 12 profiles. These combinations are listed in Table 1.

The intent of this assessment was to gather information about boundary layer effects and flow uniformity throughout the square cross section of the test section. Only one quadrant of the tunnel was examined, and the assumption made that the remaining quadrants were symmetrical about their respective axes.

Calculated quantities:

The data of interest obtained from calibration and tunnel flow quality evaluation include model and dynamic pressure, and fan speed (RPM). Other parameters obtained from ambient conditions include

$$P_{air} = 0.984 \text{ bar}, T_{air} = 295.93 \text{ K}, \text{ and } R_g = 287.1 \frac{\text{J}}{\text{kg}\cdot\text{K}}.$$

The ideal gas equation is used to find density from air pressure P , the gas constant for air R_g , and air temperature, T .

$$\rho = \frac{P}{R_g T}$$

To obtain flow velocity from total and static pressure as measured by the pressure transducer and pitot-static probe, Bernoulli's equation is utilized where P is pressure, ρ is density, V is flow velocity, g is gravitational acceleration, and h is elevation. The equality between subscripts 1 and 2 indicate a conservation of energy between two states.

$$P_1 + \frac{1}{2}\rho V_1^2 + \rho g h_1 = P_2 + \frac{1}{2}\rho V_2^2 + \rho g h_2$$

Reducing the equation by eliminating the potential energy terms and assuming a $V_1 = 0 \text{ m/s}$ for total pressure yields:

$$V_2 = \sqrt{\frac{2(P_1 - P_2)}{\rho}}$$

Defining $P_1 = P_t$ for total pressure and $P_2 = P_s$ for static pressure, results in the following equation that allows for the calculation of flow velocity.

$$V_2 = \sqrt{\frac{2(P_t - P_s)}{\rho}}$$

For V as freestream velocity, x as test section length to pitot probe, and μ as dynamic viscosity, Reynolds Number is calculated by:

$$Re = \frac{\rho V x}{\mu}$$

Errors are found by dividing the difference of true and calculated values by the true value.

$$Error = \frac{\text{true value} - \text{measured value}}{\text{true value}}$$

3. RESULTS AND DISCUSSION

3.1. Summary:

This experiment first calibrated the Aerolab wind tunnel pressure measurements for freestream velocity using a manometer to validate the tunnel's pressure transducer. It was found that freestream velocity of the tunnel varies linearly with fan RPM, and as a result, the freestream velocity can be

calculated for a new fan RPM. Following calibration, the cross-sectional profile of the wind tunnel test section was mapped to locate velocity gradients resulting from boundary layer effects. It was found that there is wide variance in velocity nearest the bottom of the test section, then a general increase, and followed by a decrease in velocity nearing the middle of the tunnel. These decreases however are limited to 0.3 m/s or less, so the cross section can be reasonable assumed as constant velocity throughout.

3.2. Calibration of Pressure Transducer and Free Stream Velocity

For calibrating the wind tunnel's pressure transducer, a manometer was used to compare pressure data. These data are shown in Figure 3 and feature 3 different data series: ramp up to 675 RPM fan speed, ramp back down to zero RPM, and a second ramp up to 675 RPM. Hysteresis was also studied for this: the effect of approaching value from above or below. With these points plotted, a best-fit trendline was generated and the point-slope equation form displayed on the graph with the R^2 value.

These trendlines correspond very well to the data, with R^2 values over 0.997 or better. Each trendline is overlapping the others, with error bars covering similar ranges of manometer pressure, meaning the data is consistent from ramp up 1, ramp down 1, and ramp up 2.

For the equations defined by the above trendlines, the model pressure may be corrected and used for calculation of the tunnel's horizontal velocity. The velocity is calculated from the reduced form of Bernoulli's equation as defined in the previous section. These velocities are plotted in Figure 4 as a result of fan RPM.

The best-fit trendlines equations are displayed on the above figure, and the slope of the slope-intercept equation form was used to calculate the freestream speed. The figure for slope, 0.0259, was used for remaining freestream speed calculations by multiplying it by the fan speed RPM to obtain the flow velocity at a given fan speed.

Errors have been quantified in Tables 2 and 3 based upon pressure and velocity. Most errors are less than 5%, but some outliers exist, at 300 RPM ramp up and 75 RPM ramp down, for example. The #DIV/0! cells are a result of a true value of 0 inches observed on the manometer (indiscernible pressure

rise).

An identical table for velocity measurements, Table 3, contains error values that are even less for the velocity calculations.

Additionally, hysteresis and repeatability were also studied for the ramp up – ramp down and ramp up 1 and 2, respectively. These results are tabulated in Table 4.

The #NUM! cells are a result of negative pressure transducer measurements near zero fan speed, and the negatives are not calculated when under the square root of the velocity calculation. For hysteresis and repeatability, the minimum and maximum values are indicated in green and red, respectively.

These hysteresis data indicate that the lengthy time spent between reaching 75 RPM on the ramp up and down allows for some instrumentation error when approached from below and above. The velocities are less repeatable when approached multiple times from zero fan speed to the max of 675 RPM in this experiment.

These calibration data allow for a valuable observation and calibration calculation. It appears that there is a linear relationship between fan speed and the resulting freestream velocity. With the following calibration equation of $U_{\infty} = 0.0259(\text{RPM})$, the tunnel's velocity may be calculated for any given fan speed between 0 and 720 RPM which are used in the next phase of the laboratory.

3.3. Tunnel Flow Quality Assessment

For this portion of the experiment, the y and z probe locations were varied to map a 2D velocity profile of the tunnel test section. 3 y locations starting at $y=0$ in (0 m), $y=3.5$ in (0.0889 m), and $y=7$ in (0.1778 m) were selected and are plotted in Figure 5 for varying z locations. The $z=0$ location is the bottom of the wind tunnel test section and rises from there towards the center.

There is not a significant difference in velocities between the y locations, and this could be the result of the low airspeed at 3.11 m/s. There is actually a reduction in measured airspeed further from the bottom floor of the tunnel, but this slowdown is 0.3 m/s or less, still less than 10% of the flow speed.

For a maximum operating fan speed of 720 RPM (corresponding to 18.65 m/s), the observed velocity changes in the y and z directions are more distinctive, as seen in Figure 8. The higher velocity occurs at the center of the tunnel for $y=0$ m and exhibits some varying behavior in the z direction. The slowest velocities are observed nearest the tunnel floor, then increases to a max around 0.05m in height, but then slows down again nearest the center of the tunnel. This may be due to the higher number of samples collected nearest the tunnel floor.

The reason for the bulge could be due to the installed plate that exhibits the 6° ramp as explained in the previous section. However, much like the behavior in Figure 5, the difference in velocity is only about 0.2 m/s, which for a calibrated airspeed of 18.65 m/s, this is a slowdown of only 1% of the tunnel's speed. The intermediate plots at 9.3 m/s and 13.99 m/s are shown in the appendix.

These plots and analysis allude to higher flow speeds and largest degree of velocity uniformity nearest the center of the tunnel.

Following the above analysis, a non-dimensional assessment was also made of velocities and displacements as a scaled function of the tunnel airspeed and tunnel height, respectively. Figure 9 shows these data for the center of the tunnel at $y=0$ m.

The significance of this plot is it shows the horizontal velocity plotted as a fraction of the free stream speed. The proximity to $u/U_\infty=1$ indicates a horizontal air velocity as matching the free stream speed. The higher tunnel speeds approach 1 closer than the lower tunnel speeds. As the probe approaches the center of the tunnel and z/H increases, the flow experiences fewer boundary layer effects than near the bottom of the tunnel. This is supported also by Figure 11 which is the same plot, but displaying the values associated with $y=0.1778$ m, closest to the tunnel wall. The intermediate plot for $y=0.0889$ m is shown in Figure 10.

Reynolds number is also calculated for each of the 12 test points and is included in the appendix.

3.4. Limitations:

The primary assumption made in this study is that airflow is incompressible throughout all parts of the tunnel and therefore constant density during the tests. It was also assumed that air temperature outside the tunnel was identical to the air temperature inside being used during tests. The refrigerant system was also not enabled, so constant temperature throughout the lab experiment was also used.

The largest limitation was the inability to map velocities nearest the tunnel walls. The traverse had built-in displacement limits that prevented moving the probe within several centimeters of the walls. It is within those bounds that the largest velocity gradients may exist, but unfortunately, they cannot be tested with the current setup.

4. CONCLUSIONS

1. Wind tunnel freestream speed as a function of fan rotational velocity is obtained. This enables future testing without recalibrating pressure transducer.
2. Higher flow velocities occur near the middle of the tunnel and experience a slowdown near the walls.
3. Velocity gradients in the OSU Endeavor Wind Tunnel are more prevalent as a percentage of the flow speed for low flow velocities. Flow quality is most uniform near the middle of the test section.

REFERENCES

- [1] Harvey, William D., Stainback, P. Calvin., Owen, Kevin F. “Evaluation of Flow Quality in Two Large NASA Wind Tunnels and Transonic Speeds.” NASA. December 1980.
- [2] Lindgren, Bjorn & Johansson, Arne. “Evaluation of the Flow Quality in the MTL Wind Tunnel.” Department of Mechanics. Royal Institute of Technology. Stockholm, Sweden. October 2002.
- [3] Patel, Havya. “Oklahoma State University Endeavor Lab Wind Tunnel Operations Manual.” *Aerolab LLC*. June 13, 2018.

TABLES

Pitot-Static Probe Location	Fan RPM 1	Fan RPM 2	Fan RPM 3	Fan RPM 4
$y + 0\text{cm}$	120	360	540	720
$y + 8.89\text{cm}$	120	360	540	720
$y + 17.78\text{cm}$	120	360	540	720

Table 1: Listing of the 12 Samples Taken at Varying Probe Location and Fan RPM

RPM	ΔP_{mano} (Pa)	$\Delta P_{\text{cal,eqn}}$ (Pa)	Error
0	0.00	0.22	#DIV/0!
75	0.00	1.29	#DIV/0!
150	4.98	5.12	-2.8%
225	11.84	11.43	3.4%
300	15.57	19.95	-28.1%
375	32.39	30.99	4.3%
450	44.85	44.07	1.7%
525	59.80	58.28	2.6%
600	74.75	75.16	-0.5%
675	89.70	91.42	-1.9%
600	74.75	74.58	0.2%
525	59.80	56.91	4.8%
450	44.85	42.93	4.3%
375	29.90	30.59	-2.3%
300	19.93	19.41	2.6%
225	9.97	10.91	-9.5%
150	4.98	4.63	7.0%
75	1.87	0.66	64.8%
0	0.00	-0.11	#DIV/0!

Table 2: List of Pressure Errors for Ramp Up 1 and Ramp Down 1

RPM	U_{∞_APmano} (m/s)	$U_{\infty_cal,eqn}$ (m/s)	Error
0	0.00	0.00	#DIV/0!
75	0.00	1.94	#DIV/0!
150	4.15	3.89	6.4%
225	6.39	5.83	8.9%
300	7.33	7.77	-5.9%
375	10.58	9.71	8.2%
450	12.45	11.66	6.4%
525	14.37	13.60	5.4%
600	16.07	15.54	3.3%
675	17.60	17.48	0.7%
600	16.07	16.08	-0.1%
525	14.37	14.07	2.1%
450	12.45	12.06	3.1%
375	10.16	10.05	1.1%
300	8.30	8.04	3.1%
225	5.87	6.03	-2.8%
150	4.15	4.02	3.1%
75	2.54	2.01	20.9%
0	0.00	0.00	#DIV/0!

Table 3: Errors for Velocity.

RPM	$U_{\infty\text{rampup1}}$	$U_{\infty\text{rampdown1}}$	Hysteresis	$U_{\infty\text{rampup2}}$	Repeatability
0	0.867	#NUM!	#NUM!	#NUM!	0.000
75	2.112	1.508	0.603	1.393	0.083
150	4.206	4.000	0.206	4.083	0.165
225	6.284	6.139	0.145	6.170	0.248
300	8.302	8.189	0.113	8.274	0.330
375	10.346	10.279	0.067	10.351	0.413
450	12.339	16.050	0.162	12.309	0.495
525	14.188	14.021	0.167	14.184	0.578
600	16.113	12.177	0.063	16.161	0.660
675	17.771	17.749	0.022	17.809	0.743

Table 4: Hysteresis and Repeatability of Horizontal Velocity

FIGURES

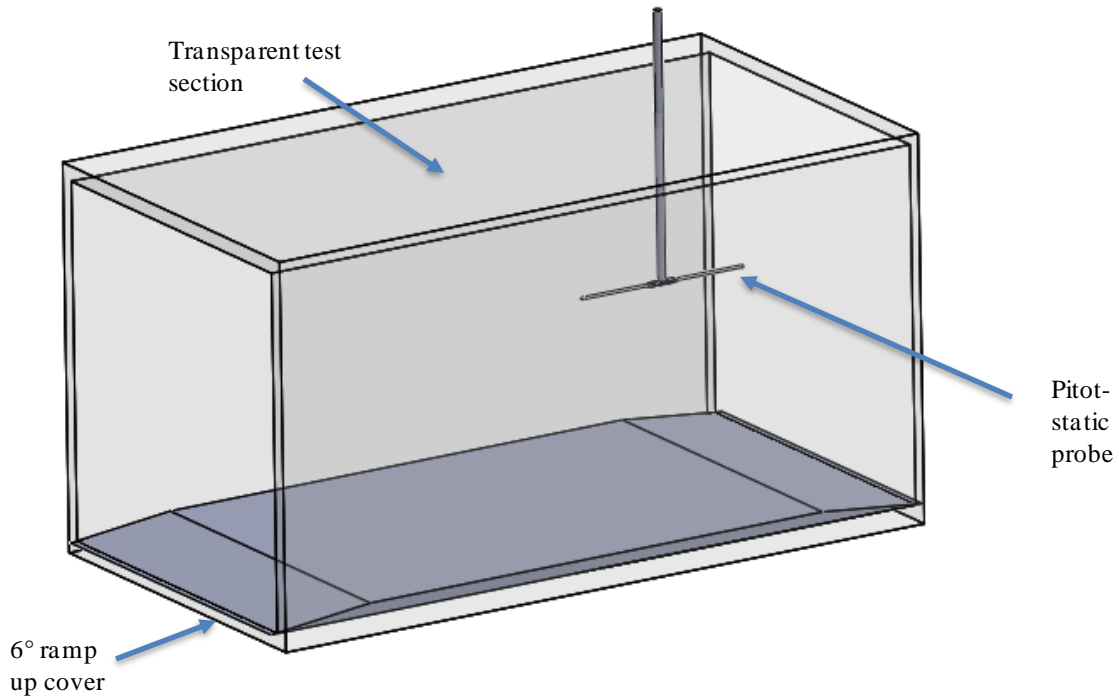


Figure 1: Schematic of Aerolab Wind Tunnel Test Section with Installed Pitot-Static Probe.

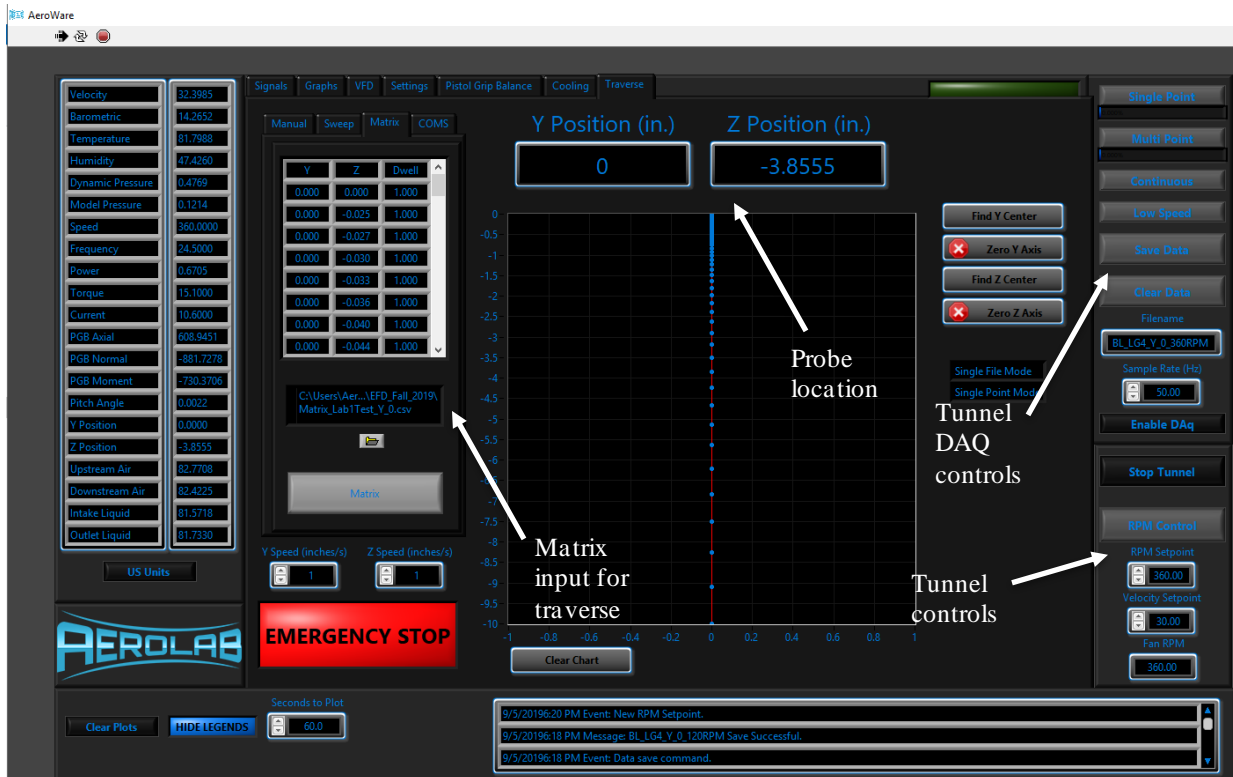


Figure 2: Screenshot of the Aerolab Wind Tunnel VI, with Buttons Labeled.

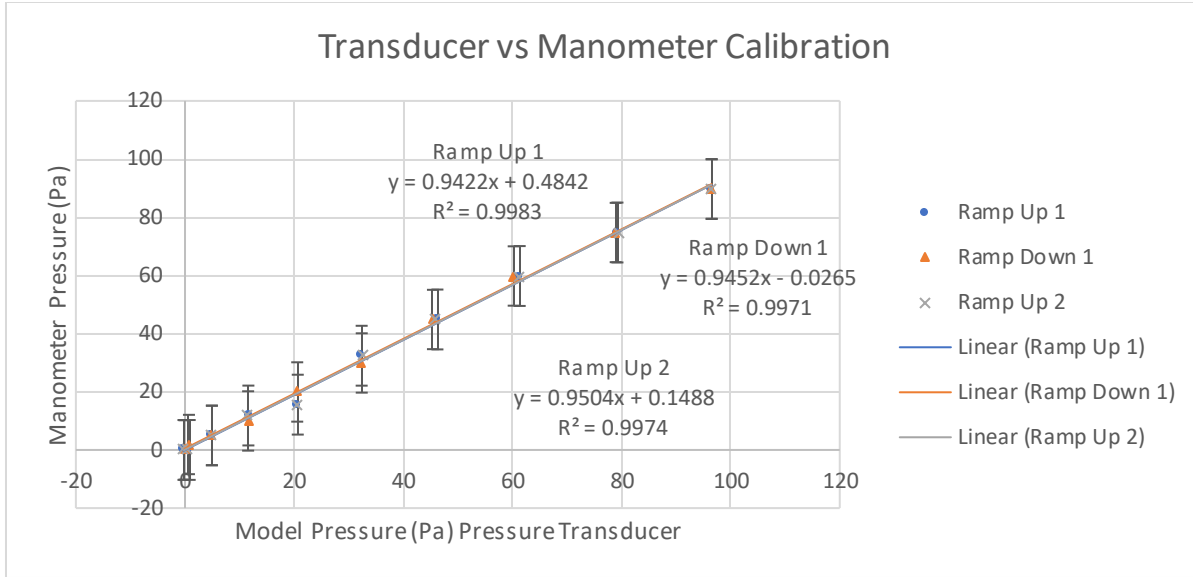


Figure 3: Graph Displaying Transducer Calibration with Best-Fit Lines and Linear Equations

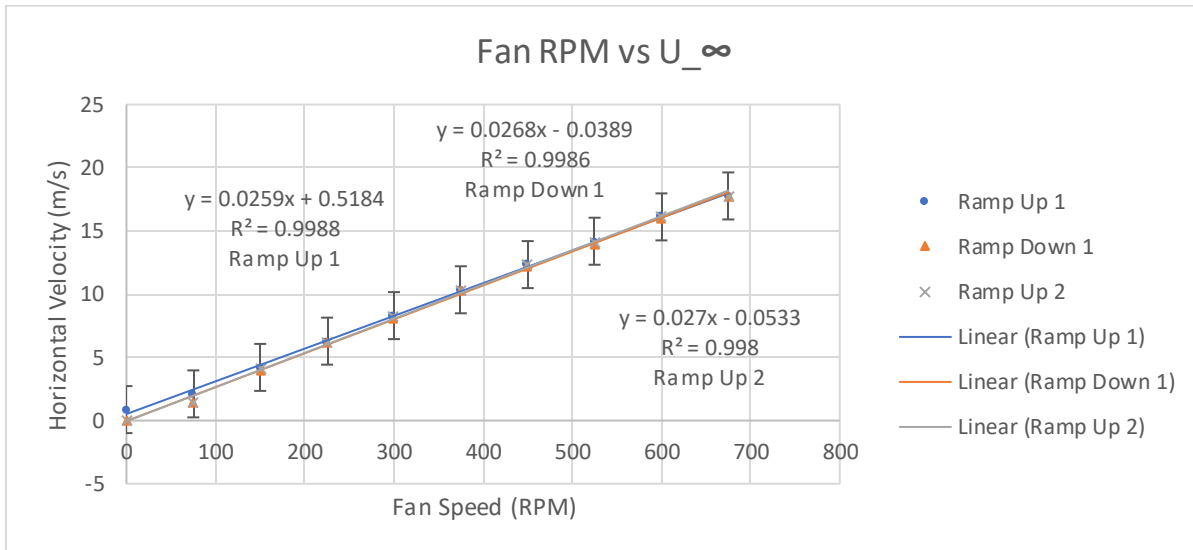


Figure 4: Fan RPM vs Horizontal Velocity with Best-Fit Lines and Linear Equations.

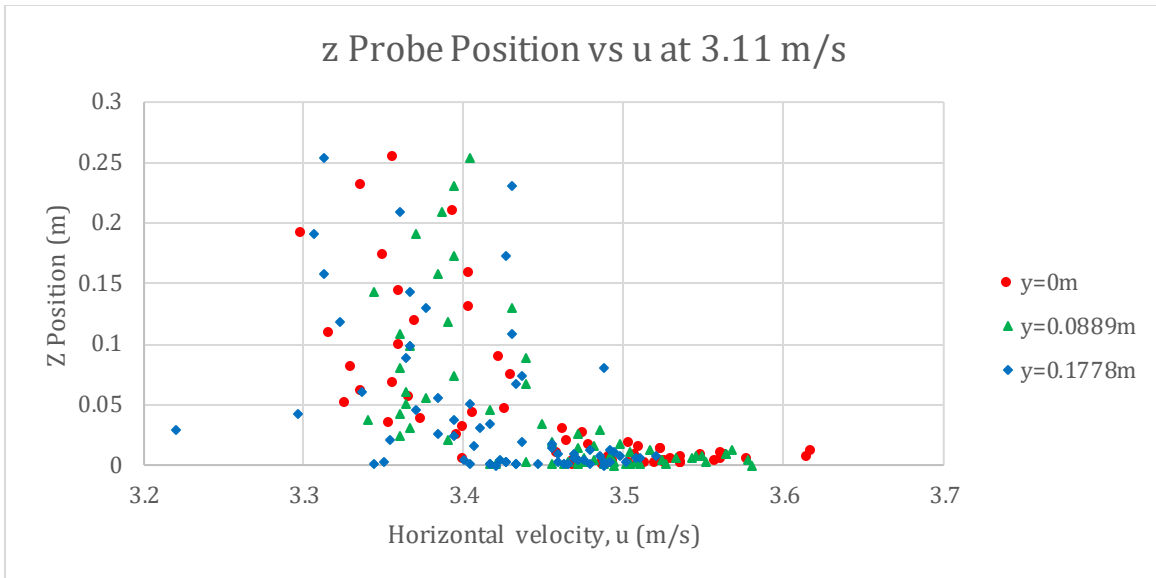


Figure 5: Probe Position and Resulting Horizontal Velocity at 120 RPM Fan Speed.

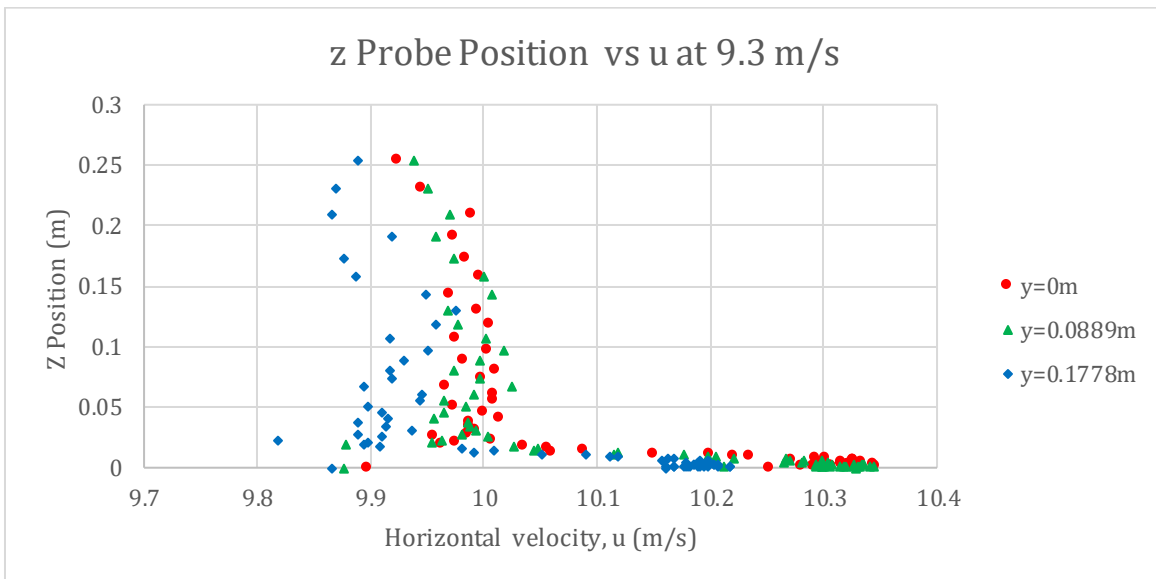


Figure 6: Probe Position and Resulting Horizontal Velocity at 360 RPM Fan Speed.

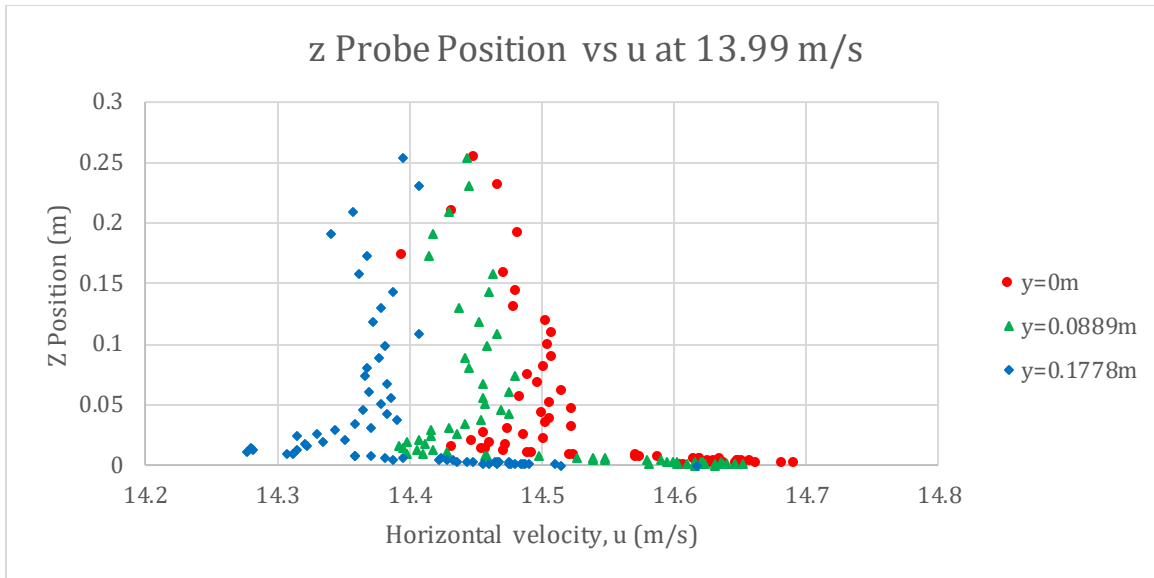


Figure 7: Probe Position and Resulting Horizontal Velocity at 540 RPM Fan Speed.

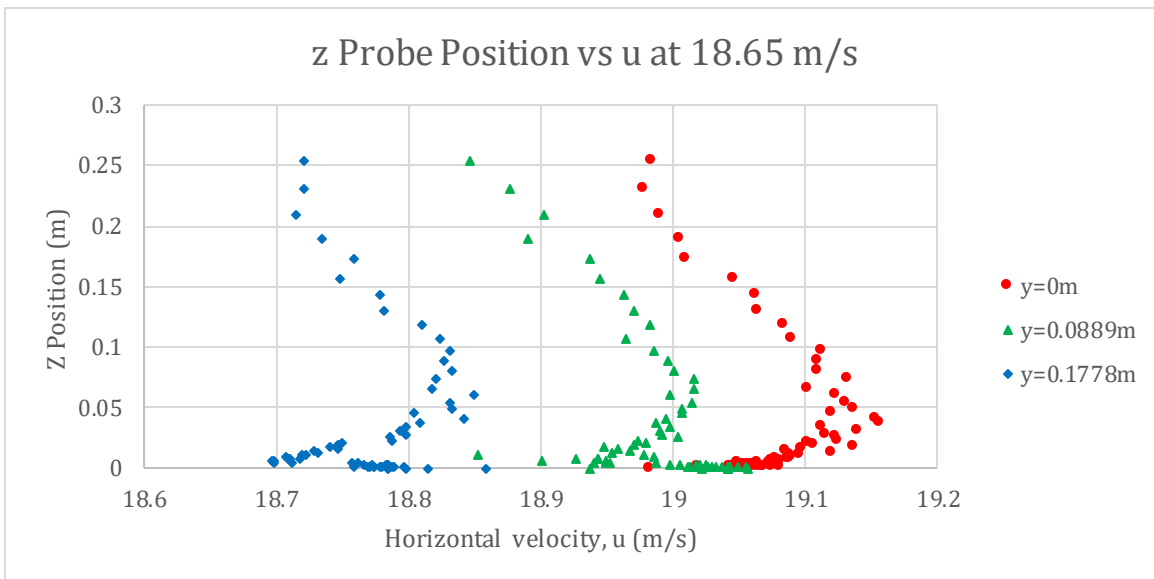


Figure 8: Probe Position and Resulting Horizontal Velocity at 720 RPM Fan Speed.

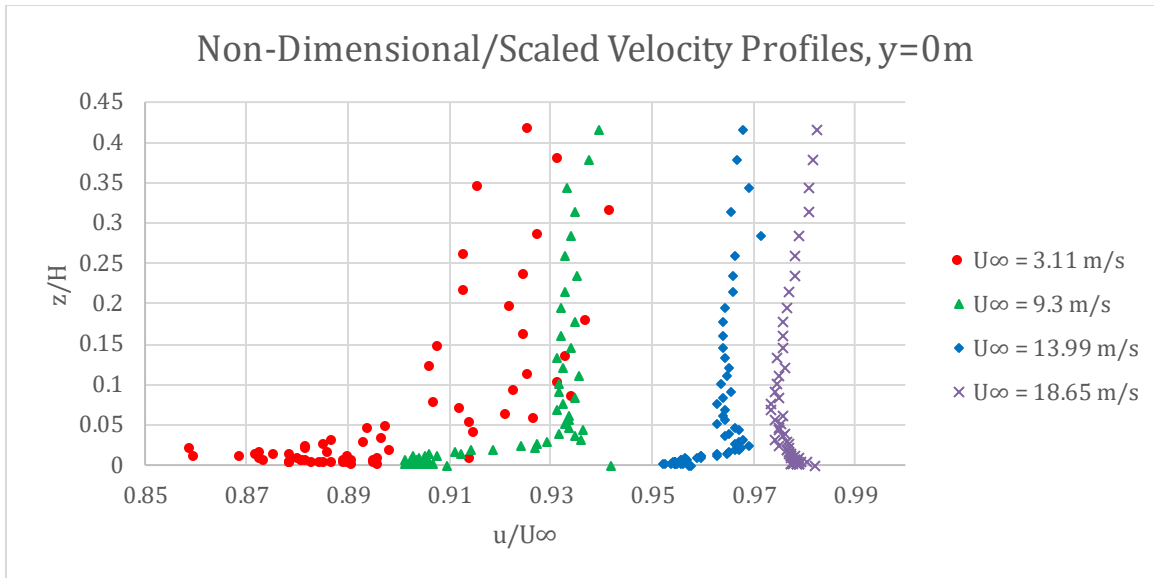


Figure 9: Non-Dimensional Plots for Varying Free Stream Speeds.

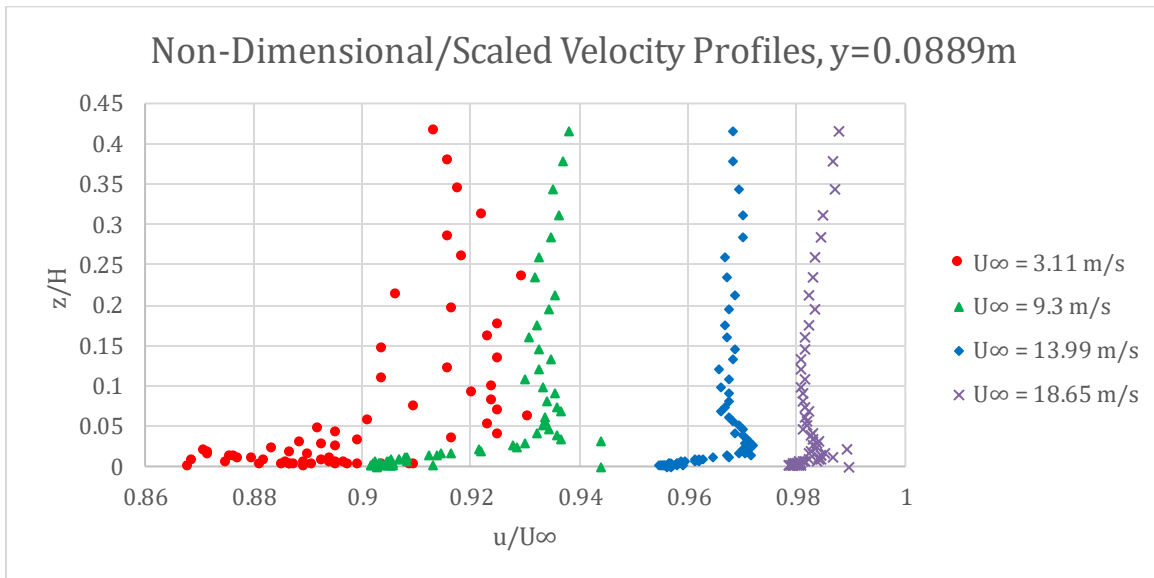


Figure 10: Non-Dimensional Plots for Varying Free Stream Speeds Closest to the *y-direction* Wall.

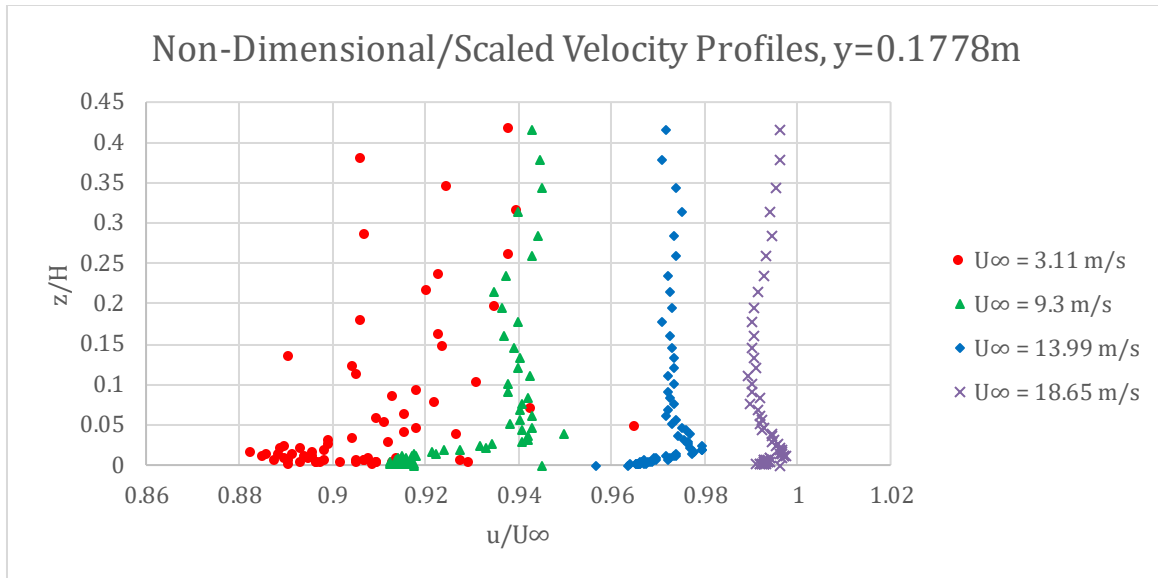


Figure 11: Non-Dimensional Plots for Varying Free Stream Speeds Closest to the y -direction Wall.

RAW DATA (expand)

Pressure Transducer		Ramp 1 Transducer		Ramp 2 Transducer		Manometer			
RPM	Q	Model P (in H2O)	Model P (Pa)	Model P (in H2O)	Model P (Pa)	ΔP_{mano} (Pa)	U_{inf}		
0	0.00108	-0.0011357	-0.282986912	-0.0008864	-0.220867834	0	0		
75	0.0140609	0.0034358	0.856112029	0.0017455	0.434933217	0	0		
150	0.071031	0.0197561	4.922706461	0.0197561	4.922706461	4.98348	4.148987017		
225	0.174745	0.0466324	11.61958164	0.0459119	11.44005177	11.835765	6.394018416		
300	0.326739	0.0829301	20.66402474	0.0830686	20.69853534	15.573375	7.334442136		
375	0.528228	0.1299231	32.37345852	0.1303388	32.47704015	32.39262	10.57788288		
450	0.780616	0.1856717	46.26456018	0.1845905	45.99515325	44.85132	12.44696105		
525	1.0867633	0.2461578	61.33612366	0.2453267	61.12903515	59.80176	14.37251263		
600	1.4427298	0.318088	79.25925931	0.318642	79.39730171	74.7522	16.06895762		
675	1.8465179	0.387358	96.51954229	0.3871087	96.45742321	89.70264	17.60266113		
600	1.4383845	0.3167579	78.92783297	0.3157325	78.67232996	74.7522	16.06895762		
525	1.085441	0.2417525	60.23843744	0.2419741	60.29365439	59.80176	14.37251263		
450	0.7812099	0.1823744	45.44295875	0.181681	45.27018149	44.85132	12.44696105		
375	0.5276345	0.1299784	32.38723784	0.129313	32.22143746	29.90088	10.16290114		
300	0.326307	0.0825423	20.56739506	0.0831517	20.7192417	19.93392	8.297974033		
225	0.174718	0.0464382	11.57119205	0.0468822	11.6818253	9.96696	5.867553709		
150	0.071517	0.0197838	4.929608581	0.0198669	4.950314941	4.98348	4.148987017		
75	0.0161926	0.0029095	0.724971753	0.0041837	1.042469264	1.868805	2.540725285		
0	0.006315	-0.0003601	-0.089727557	-0.0013296	-0.33130175	0	0		
P_corr RU1 (Pa)	P_corr error	u (m/s)	U_{∞} (m/s)	U_{∞} error	P_corr RD1 (Pa)	P_corr error	u (m/s)	U_{∞} (m/s)	U_{∞} error
0.217569732	#DIV/0!	0.866911879	0	#DIV/0!					
1.290828754	#DIV/0!	2.111592114	1.9425	#DIV/0!					
5.122374028	-0.027870891	4.206407658	3.885	0.06362686					
11.43216982	0.034099628	6.284056042	5.8275	0.088601311					
19.95384411	-0.28127937	8.302119942	7.77	-0.05938528					
30.98647262	0.043409498	10.34574539	9.7125	0.081810594					
44.0746686	0.017316133	12.33872383	11.655	0.06362686					
58.27509571	0.025528752	14.18787043	13.5975	0.053923252					
75.16227412	-0.00548578	16.11297272	15.54	0.03291798					
91.42491275	-0.0191998	17.77084149	17.4825	0.006826305	91.20377137	-0.016734528	17.74933615	18.09	-0.027685523
					74.57608773	0.002355948	16.05001765	16.08	-0.000687187
					56.91087106	0.048341202	14.02081737	14.07	0.021047999
					42.92618461	0.042922603	12.17690339	12.06	0.031088797
					30.58591721	-0.022910269	10.27865928	10.05	0.011109145
					19.41380181	0.026092118	8.189002654	8.04	0.031088797
					10.91059072	-0.094675881	6.139031311	6.03	-0.027685523
					4.632966031	0.070335181	4.00041709	4.02	0.031088797
					0.658743301	0.647505598	1.508460081	2.01	0.208887316
					-0.111310487	#DIV/0!	#NUM!	0	#DIV/0!

P_corr RU2 (Pa)	P_corr error	u (m/s)	U_∞ (m/s)	U_∞ error	Hysteresis	Repeatability
-0.061112789	#DIV/0!	#NUM!	0	#DIV/0!	#NUM!	0
0.562160529	#DIV/0!	1.393496527	2.025	#DIV/0!	0.603132	0.0825
4.827340221	0.031331475	4.083472827	4.05	0.023858117	0.2059906	0.165
11.0214252	0.068803309	6.170133984	6.075	0.049893259	0.1450247	0.2475
19.82068798	-0.272729128	8.274372693	8.1	-0.104378472	0.1131173	0.33
31.01497896	0.042529472	10.35050314	10.125	0.042814133	0.0670861	0.4125
43.86259365	0.022044532	12.30900279	12.15	0.023858117	0.1618204	0.495
58.245835	0.026018047	14.18430802	14.175	0.013742387	0.1670531	0.5775
75.60799554	-0.011448433	16.16067804	16.2	-0.008155002	0.0629551	0.66
91.82193502	-0.023625782	17.80938557	18.225	-0.035354818	0.0215053	0.7425

Speed (RPM)	Tunnel Speed Model P (in)	Model P (Pa)	P corrected (Pa)	u (m/s)	Z Position (in)	Z position (m)	Figures	U_{∞} (m/s)	u/U_{∞}	z/H	Re	
120	3.108	0.0129399	3.224286643	3.522122875	3.488011976	0	Density	1.158 kg/m ³	3.108	0.891052	0	174268.2
120	3.108	0.0129953	3.238090882	3.535129229	3.494446237	-0.02475	H	0.61 m	3.108	0.889411	0.001031	174590
120	3.108	0.0133554	3.32781844	3.619670534	3.53598356	-0.02725	Mu	0.00001825 kg/(m-s)	3.108	0.878963	0.001135	176665.3
120	3.108	0.0131338	3.272601481	3.567645116	3.510480295	-0.02975	x (entrance to probe)	0.7874 m	3.108	0.885349	0.001239	175391.1
120	3.108	0.0128014	3.189776044	3.489606988	3.471874155	-0.03275			3.108	0.895194	0.001364	173462.3
120	3.108	0.0133554	3.32781844	3.619670534	3.53598356	-0.03625			3.108	0.878963	0.001509	176665.3
120	3.108	0.0133554	3.32781844	3.619670534	3.53598356	-0.03975			3.108	0.878963	0.001655	176665.3
120	3.108	0.0131615	3.279503601	3.574148293	3.513678326	-0.04375			3.108	0.884543	0.001822	175550.9
120	3.108	0.0129676	3.231188762	3.528626052	3.491230589	-0.048			3.108	0.890231	0.001999	174429.4
120	3.108	0.0130784	3.258797242	3.554638761	3.504075476	-0.053			3.108	0.886967	0.002207	175071.1
120	3.108	0.0132169	3.293307841	3.587154647	3.520065673	-0.05825			3.108	0.882938	0.002425	175870
120	3.108	0.0132723	3.30711208	3.600161002	3.52644145	-0.064			3.108	0.881342	0.002665	176188.6
120	3.108	0.0129399	3.224286643	3.522122875	3.488011976	-0.0705			3.108	0.891052	0.002936	174268.6
120	3.108	0.0135493	3.376133278	3.665192775	3.55814897	-0.0775			3.108	0.873488	0.003227	177772.8
120	3.108	0.0129953	3.238090882	3.535129229	3.494446237	-0.0825			3.108	0.889411	0.00355	174590
120	3.108	0.0128014	3.189776044	3.489606988	3.471874155	-0.09375			3.108	0.895194	0.003904	173462.3
120	3.108	0.0132723	3.30711208	3.600161002	3.52644145	-0.103			3.108	0.881342	0.004289	176188.6
120	3.108	0.0132446	3.30020996	3.593657825	3.523255003	-0.1135			3.108	0.882139	0.004726	176029.4
120	3.108	0.0127737	3.182873924	3.483103811	3.468637581	-0.12475			3.108	0.896029	0.005195	173300.6
120	3.108	0.0133	3.3140142	3.606664179	3.529625019	-0.13725			3.108	0.880547	0.005715	176347.6
120	3.108	0.013577	3.383035398	3.671695952	3.561304195	-0.151			3.108	0.872714	0.006288	177930.4
120	3.108	0.0121916	3.037829738	3.34644318	3.399910178	-0.166			3.108	0.914142	0.006912	169866.8
120	3.108	0.0137155	3.417545997	3.704211838	3.577038575	-0.1825			3.108	0.868875	0.007599	178716.5
120	3.108	0.0140479	3.500371435	3.782249966	3.614521645	-0.20075			3.108	0.859865	0.008359	180589.3
120	3.108	0.0129676	3.231188762	3.528626052	3.491230589	-0.221			3.108	0.890231	0.009202	174429.4
120	3.108	0.0133554	3.32781844	3.619670534	3.53598356	-0.243			3.108	0.878963	0.010118	176665.3
120	3.108	0.0136047	3.389937518	3.678199129	3.564456628	-0.26725			3.108	0.871942	0.011128	178087.9
120	3.108	0.0134662	3.355426919	3.645683243	3.548666461	-0.294			3.108	0.870582	0.012242	177299
120	3.108	0.0131061	3.265699361	3.561141938	3.507279348	-0.3235			3.108	0.886157	0.01347	175231.2
120	3.108	0.013577	3.383035398	3.671695952	3.561304195	-0.3575			3.108	0.872714	0.014813	177930.4
120	3.108	0.0126903	3.162092812	3.463523848	3.45887452	-0.3915			3.108	0.898558	0.016302	172812.8
120	3.108	0.0140756	3.507273554	3.788753143	3.617627703	-0.4305			3.108	0.859127	0.017926	180744.5
120	3.108	0.0132446	3.30020996	3.593657825	3.523255003	-0.4735			3.108	0.882139	0.019716	176029.4
120	3.108	0.0132446	3.30020996	3.593657825	3.523255003	-0.521			3.108	0.882139	0.021694	176029.4
120	3.108	0.0131338	3.272601481	3.567645116	3.510480295	-0.573			3.108	0.885349	0.023859	175391.1
120	3.108	0.0128568	3.203580283	3.502613343	3.478338268	-0.6305			3.108	0.89353	0.026254	173785.3
120	3.108	0.0130784	3.258797242	3.554638761	3.504075476	-0.6935			3.108	0.886967	0.028877	175071.1
120	3.108	0.012746	3.175971804	3.476600634	3.465397984	-0.76275			3.108	0.896667	0.03176	173138.7
120	3.108	0.0085062	2.119523879	2.481215399	2.927574461	-0.839			3.108	1.06163	0.034935	146267.9
120	3.108	0.0121642	3.031002371	3.340010434	3.396640845	-0.923			3.108	0.915022	0.038433	169703.5
120	3.108	0.0128291	3.196678163	3.496110166	3.475107715	-1.01525			3.108	0.894361	0.042274	173623.8
120	3.108	0.0127183	3.169069684	3.470097456	3.462155356	-1.11675			3.108	0.897707	0.046501	172976.7
120	3.108	0.0121919	3.037904491	3.346513611	3.399945957	-1.2285			3.108	0.914132	0.051154	169866.8
120	3.108	0.0118032	2.941050557	3.252527835	3.353269142	-1.35125			3.108	0.926857	0.056265	167536.5
120	3.108	0.0119697	2.982538028	3.29434733	3.373342274	-1.4865			3.108	0.921341	0.061897	168539.4
120	3.108	0.0122473	3.05170873	3.359519966	3.40654656	-1.635			3.108	0.912361	0.06808	170198.4
120	3.108	0.0124136	3.093146366	3.398562506	3.426283911	-1.7985			3.108	0.907105	0.074888	171184.5
120	3.108	0.0115816	2.885833598	3.203232416	3.326365299	-1.9785			3.108	0.934353	0.082383	166192.4
120	3.108	0.011914	2.968659036	3.281270544	3.36664044	-2.17625			3.108	0.923176	0.090618	168204.6
120	3.108	0.0116647	2.906539958	3.222741948	3.336479663	-2.394			3.108	0.931521	0.099865	166697.7
120	3.108	0.0118309	2.947952677	3.261761012	3.35661696	-2.63325			3.108	0.925932	0.109647	167703.8
120	3.108	0.0124413	3.100048486	3.405065684	3.429560455	-2.8965			3.108	0.906239	0.120608	171348.2
120	3.108	0.0116093	2.892735718	3.209735594	3.329740167	-3.18625			3.108	0.933406	0.132673	166361
120	3.108	0.0123859	3.086244247	3.392059329	3.42300423	-3.505			3.108	0.907974	0.145946	171020.6
120	3.108	0.0118587	2.954879714	3.268287666	3.35997351	-3.8555			3.108	0.925007	0.16054	167871.5
120	3.108	0.0114985	2.865127239	3.183722885	3.316220087	-4.241			3.108	0.937212	0.176592	165685.5
120	3.108	0.0119418	2.975586073	3.287797198	3.369987007	-4.665			3.108	0.922259	0.194248	168371.8
120	3.108	0.0122196	3.04480661	3.353016788	3.403247859	-5.1315			3.108	0.913245	0.213672	170033.6
120	3.108	0.0118586	2.954854796	3.268264189	3.359961443	-5.64475			3.108	0.925011	0.235044	167870.9
120	3.108	0.0122197	3.044831528	3.353040265	3.403259773	-6.20925			3.108	0.913242	0.258549	170034.2
120	3.108	0.0117756	2.934173354	3.248778135	3.349930082	-6.83			3.108	0.927781	0.284397	167369.7
120	3.108	0.01136	2.83061664	3.151206998	3.299242075	-7.513			3.108	0.942035	0.312836	164837.2
120	3.108	0.0121364	3.024075334	3.333483779	3.393320565	-8.2645			3.108	0.915917	0.344128	169537.6
120	3.108	0.0116647	2.906539958	3.222741948	3.336479663	-9.091			3.108	0.931521	0.378543	166697.7
120	3.108	0.0118309	2.947952677	3.261761012	3.35661696	-10			3.108	0.925932	0.416393	167703.8
120	3.108	0.0127737	3.182873924	3.483103811	3.468637581	0			3.108	0.896029	0	173300.6

Speed (RPM)	Tunnel Speed	Model P (in)	Model P (Pa)	P corrected (u (m/s))	Z Position (in)	Z position (m)	Figures	Density	U [∞] (m/s)	u/U [∞]	z/H	Re
540	13.986	0.2610926	65.05748751	61.78136473	14.60846098	0	0	1.158 kg/m ³	13.986	0.95739	0	729870.1
540	13.986	0.2640847	65.80304104	62.48832527	14.6912761	-0.02475	0.000629	0.61 m	13.986	0.951994	0.001031	734007.7
540	13.986	0.2630875	65.55456473	62.24971088	14.66372763	-0.02725	0.000692	0.00001825 kg/(m-s)	13.986	0.953782	0.001135	732631.3
540	13.986	0.2625058	65.40962021	62.11314416	14.64763377	-0.02975	0.000756	x (entrance to probe)	13.986	0.95483	0.001239	731827.2
540	13.986	0.2627551	65.47173929	62.17167276	14.6545333	-0.03275	0.000832		13.986	0.95438	0.001364	732172
540	13.986	0.2620626	65.29918629	62.00909332	14.6353599	-0.03625	0.000921		13.986	0.955631	0.001509	731214
540	13.986	0.2625612	65.42342445	62.12615052	14.64916728	-0.03975	0.00101		13.986	0.95473	0.001655	731903.9
540	13.986	0.261813	65.23699246	61.9504943	14.628443	-0.04375	0.001111		13.986	0.956083	0.001822	730868.4
540	13.986	0.26378	65.72711772	62.41229032	14.68286399	-0.048	0.001219		13.986	0.952539	0.001999	733587.4
540	13.986	0.2627551	65.47173929	62.17167276	14.6545333	-0.053	0.001346		13.986	0.95438	0.002207	732172
540	13.986	0.2626166	65.43722869	62.13915687	14.65070063	-0.05825	0.00148		13.986	0.95463	0.002425	731980.5
540	13.986	0.2621734	65.32679477	62.03510603	14.63842933	-0.064	0.001626		13.986	0.95543	0.002665	731367.4
540	13.986	0.2625612	65.42342445	62.12615052	14.64916728	-0.0705	0.001791		13.986	0.95473	0.002936	731903.9
540	13.986	0.2626997	65.45793505	62.1586664	14.65300035	-0.0775	0.001969		13.986	0.95448	0.003227	732095.4
540	13.986	0.2620903	65.30608841	62.0155965	14.63612732	-0.0825	0.002165		13.986	0.955581	0.00355	731252.4
540	13.986	0.2628936	65.50624989	62.20418864	14.65836497	-0.09375	0.002381		13.986	0.95431	0.003904	732363.4
540	13.986	0.2625889	65.43032657	62.13265369	14.64993397	-0.103	0.002616		13.986	0.95468	0.004289	731942.2
540	13.986	0.2617301	65.21633594	61.93103172	14.62614496	-0.1135	0.002883		13.986	0.956233	0.004726	730753.6
540	13.986	0.2619241	65.26467569	61.97657744	14.6315222	-0.12475	0.003169		13.986	0.955881	0.005195	731022.3
540	13.986	0.2615359	65.16794635	61.88543905	14.6207602	-0.13725	0.003486		13.986	0.956585	0.005715	730484.6
540	13.986	0.2613695	65.12648379	61.84637303	14.61614447	-0.151	0.003835		13.986	0.956887	0.006288	730254
540	13.986	0.2620626	65.29918629	62.00909332	14.6353599	-0.166	0.004216		13.986	0.955631	0.006912	731214
540	13.986	0.2615361	65.16799618	61.885486	14.62076575	-0.1825	0.004636		13.986	0.956585	0.007599	730484.9
540	13.986	0.2603719	64.87790781	61.61216474	14.58844324	-0.20075	0.005099		13.986	0.958704	0.008359	728870
540	13.986	0.2598733	64.75366965	61.49510755	14.57457833	-0.221	0.005613		13.986	0.959616	0.009202	728177.2
540	13.986	0.2597625	64.72606118	61.46909484	14.57149545	-0.243	0.006172		13.986	0.959819	0.010118	728023.2
540	13.986	0.2597902	64.73296329	61.47559802	14.57226623	-0.26725	0.006788		13.986	0.959768	0.011128	728061.7
540	13.986	0.2581279	64.31876135	61.08533695	14.52593856	-0.294	0.007468		13.986	0.962829	0.012242	725747.1
540	13.986	0.2580167	64.29105321	61.05923033	14.52283418	-0.3235	0.008217		13.986	0.963035	0.01347	725592
540	13.986	0.2569638	64.0286979	60.81203916	14.49340737	-0.3575	0.009036		13.986	0.96499	0.014813	724121.8
540	13.986	0.2568807	64.00799154	60.79252963	14.49108232	-0.3915	0.009944		13.986	0.965145	0.016302	724005.6
540	13.986	0.2562159	63.84234067	60.63645338	14.47246846	-0.4305	0.010935		13.986	0.966387	0.017926	723075.6
540	13.986	0.2557173	63.71810251	60.51939619	14.45849234	-0.4735	0.012027		13.986	0.967321	0.019716	722377.3
540	13.986	0.2556342	63.69739615	60.49986865	14.45616167	-0.521	0.013233		13.986	0.967477	0.021694	722260.9
540	13.986	0.2548031	63.49030764	60.30476786	14.43283149	-0.573	0.014554		13.986	0.969041	0.023859	721095.3
540	13.986	0.2562713	63.85614491	60.64945973	14.47402053	-0.6305	0.016015		13.986	0.966283	0.026254	723153.2
540	13.986	0.2558558	63.75261311	60.55191207	14.46237595	-0.6935	0.017615		13.986	0.967061	0.028877	722571.4
540	13.986	0.2553572	63.62837495	60.43485488	14.44839006	-0.76275	0.019374		13.986	0.967997	0.03176	721872.6
540	13.986	0.2572962	64.11152334	60.89007729	14.50270385	-0.839	0.021311		13.986	0.964372	0.034935	724586.2
540	13.986	0.2567422	63.97348094	60.76001374	14.4872064	-0.923	0.023444		13.986	0.965404	0.038433	723811.9
540	13.986	0.2556896	63.71120039	60.51289301	14.45771549	-1.01525	0.025787		13.986	0.967373	0.042274	722338.5
540	13.986	0.2562999	63.86304703	60.65596291	14.4747965	-1.11675	0.028365		13.986	0.966231	0.046501	723191.9
540	13.986	0.2580445	64.29798024	61.06575698	14.52361034	-1.2285	0.031204		13.986	0.962984	0.051154	725630.8
540	13.986	0.2573239	64.11842546	60.89658047	14.50347829	-1.35125	0.034322		13.986	0.96432	0.056265	724624.9
540	13.986	0.2574624	64.15293606	60.92909635	14.50734986	-1.4865	0.037757		13.986	0.964063	0.061897	724818.4
540	13.986	0.2572408	64.0977191	60.87707094	14.50115485	-1.635	0.041529		13.986	0.964475	0.06808	724508.8
540	13.986	0.2580723	64.30490728	61.07228364	14.52438645	-1.7985	0.045682		13.986	0.962932	0.074888	725669.5
540	13.986	0.2574347	64.14603394	60.92259318	14.50657562	-1.9785	0.050254		13.986	0.964115	0.082383	724779.7
540	13.986	0.2566591	63.95277458	60.74050421	14.48488036	-2.17625	0.055277		13.986	0.965559	0.090618	723695.7
540	13.986	0.2577671	64.22885938	61.0006313	14.51586367	-2.394	0.060808		13.986	0.963498	0.099685	725243.7
540	13.986	0.25713	64.07011062	60.85105823	14.49805636	-2.63325	0.066885		13.986	0.964681	0.109647	724354
540	13.986	0.2568807	64.00799154	60.79252963	14.49108232	-2.8965	0.073571		13.986	0.965145	0.120608	724005.6
540	13.986	0.2572685	64.10462122	60.88357411	14.50192937	-3.18625	0.080931		13.986	0.964423	0.132673	724547.5
540	13.986	0.2574901	64.15983818	60.93559953	14.50812405	-3.505	0.089027		13.986	0.964012	0.145946	724857
540	13.986	0.2573793	64.1322297	60.90958682	14.50502704	-3.8555	0.09793		13.986	0.964217	0.16054	724702.3
540	13.986	0.2574904	64.15991293	60.93566996	14.50813243	-4.241	0.107721		13.986	0.964011	0.176592	724857.5
540	13.986	0.2573516	64.12532758	60.90308364	14.50425268	-4.665	0.118491		13.986	0.964269	0.194248	724663.6
540	13.986	0.2564652	63.90445974	60.69498197	14.47945146	-5.1315	0.13034		13.986	0.965921	0.213672	723424.5
540	13.986	0.2565206	63.91826398	60.70798833	14.48100278	-5.64475	0.143377		13.986	0.965817	0.235044	723502
540	13.986	0.2561882	63.83543855	60.6299502	14.47169236	-6.20925	0.157715		13.986	0.966438	0.258549	723036.8
540	13.986	0.2534728	63.15883147	59.99245101	14.39540934	-6.83	0.173482		13.986	0.97156	0.284397	719225.6
540	13.986	0.2566037	63.93897034	60.72749786	14.48332945	-7.513	0.19083		13.986	0.965662	0.312836	723618.2
540	13.986	0.2548309	63.49723468	60.31129451	14.43361248	-8.2645	0.209918		13.986	0.968988	0.344128	721134.3
540	13.986	0.2560497	63.80092795	60.59743431	14.46781125	-9.091	0.230911		13.986	0.966698	0.378543	722842.9
540	13.986	0.2553849	63.63527707	60.44135806	14.44916741	-10	0.254		13.986	0.967945	0.416393	721911.4
540	13.986	0.2609813	65.02975445	61.75523464	14.60537136	0	0		13.986	0.957593	0	729715.7

Speed (RPM)	Tunnel Speed Model P (in)	Model P (Pa)	P corrected (Pa)	u (m/s)	Z Position (in)	Z position (m)	Figures	U ∞ (m/s)	u/U ∞	z/H	Re	
120	3.108	0.0129953	3.238090882	3.535129229	3.494446237	0	Density	1.158 kg/m ³	3.108	0.889411	0	174590
120	3.108	0.0130784	3.258797242	3.554638761	3.504075476	-0.02475	H	0.61 m	3.108	0.886967	0.001031	175071.1
120	3.108	0.0126629	3.155265445	3.457091102	3.455660972	-0.02725	Mu	0.00001825 kg/(m-s)	3.108	0.899394	0.001135	172652.2
120	3.108	0.0132723	3.30711208	3.600161002	3.52644145	-0.02975	x (entrance to probe)	0.7874 m	3.108	0.881342	0.001239	176188.6
120	3.108	0.0130784	3.258797242	3.554638761	3.504075476	-0.03275			3.108	0.886967	0.001364	175071.1
120	3.108	0.0129399	3.224286643	3.522122875	3.488011976	-0.03625			3.108	0.891052	0.001509	174268.6
120	3.108	0.0127183	3.169069684	3.470097456	3.462155356	-0.03975			3.108	0.897707	0.001655	172976.7
120	3.108	0.0123305	3.072440007	3.379052975	3.416435423	-0.04375			3.108	0.90972	0.001822	170692.5
120	3.108	0.0123582	3.079342127	3.385556152	3.419721404	-0.048			3.108	0.908846	0.001999	170856.6
120	3.108	0.0130507	3.251895122	3.548135584	3.500868673	-0.053			3.108	0.88778	0.002207	174910.9
120	3.108	0.0131338	3.272601481	3.567645116	3.510480295	-0.05825			3.108	0.885349	0.002425	175391.1
120	3.108	0.0128014	3.189776044	3.489606988	3.471874155	-0.064			3.108	0.895194	0.002665	173462.3
120	3.108	0.0125244	3.120754846	3.424575216	3.439371361	-0.0705			3.108	0.903654	0.002936	171838.4
120	3.108	0.0129953	3.238090882	3.535129229	3.494446237	-0.0775			3.108	0.889411	0.003227	174590
120	3.108	0.0128291	3.196678163	3.496110166	3.475107715	-0.08525			3.108	0.894361	0.00355	173623.8
120	3.108	0.012746	3.175971804	3.476600634	3.465397984	-0.09375			3.108	0.896867	0.003904	173138.7
120	3.108	0.0128014	3.189776044	3.489606988	3.471874155	-0.103			3.108	0.895194	0.004289	173462.3
120	3.108	0.0131061	3.265699361	3.561141938	3.507279348	-0.1135			3.108	0.886157	0.004726	175231.2
120	3.108	0.0134939	3.362329039	3.65218642	3.55183011	-0.12475			3.108	0.875042	0.005195	177457.1
120	3.108	0.0128845	3.210482403	3.50911652	3.481565824	-0.13725			3.108	0.892702	0.005715	173946.5
120	3.108	0.0132446	3.30020996	3.593657825	3.523255003	-0.151			3.108	0.882139	0.006288	176029.4
120	3.108	0.0137155	3.417545997	3.704211838	3.577038575	-0.166			3.108	0.868875	0.006912	178716.5
120	3.108	0.0128291	3.196678163	3.496110166	3.475107715	-0.1825			3.108	0.894361	0.007599	173623.8
120	3.108	0.0134108	3.341622679	3.632676888	3.542330687	-0.20075			3.108	0.877388	0.008359	176982.4
120	3.108	0.0128291	3.196678163	3.496110166	3.475107715	-0.221			3.108	0.894361	0.009202	173623.8
120	3.108	0.0133277	3.32091632	3.613167357	3.53280572	-0.243			3.108	0.879754	0.010118	176506.6
120	3.108	0.0134385	3.348524799	3.639180066	3.545499989	-0.26725			3.108	0.876604	0.011128	177140.8
120	3.108	0.0134662	3.35426919	3.645683243	3.548666461	-0.294			3.108	0.875822	0.012242	177299
120	3.108	0.0129676	3.231188762	3.528626052	3.491230589	-0.3235			3.108	0.890231	0.01347	174429.4
120	3.108	0.0136047	3.389937518	3.678199129	3.564456628	-0.3575			3.108	0.871942	0.014813	178087.9
120	3.108	0.0136047	3.389937518	3.678199129	3.564456628	-0.3915			3.108	0.871942	0.016302	178087.9
120	3.108	0.0130784	3.258797242	3.554638761	3.504075476	-0.4305			3.108	0.886967	0.017926	175071.1
120	3.108	0.0136324	3.396839638	3.684702307	3.567606275	-0.4735			3.108	0.871172	0.019716	178245.3
120	3.108	0.0131892	3.286405721	3.58065147	3.51687345	-0.521			3.108	0.88374	0.021694	175710.6
120	3.108	0.0128014	3.189776044	3.489606988	3.471874155	-0.573			3.108	0.895194	0.023859	173462.3
120	3.108	0.0128845	3.210482403	3.50911652	3.481565824	-0.6305			3.108	0.892702	0.026254	173946.5
120	3.108	0.013023	3.244993002	3.541632406	3.497658929	-0.6935			3.108	0.888594	0.028877	174750.6
120	3.108	0.0126629	3.155265445	3.457091102	3.455660972	-0.76275			3.108	0.899394	0.03176	172652.2
120	3.108	0.0121086	3.017148296	3.326957125	3.389997032	-0.839			3.108	0.916815	0.034935	169371.5
120	3.108	0.0118586	2.954854796	3.268264189	3.359961443	-0.923			3.108	0.925011	0.038433	167870.9
120	3.108	0.0128014	3.189776044	3.489606988	3.471874155	-1.01525			3.108	0.895194	0.042274	173462.3
120	3.108	0.0129122	3.217384523	3.515619697	3.484790391	-1.11675			3.108	0.891876	0.046501	174107.6
120	3.108	0.0119141	2.968683953	3.281294021	3.366652484	-1.2285			3.108	0.923172	0.051154	168205.2
120	3.108	0.0126075	3.141461205	3.444084747	3.449154359	-1.35125			3.108	0.90109	0.056265	172327.2
120	3.108	0.0116924	2.913442078	3.229245126	3.339844311	-1.4865			3.108	0.930582	0.061897	166865.8
120	3.108	0.0118587	2.954879714	3.268287666	3.35997351	-1.635			3.108	0.925007	0.06808	167871.5
120	3.108	0.0123305	3.072440007	3.379052975	3.416435423	-1.7985			3.108	0.90972	0.074888	170692.5
120	3.108	0.0118863	2.961756916	3.274767366	3.363302599	-1.9785			3.108	0.924092	0.082383	168037.8
120	3.108	0.0119974	2.989440148	3.300850507	3.376670191	-2.17625			3.108	0.920433	0.090618	168705.7
120	3.108	0.0118863	2.961756916	3.274767366	3.363302599	-2.394			3.108	0.924092	0.099685	168037.8
120	3.108	0.0125244	3.120754846	3.424575216	3.439371361	-2.63325			3.108	0.903654	0.109647	171838.4
120	3.108	0.0121364	3.024075334	3.333483779	3.393320565	-2.8965			3.108	0.915917	0.120608	169537.6
120	3.108	0.0118586	2.954854796	3.268264189	3.359961443	-3.18625			3.108	0.925011	0.132673	167870.9
120	3.108	0.0125244	3.120754846	3.424575216	3.439371361	-3.505			3.108	0.903654	0.145946	171838.4
120	3.108	0.0119142	2.968708871	3.281317498	3.366664528	-3.8555			3.108	0.923169	0.16054	168205.8
120	3.108	0.0118586	2.954854796	3.268264189	3.359961443	-4.241			3.108	0.925011	0.165952	167870.9
120	3.108	0.0121085	3.017123379	3.326933648	3.389985071	-4.665			3.108	0.916818	0.194248	169370.9
120	3.108	0.0124413	3.100048486	3.405065684	3.429560455	-5.1315			3.108	0.906239	0.213672	171348.2
120	3.108	0.0117201	2.920344197	3.235748303	3.343205572	-5.64475			3.108	0.929647	0.235044	167033.7
120	3.108	0.0120531	3.003319139	3.313927293	3.383352158	-6.20925			3.108	0.918616	0.258549	169039.5
120	3.108	0.0121364	3.024075334	3.333483779	3.393320565	-6.83			3.108	0.915917	0.284397	169537.6
120	3.108	0.0119418	2.975586073	3.287797198	3.369987007	-7.513			3.108	0.922259	0.312836	168371.8
120	3.108	0.0120808	3.010221259	3.32043047	3.386670238	-8.2645			3.108	0.917716	0.344128	169205.3
120	3.108	0.0121363	3.024050416	3.333460302	3.393308615	-9.091			3.108	0.91592	0.378543	169537
120	3.108	0.0122196	3.04480661	3.353016788	3.403247859	-10			3.108	0.913245	0.416393	170033.6
120	3.108	0.0137432	3.424448117	3.710715016	3.580177153	0			3.108	0.868113	0	178873.3

Speed (RPM)	Tunnel Speed Model P (in)	Model P (Pa)	P corrected (Pa)	u (m/s)	Z Position (in)	Z position (m)	Figures	U _∞ (m/s)	u/U _∞	z/H	Re	
120	3.108	0.0123582	3.079342127	3.385556152	3.419721404	0	Density	1.158 kg/m ³	3.108	0.908846	0	170856.6
120	3.108	0.0122197	3.044831528	3.353040265	3.403259773	-0.02475	H	0.61 m	3.108	0.913242	0.001031	170034.2
120	3.108	0.0127183	3.169069684	3.470097456	3.462155356	-0.02725	Mu	0.00001825 kg/(m-s)	3.108	0.897707	0.001135	172976.7
120	3.108	0.0123305	3.072440007	3.379052975	3.416435423	-0.02975	x (entrance to probe)	0.7874 m	3.108	0.90972	0.001239	170692.5
120	3.108	0.0123305	3.072440007	3.379052975	3.416435423	-0.03275			3.108	0.90972	0.001364	170692.5
120	3.108	0.0128568	3.203580283	3.502613343	3.478338268	-0.03625			3.108	0.89353	0.001509	173785.3
120	3.108	0.012746	3.175971804	3.476600634	3.465397984	-0.03975			3.108	0.896867	0.001655	173138.7
120	3.108	0.012469	3.106950606	3.411568861	3.432833873	-0.04375			3.108	0.905374	0.002822	171511.8
120	3.108	0.0117203	2.920394032	3.235795257	3.343229829	-0.048			3.108	0.92964	0.001999	167034.9
120	3.108	0.0125798	3.134559085	3.43758157	3.445896446	-0.053			3.108	0.901942	0.002207	172164.4
120	3.108	0.012746	3.175971804	3.476600634	3.465397984	-0.05825			3.108	0.896867	0.002425	173138.7
120	3.108	0.012469	3.106950606	3.411568861	3.432833873	-0.064			3.108	0.905374	0.002665	171511.8
120	3.108	0.0129399	3.224286643	3.522122875	3.488011976	-0.0705			3.108	0.891052	0.002936	174268.6
120	3.108	0.0124136	3.093146366	3.398562506	3.426283911	-0.0775			3.108	0.907105	0.003227	171184.5
120	3.108	0.0124136	3.093146366	3.398562506	3.426283911	-0.08525			3.108	0.907105	0.00355	171184.5
120	3.108	0.0126906	3.162167564	3.463594279	3.458909688	-0.09375			3.108	0.898549	0.003904	172814.6
120	3.108	0.0130507	3.251895122	3.548135584	3.500868673	-0.103			3.108	0.88778	0.004289	174919.0
120	3.108	0.0117757	2.934198272	3.248801612	3.349942186	-0.1135			3.108	0.927777	0.004726	167370.3
120	3.108	0.0129676	3.231188762	3.528626052	3.491230589	-0.12475			3.108	0.890231	0.005195	174429.4
120	3.108	0.0128014	3.189776044	3.489606988	3.471874155	-0.13725			3.108	0.895194	0.005715	173462.3
120	3.108	0.012192	3.037929408	3.346537088	3.399957883	-0.151			3.108	0.914129	0.006288	169866.2
120	3.108	0.0123859	3.086244247	3.392059329	3.42300423	-0.166			3.108	0.907974	0.006912	171020.6
120	3.108	0.0128291	3.196678163	3.496110166	3.475107715	-0.1825			3.108	0.894361	0.007599	173632.8
120	3.108	0.0131338	3.272601481	3.567645116	3.510480295	-0.20075			3.108	0.885349	0.008359	175391.1
120	3.108	0.0127737	3.182873924	3.483103811	3.468637581	-0.221			3.108	0.896029	0.009202	173300.6
120	3.108	0.0131061	3.265699361	3.561141938	3.507279348	-0.243			3.108	0.886157	0.010118	175231.2
120	3.108	0.0129122	3.217384523	3.515619697	3.484790391	-0.26725			3.108	0.891876	0.011128	174107.6
120	3.108	0.013023	3.244993002	3.541632406	3.497658929	-0.294			3.108	0.888594	0.012242	174750.6
120	3.108	0.0132169	3.293307841	3.587154647	3.520065673	-0.3235			3.108	0.882938	0.01347	175870
120	3.108	0.0127737	3.182873924	3.483103811	3.468637581	-0.3575			3.108	0.890629	0.014813	173300.6
120	3.108	0.0126906	3.162167564	3.463594279	3.458909688	-0.3915			3.108	0.898549	0.016302	172814.6
120	3.108	0.0129953	3.238008082	3.535129229	3.494446237	-0.4305			3.108	0.889411	0.017926	174590
120	3.108	0.0128568	3.203580283	3.502613343	3.478338268	-0.4735			3.108	0.89353	0.019716	173785.3
120	3.108	0.0129676	3.231188762	3.528626052	3.491230589	-0.521			3.108	0.890231	0.021694	174429.4
120	3.108	0.0126629	3.155265445	3.457091102	3.455660972	-0.573			3.108	0.899394	0.023859	172652.2
120	3.108	0.0122472	3.051683813	3.359496488	3.406534657	-0.6305			3.108	0.912364	0.026254	170197.8
120	3.108	0.0126629	3.155265445	3.457091102	3.455660972	-0.6935			3.108	0.899394	0.028877	172652.2
120	3.108	0.0124967	3.113852726	3.418072038	3.436104171	-0.76275			3.108	0.904513	0.03176	171675.1
120	3.108	0.0118032	2.941050557	3.255257835	3.353269142	-0.839			3.108	0.926857	0.034935	167536.5
120	3.108	0.0121364	3.024075334	3.333483779	3.393320565	-0.923			3.108	0.915917	0.038433	169537.6
120	3.108	0.012053	3.003294222	3.313903816	3.383340173	-1.01525			3.108	0.918619	0.042274	169038.9
120	3.108	0.0107229	2.671867885	3.001633921	3.21999041	-1.11675			3.108	0.96522	0.046501	160877.6
120	3.108	0.0122748	3.058561015	3.365976189	3.409818288	-1.2285			3.108	0.911486	0.051154	170361.8
120	3.108	0.0123305	3.072440007	3.379052975	3.416435423	-1.35125			3.108	0.90972	0.056265	170692.5
120	3.108	0.0121362	3.024025499	3.333436825	3.393296666	-1.4865			3.108	0.915923	0.061897	169536.4
120	3.108	0.0113323	2.82371452	3.144703821	3.295835977	-1.635			3.108	0.943008	0.06808	164667
120	3.108	0.011942	2.975635908	3.287844153	3.370011071	-1.7985			3.108	0.922252	0.074888	168373
120	3.108	0.0122196	3.04480661	3.353016788	3.403247859	-1.9785			3.108	0.913245	0.082383	170033.6
120	3.108	0.012053	3.003294222	3.313903816	3.383340173	-2.17625			3.108	0.918619	0.090618	169038.9
120	3.108	0.0116647	2.906539958	3.222741948	3.336479663	-2.394			3.108	0.931521	0.099685	166697.7
120	3.108	0.012469	3.106950606	3.411568861	3.432833873	-2.63325			3.108	0.905374	0.109647	171511.8
120	3.108	0.0124967	3.113852726	3.418072038	3.436104171	-2.8965			3.108	0.904513	0.120608	171675.1
120	3.108	0.0129399	3.224286643	3.522122875	3.488011976	-3.18625			3.108	0.891052	0.132673	174268.6
120	3.108	0.0118863	2.961756916	3.274767366	3.363302599	-3.505			3.108	0.924092	0.145946	168037.8
120	3.108	0.011914	2.968659036	3.281270544	3.36664044	-3.8555			3.108	0.923176	0.16054	168204.6
120	3.108	0.0124413	3.100048486	3.405065684	3.429560455	-4.241			3.108	0.906239	0.176592	171348.2
120	3.108	0.0115539	2.878931479	3.196729239	3.322987003	-4.665			3.108	0.935303	0.194248	166023.6
120	3.108	0.0119975	2.989465065	3.300873984	3.376682199	-5.1315			3.108	0.92043	0.213672	168706.3
120	3.108	0.0119141	2.968683953	3.281294021	3.366652484	-5.64475			3.108	0.923172	0.235044	168205.2
120	3.108	0.0114708	2.858225119	3.177219707	3.312831445	-6.20925			3.108	0.93817	0.258549	165516.2
120	3.108	0.0124136	3.093146366	3.398562506	3.426283911	-6.83			3.108	0.907105	0.284397	171184.5
120	3.108	0.0114154	2.84442088	3.164213353	3.306043742	-7.513			3.108	0.940096	0.312836	165177
120	3.108	0.0118586	2.954854796	3.268264189	3.359961443	-8.2645			3.108	0.925011	0.344128	167870.9
120	3.108	0.0124413	3.100048486	3.405065684	3.429560455	-9.091			3.108	0.906239	0.378543	171348.2
120	3.108	0.0114708	2.858225119	3.177219707	3.312831445	-10			3.108	0.93817	0.416393	165516.2
120	3.108	0.0129399	3.224286643	3.522122875	3.488011976	0			3.108	0.891052	0	174268.6

Speed (RPM)	Tunnel Speed Model P (in)	Model P (Pa)	P corrected (Pa)	u (m/s)	Z Position (in)	Z position (m)	Figures	U_{∞} (m/s)	u/U_{∞}	z/H	Re	
360	9.324	0.12524	31.20655176	29.88701307	10.16054428	0	Density	1.158 kg/m ³	9.324	0.917667	0	507642.6
360	9.324	0.1261541	31.43432171	30.10161792	10.19695812	-0.02475	H	0.61 m	9.324	0.914399	0.001031	509461.9
360	9.324	0.125794	31.34459416	30.01707661	10.18262881	-0.02725	Mu	0.00001825 kg/(m-s)	9.324	0.915677	0.001135	508746
360	9.324	0.1256556	31.31010847	29.9845842	10.17711616	-0.02975	x (entrance to probe)	0.7874 m	9.324	0.916173	0.001239	508470.6
360	9.324	0.1260987	31.42051747	30.08861156	10.19475492	-0.03275			9.324	0.914588	0.001364	509351.9
360	9.324	0.1264039	31.49656538	30.1602639	10.20688648	-0.03625			9.324	0.913501	0.001509	509958
360	9.324	0.1254339	31.2548666	29.93253531	10.16827932	-0.03975			9.324	0.916969	0.001655	508029.1
360	9.324	0.1254339	31.2548666	29.93253531	10.16827932	-0.04375			9.324	0.916969	0.001822	508029.1
360	9.324	0.1259602	31.38600687	30.05609568	10.18924484	-0.048			9.324	0.915083	0.001999	509076.6
360	9.324	0.12524	31.20655176	29.88701307	10.16054428	-0.053			9.324	0.917667	0.002207	507642.6
360	9.324	0.1266811	31.56563641	30.22534263	10.21789257	-0.05825			9.324	0.912517	0.002425	510507.9
360	9.324	0.1259879	31.39290899	30.06259885	10.1903471	-0.064			9.324	0.914984	0.002665	509131.6
360	9.324	0.1257109	31.3238878	29.99756708	10.17931919	-0.0705			9.324	0.915975	0.002936	508580.7
360	9.324	0.1266536	31.55878413	30.2188864	10.21680123	-0.0775			9.324	0.912614	0.003227	510453.3
360	9.324	0.1256832	31.31698568	29.9910639	10.17821574	-0.08525			9.324	0.916074	0.003555	508525.5
360	9.324	0.1258494	31.3583984	30.03008297	10.18483463	-0.09375			9.324	0.915479	0.003904	508856.2
360	9.324	0.1263759	31.48958851	30.15369029	10.20577409	-0.103			9.324	0.9136	0.004289	509902.4
360	9.324	0.1259325	31.37910476	30.0495925	10.18814247	-0.1135			9.324	0.915182	0.004726	509021.5
360	9.324	0.1258494	31.3583984	30.03008297	10.18483463	-0.12475			9.324	0.915479	0.005195	508856.2
360	9.324	0.1262927	31.46885723	30.13415728	10.202468	-0.13725			9.324	0.913897	0.005715	509737.2
360	9.324	0.1263204	31.47575935	30.1406046	10.20356883	-0.151			9.324	0.913798	0.006288	509792.2
360	9.324	0.1261542	31.43434663	30.1016414	10.19696209	-0.166			9.324	0.914399	0.006912	509461.9
360	9.324	0.1256832	31.31698568	29.9910639	10.17821574	-0.1825			9.324	0.916074	0.007599	508525.5
360	9.324	0.1259602	31.38600687	30.05609568	10.18924484	-0.20075			9.324	0.915083	0.008359	509076.6
360	9.324	0.1261818	31.44122383	30.1081211	10.19805954	-0.221			9.324	0.914292	0.009202	509517
360	9.324	0.1259879	31.39290899	30.06259885	10.1903471	-0.243			9.324	0.914984	0.010118	509131.6
360	9.324	0.1251569	31.1858454	29.86750354	10.15722745	-0.26725			9.324	0.917967	0.011128	507476.9
360	9.324	0.1254339	31.2548666	29.93253531	10.16827932	-0.294			9.324	0.916969	0.012242	508029.1
360	9.324	0.1252954	31.220356	29.90001942	10.16275489	-0.3235			9.324	0.917468	0.01347	507573.1
360	9.324	0.1239935	30.89595637	29.59437009	10.11067769	-0.3575			9.324	0.922193	0.014813	505151.2
360	9.324	0.1241874	30.94427121	29.63989233	10.11845086	-0.3915			9.324	0.921485	0.016302	505539.5
360	9.324	0.1234672	30.76481609	29.47080972	10.08954892	-0.4305			9.324	0.921425	0.017926	504095.5
360	9.324	0.1225244	30.52989485	29.24946692	10.05158834	-0.4735			9.324	0.927615	0.019716	502198.9
360	9.324	0.1210286	30.15718038	28.89829535	9.991066018	-0.521			9.324	0.933234	0.021694	499175.1
360	9.324	0.1214718	30.26761429	29.00234619	10.00903671	-0.573			9.324	0.931558	0.023859	500073
360	9.324	0.1207516	30.08815918	28.83326358	9.979817903	-0.6305			9.324	0.934286	0.026254	498613.1
360	9.324	0.1190056	29.65310137	28.42335211	9.90862434	-0.6935			9.324	0.940998	0.028877	495056.2
360	9.324	0.1186731	29.57025102	28.34529051	9.895008513	-0.76275			9.324	0.942293	0.03176	494375.9
360	9.324	0.1187562	29.59095738	28.36480004	9.898413202	-0.839			9.324	0.941969	0.034935	494546
360	9.324	0.1167895	29.10090687	27.90307446	9.817518876	-0.923			9.324	0.949731	0.038433	490504.3
360	9.324	0.1190332	29.65997858	28.42983182	9.909753716	-1.01525			9.324	0.940891	0.042274	495112.6
360	9.324	0.1185069	29.5288383	28.30627145	9.888195619	-1.11675			9.324	0.942943	0.046501	494035.5
360	9.324	0.1196712	29.81895159	28.57961619	9.935824505	-1.2285			9.324	0.938422	0.051154	496415.1
360	9.324	0.119144	29.68758706	28.45584452	9.914286289	-1.35125			9.324	0.940461	0.056265	495339
360	9.324	0.1185346	29.53574042	28.31277462	9.889331427	-1.4865			9.324	0.942834	0.061897	494092.2
360	9.324	0.1191717	29.69448918	28.4623477	9.915419109	-1.635			9.324	0.940354	0.06808	495395.6
360	9.324	0.1190609	29.6668807	28.43633499	9.910887053	-1.7985			9.324	0.940784	0.074888	495169.2
360	9.324	0.1187562	29.59095738	28.36480004	9.898413202	-1.9785			9.324	0.941969	0.082383	494546
360	9.324	0.1198652	29.86729134	28.62516191	9.943738434	-2.17625			9.324	0.937676	0.090618	496810.5
360	9.324	0.1198929	29.87419346	28.63166508	9.944867899	-2.394			9.324	0.937569	0.099685	496867
360	9.324	0.1186454	29.5633489	28.33878733	9.893873356	-2.63325			9.324	0.942401	0.109647	494319.2
360	9.324	0.1192549	29.71522045	28.48188071	9.918820879	-2.8965			9.324	0.940031	0.120608	495565.6
360	9.324	0.1191994	29.7013913	28.46885088	9.916551799	-3.18625			9.324	0.940246	0.132673	495452.2
360	9.324	0.1195322	29.7843164	28.54698291	9.930150337	-3.505			9.324	0.938959	0.145946	496131.6
360	9.324	0.1200314	29.90870406	28.66418097	9.950513299	-3.8555			9.324	0.937037	0.16054	497149
360	9.324	0.1192271	29.70829342	28.47535406	9.91768436	-4.241			9.324	0.940139	0.176592	495508.8
360	9.324	0.1202253	29.9570189	28.70970321	9.958411483	-4.665			9.324	0.936294	0.194248	497543.6
360	9.324	0.1206408	30.0605507	28.80725087	9.975315106	-5.1315			9.324	0.934707	0.213672	498388.2
360	9.324	0.119976	29.89489882	28.65117461	9.948255523	-5.64475			9.324	0.93725	0.235044	497036.2
360	9.324	0.1184792	29.52193618	28.29976827	9.88705968	-6.20925			9.324	0.943051	0.258549	493978.7
360	9.324	0.1182299	29.4588171	28.24123967	9.876830352	-6.83			9.324	0.944028	0.284397	493467.7
360	9.324	0.1192549	29.71522045	28.48188071	9.918820879	-7.513			9.324	0.940031	0.312836	495565.6
360	9.324	0.1179806	29.39769802	28.18271108	9.866590419	-8.2645			9.324	0.945007	0.344128	492956.1
360	9.324	0.118036	29.41150226	28.19571743	9.868866878	-9.091			9.324	0.944789	0.378543	493069.8
360	9.324	0.1185346	29.53574042	28.31277462	9.889331427	-10			9.324	0.942834	0.416393	494092.2
360	9.324	0.1179806	29.39769802	28.18271108	9.866590419	0			9.324	0.945007	0	492956.1

Speed (RPM)	Tunnel Speed Model P (in)	Model P (Pa)	P corrected (Pa)	u (m/s)	Z Position (in)	Z position (m)	Figures	U [∞] (m/s)	u/U [∞]	z/H	Re
540	13.986	0.2577117	64.21505514	60.98762495	14.51431608	0	Density	1.158 kg/m ³	0.9636	0	725166.4
540	13.986	0.2575733	64.18056945	60.95513254	14.51044916	-0.02475	H	0.61 m	0.963857	0.001031	724973.2
540	13.986	0.2566591	63.95277458	60.74050421	14.48488036	-0.02725	Mu	0.00001825 kg/(m-s)	0.965559	0.001135	723695.7
540	13.986	0.2568807	64.00799154	60.79252963	14.49108232	-0.02975	x (entrance to probe)	0.7874 m	0.965145	0.001239	724005.6
540	13.986	0.2564652	63.90445974	60.69498197	14.47945146	-0.03275			0.965921	0.001364	723424.5
540	13.986	0.2565342	63.69739615	60.49988665	14.45616167	-0.03625			0.967477	0.001509	722260.9
540	13.986	0.2566868	63.9596767	60.74700739	14.48565575	-0.03975			0.965507	0.001655	723734.5
540	13.986	0.2567699	63.98038306	60.76651692	14.48798167	-0.04375			0.965352	0.001822	723850.7
540	13.986	0.2563821	63.88375339	60.67547244	14.47712417	-0.048			0.966076	0.001999	723308.2
540	13.986	0.2557727	63.73190675	60.53240254	14.46004591	-0.053			0.967217	0.002207	722455
540	13.986	0.2563267	63.86994915	60.66246609	14.47557243	-0.05825			0.966179	0.002425	723230.7
540	13.986	0.256022	63.79402583	60.59093114	14.4670349	-0.064			0.96675	0.002665	722804.1
540	13.986	0.2559666	63.78022159	60.57792478	14.46548209	-0.0705			0.966853	0.002936	722726.6
540	13.986	0.2549417	63.52484316	60.33730722	14.43672481	-0.0775			0.968779	0.003227	721289.8
540	13.986	0.2563267	63.86994915	60.66246609	14.47557243	-0.0825			0.966179	0.00355	723230.7
540	13.986	0.2560497	63.80092795	60.59743431	14.46781125	-0.09375			0.966698	0.003904	722842.9
540	13.986	0.255191	63.58696223	60.39583582	14.44372509	-0.103			0.96831	0.004289	721639.5
540	13.986	0.2553295	63.62147283	60.4283517	14.44761267	-0.1135			0.968049	0.004726	721833.8
540	13.986	0.2559943	63.78712371	60.58442796	14.46625852	-0.12475			0.966801	0.005195	722765.3
540	13.986	0.2548308	63.49720976	60.31127104	14.43360967	-0.13725			0.968988	0.005715	721134.1
540	13.986	0.2544425	63.4004555	60.22010917	14.42269718	-0.151			0.969722	0.006288	720588.9
540	13.986	0.2531956	63.08976043	59.92737228	14.38759928	-0.166			0.972087	0.006912	718335.4
540	13.986	0.2546645	63.45577212	60.27222849	14.42893711	-0.1825			0.969302	0.007599	720900.7
540	13.986	0.2544979	63.41425973	60.23311552	14.42425461	-0.20075			0.969617	0.008359	720666.7
540	13.986	0.252974	63.03454348	59.87534686	14.38135269	-0.221			0.972509	0.009202	718523.3
540	13.986	0.2534726	63.15878163	59.99240405	14.39540371	-0.243			0.971556	0.010118	719225.3
540	13.986	0.2525862	62.9379138	59.78430238	14.37041463	-0.26725			0.97325	0.011128	719796.8
540	13.986	0.2521984	62.84128412	59.6932579	14.35946823	-0.294			0.973992	0.012242	717429.9
540	13.986	0.2521984	62.84128412	59.6932579	14.35946823	-0.3235			0.973992	0.01347	717429.9
540	13.986	0.2505077	62.42000564	59.29632931	14.31164717	-0.3575			0.977246	0.014813	715040.6
540	13.986	0.2503415	62.37859292	59.25731025	14.30693761	-0.3915			0.977568	0.016302	714805.3
540	13.986	0.2493166	62.12321449	59.01669269	14.27786101	-0.4305			0.979558	0.017926	713352.6
540	13.986	0.2494551	62.15772509	59.04920858	14.28179374	-0.4735			0.979289	0.019716	713549.1
540	13.986	0.2506185	62.44761412	59.32234202	14.31478601	-0.521			0.977032	0.021694	715197.5
540	13.986	0.249372	62.13701873	59.02969905	14.27943423	-0.573			0.979451	0.023859	713431.2
540	13.986	0.2508958	62.51671007	59.38744423	14.3226386	-0.6305			0.976496	0.026254	71589.8
540	13.986	0.2508126	62.49597879	59.36791122	14.320283	-0.6935			0.976657	0.028877	715472.1
540	13.986	0.2513119	62.62039137	59.48513275	14.33441367	-0.76275			0.975694	0.03176	716178.1
540	13.986	0.2519214	62.77226292	59.62822613	14.35164426	-0.839			0.974522	0.034935	717039
540	13.986	0.2506185	62.44761412	59.32234202	14.31478601	-0.923			0.977032	0.038433	715197.5
540	13.986	0.2511452	62.57885406	59.4459963	14.32969745	-1.01525			0.976015	0.042274	715942.5
540	13.986	0.2516167	62.69633961	59.55669118	14.34303297	-1.11675			0.975108	0.046501	716608.7
540	13.986	0.2526139	62.94481592	59.79080556	14.37119619	-1.2285			0.973197	0.051154	718015.8
540	13.986	0.2521707	62.834382	59.68675472	14.35868602	-1.35125			0.974045	0.056265	717390.8
540	13.986	0.2532787	63.11046679	59.94688181	14.38994105	-1.4865			0.971929	0.061897	718952.4
540	13.986	0.2530571	63.05524984	59.89485639	14.38369548	-1.635			0.972351	0.06808	718640.3
540	13.986	0.2523923	62.88959896	59.73878014	14.36494247	-1.7985			0.97362	0.074888	717703.4
540	13.986	0.2528632	63.006935	59.84933415	14.37822838	-1.9785			0.972721	0.082383	718367.2
540	13.986	0.2531679	63.08285831	59.9208691	14.38681861	-2.17625			0.97214	0.090618	718796.4
540	13.986	0.2525585	62.93101168	59.7777992	14.36963302	-2.394			0.973303	0.099685	717937.7
540	13.986	0.2530571	63.05524984	59.89485639	14.38369548	-2.63325			0.972351	0.109647	718640.3
540	13.986	0.25242	62.89650108	59.74528332	14.36572433	-2.8965			0.973567	0.120608	717742.4
540	13.986	0.2525031	62.91720744	59.76479285	14.36806967	-3.18625			0.973408	0.132673	717859.6
540	13.986	0.2528078	62.99313076	59.8363278	14.37666597	-3.505			0.972826	0.145946	718289.1
540	13.986	0.252974	63.03454348	59.87534686	14.38135269	-3.8555			0.972509	0.16054	718523.3
540	13.986	0.2539158	63.26921555	60.09645489	14.40788199	-4.241			0.970719	0.176592	719848.7
540	13.986	0.2526416	62.95171804	59.79730874	14.37197772	-4.665			0.973144	0.194248	718054.9
540	13.986	0.2528909	63.01383712	59.85583733	14.37900952	-5.1315			0.972668	0.213672	718406.2
540	13.986	0.2531956	63.08976043	59.92737228	14.38759928	-5.64475			0.972087	0.235044	718835.4
540	13.986	0.2523092	62.8688926	59.71927061	14.36259662	-6.20925			0.973779	0.258549	717586.2
540	13.986	0.2525031	62.91720744	59.76479285	14.36806967	-6.83			0.973408	0.284397	717859.6
540	13.986	0.2515336	62.67563325	59.53718164	14.34068354	-7.513			0.975267	0.312836	716491.4
540	13.986	0.252143	62.82747988	59.68025154	14.35790378	-8.2645			0.974098	0.344128	717351.7
540	13.986	0.2538881	63.26231343	60.08995171	14.40710242	-9.091			0.970771	0.378543	719809.8
540	13.986	0.2534449	63.15187951	59.98590088	14.39462345	-10			0.971613	0.416393	719186.3
540	13.986	0.2613972	65.13338591	61.85287621	14.61691312	0			0.956837	0	730292.4

